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DESIGN OF A 1500 FT/SEC, TRANSONIC, HIGH-THROUGH-FLOW, SINGLE-STAGE AXIAL-FLOW COMPRESSOR WITH LOW HUB/TIP RATIO

COMPONENTS BRANCH TURBINE ENGINE DIVISION



OCTOBER 1976

TECHNICAL REPORT AFAPL-TR-76-59
FINAL REPORT FOR PERIOD 1 APRIL 1971 - 31 JANUARY 1974

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This technical report has been reviewed and is approved for publication.

ARIHUR 5. WENNERSTROM, GS-15 Chief, Compressor Research Group

FOR THE COMMANDER

JAMES L. RADLOFF, Major, USAF Chief, Components Branch ALLEGACIO LA PORTE DE LEGIO DE LA PRIME DE

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SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered) READ INSTRUCTIONS BEFORE COMPLETING FORM REPORT DOCUMENTATION PAGE 2. GOVT ACCESSION I AFAPL-TR-76-59 ATT OF ALL DESIGN OF A 1500 FT/SEC, TRANSONIC, HIGH-THROUGH-FLOW, SINGLE-STAGE AXIAL FLOW COMPRESSOR WITH LOW HUB/TIP RATIO TECHNICAL REPORT (PINAL) 1 APR 71 - 31 JAN 74 6. PERFORMING ORG. REPORT NUMBE AUTHOR'S 8. CONTRACT OR GRANT NUMBER(a) ARIHUR J. WENNERSTROM GECAPT GEORGE R. 10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT HUMBERS PERFORMING ORGANIZATION NAME AND ADDRESS ATR FORCE AERO-PROPULSION LAB/TB Project 7065, Task 13, (Formerly Aerospace Research Lab/LF) Work Unit 27 WRIGHT-PATTERSON AFB OH 45433 12. REPORT DATE 1. CONTROLLING OFFICE NAME AND ADDRESS October 2076 COMPONENTS BRANCH, TURBINE ENGINE DIVISION AIR FORCE AERO-PROPULSION LABORATORY WRIGHT-PATTERSON AFR OH ASASS 15. SECURITY CLASS. (of th UNCLASSIFIED 190. DECLASSIFICATION/DOWNGRADING 16. DISTRIBUTION STATEMENT (of this Report) Distribution limited to U.S. Government agencies only: Test and Evaluation; October 1976. Other requests for this document must be referred to AF Aero-Propulsion Laboratory (AFAPL/TBC), WPAFB, Chio 45433. 17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different frace Report) 18. SUPPLEMENTARY HOTES 19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Axial Compressor Gas Turbine Aircraft Turbine Engine O. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report describes the aerodynamic design of a transonic axial-flow compressor inlet stage designed for a high flow rate per unit frontal area and relatively high aerodynamic loading. The performance objectives of this stage were derived from a preliminary design study of a multi-stage compressor for an advanced turbojet engine. The design goals chosen included a tip speed of 1500 ft/sec, a flow rate of 39.7 lb/sec per square foot of frontal area, a stage total pressure ratio of DD 1 JAN 73 1473 EDITION OF 1 NOV 65 IS OBSOLETE UNCLASSIFIED SECURITY CLASSIFICATION OF THIS PAGE (When Date Ent

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1.91 and a stage isentropic efficiency of 0.83.

The techniques used in the preliminary and detail designs are described. The complete aerodynamic flow field pertaining to the design point is defined on twenty-one stream surfaces, and radial and meridional distributions of significant parameters are presented. Finally, the detailed flowpath geometry is defined and airfoil coordinates are included for both stream surfaces and cartesian manufacturing sections.

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FOREWORD

This report describes the aerodynamic design of a transonic axial-flow compressor inlet stage. The work was performed in the Aerospace Research Laboratories and transferred to the Turbine Engine Division of the Air Force Aero-Propulsion Laboratory, Air Force Systems Command, Wright-Patterson AFB, Ohio. In both laboratories, it was accomplished under Project 7065, Task 13, Work Unit 27. The effort was conducted by Dr. Arthur J. Wennerstrom and Capt George R. Frost (ARL/LF, subsequently AFAPL/TBC) during the period April 1971 to February 1974.

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SECTION I

INTRODUCTION

This report describes the aerodynamic design of a transonic axial-flow compressor inlet stage designed for a high flow rate per unit frontal area and relatively high aerodynamic loading. The performance objectives of this stage were derived from a preliminary design study of a multi-stage compressor for an advanced turbojet engine. In the course of this study it became apparent that the most serious aerodynamic design problems of the overall compressor were associated with the first stage. Specifically, it was necessary to design the first stage with relatively high diffusion factors and stator hub Mach number in addition to high flow per unit frontal area in order to keep loading levels in the remaining stages within reason while maintaining a combustor inlet Mach number less than 0.4. The design criteria finally chosen for the first stage were felt to represent the best compromise from the standpoint of the overall multi-stage compressor. This stage was chosen as the object of an independent research program because it presses the present state-of-the-art with respect to nearly all of its design parameters. Also, it appeared to be a suitable test vehicle on which to assess the usefulness of several vortex generator configurations which have recently proven successful on a more highly loaded supersonic compressor stage.

The preliminary design is discussed in the second section of this report. The third section fully describes the detailed aerodynamic design assumptions and procedures. The final aerodynamic design results are presented in the fourth section. This includes a complete aerodynamic description of the compressor stage in addition to specification of the geometry.

SECTION II

PRELIMINARY DESIGN

1. CRITERIA

All of the criteria defining the basic parameters of this compressor stage resulted from the design goals of a hypothetical turbojet engine of which this compressor comprised the first stage. A flow per unit frontal area of 39.7 lb/sec per square foot was established at the outset as a design goal. A corrected tip speed for the first stage of 1500 ft/sec was also established early in the design study as the maximum value consistent with turbine stress considerations for this particular application. Most of the rest of the compressor characteristics resulted from the overall objective of designing a compressor for a turbojet engine with the minimum number of stages consistent with an overall isentropic efficiency of 0.84, a specified pressure ratio, and a combustor inlet Mach number less than 0.4. Further details concerning design criteria for the complete multi-stage compressor have been deliberately omitted from this report to avoid restrictions imposed by security classification.

2. PROCEDURE

The preliminary design of the multi-stage compressor was accomplished with the computer program described in Reference 1. This computer program performs an axisymmetric, full radial equilibrium analysis of the compressor flow field using the streamline curvature solution technique. Through a series of iterations, it attempts to maximize the performance of each successive stage by driving the design toward one or more of a number of specified limits and with a number of specified constraints. The radial distribution of energy addition in each rotor is specified by the user as a non-dimensional total pressure distribution. The aerodynamic parameters for which limits must be supplied for each stage are:

- (1) Rotor tip diffusion factor
- (2) Stater hub diffusion factor
- (3) Stator hub Mach number
- (4) Rotor hub relative exit angle
- (5) Rotor tip exit whirl velocity

The first three of these limits were found most useful for this investigation. The fourth and fifth were simply set at values which would avoid constraining the results. The general procedure followed was to start by specifying relatively conservative values for these limits. This initially resulted in a design having insufficient pressure ratio and higher efficiency than required within the maximum number of stages allowed. Subsequently, the controlling limits were gradually raised and some adjustments were made to the radial distributions of rotor work and mid-streamline axial velocity ratios until the desired overall pressure ratio was achieved at the objective efficiency and with what appeared to be a good balance of conditions throughout the compressor. In the first part of the preliminary design, the program option involving specified mid-streamline axial velocity ratios was employed and the annulus walls were allowed to float within limits. Final fine tuning of the preliminary design was accomplished with the annulus geometry frozen. A minor modification was made to the computer program for convenience in arriving at this design. This is described in Appendix A.

3. LOSS ASSUMPTIONS

The losses attributed to each blade element and expressed as a relative total pressure loss coefficient have been assumed to be equal to the sum of two components; one associated with diffusion occurring in the profile boundary layers and one related to the presence of shock waves in each blade passage. Shock losses were estimated according to the familiar Miller-Lewis-Hartmann model described in Reference 2. This consisted of assuming the shock-related portion of the relative total pressure loss coefficient to be that resulting from a normal shock, the upstream Mach number of which was equal to the arithmetic average of the relative inlet Mach number and the suction surface Mach number at the shock impingement point. This latter Mach number was assumed to differ from the rolative inlet Mach number by a Prandtl-Meyer expansion through a specified number of degrees of turning. The previously mentioned modification (presented in Appendix I) to the computer program described in Reference 1 consisted of an option allowing the program user to specify the supersonic turning angle. This proved to be more convenient for this design exercise than other options available to accomplish the same purpose. The final version of the preliminary design assumed the supersonic turning angle to vary linearly from 12 degrees at the hub to 2 degrees at the tip for the rotor and assumed a constant 15 degrees for the These assumptions were varied somewhat in the early stages of the preliminary design until the approximate blade geometry became evident. Where the Mach number relative to a blade element is less than one, the procedure was handled slightly differently in order to effect a smooth transition in the loss distribution. The suction surface Mach number was assumed to be that resulting from a Prandtl-Heyer expansion from Mach 1 through the given supersonic turning angle. Then, the upstream shock Mach number was assumed equal to

$$H_{x} = \frac{M_{1r}}{2} \quad (1 + Mss)$$

instead of the previously used average value. Whenever $M_{\rm X}$ was less than or equal to 1.0, shock loss was assumed to be zero.

Losses resulting from diffusion were predicted in the Lieblein manner by a relative total pressure loss parameter versus diffusion factor relationship. The computer program of Reference 1 allows this relationship to be defined at 10, 50 and 90 percent span, independently for each blade Initially curves taken from Figures 33 and 34 of Reference 3 were employed as representing the latest published revision of the original correlation. However, as the preliminary design began to take shape, the objective pressure ratio was achieved within the desired number of stages, but with efficiencies bordering the incredible, several points above the best ever obtained under similar or easier circumstances. Even greatly increasing the supersonic expansion angles to clearly impossible values did not bring the predicted efficiencies within the realm of credibility. A closer examination of the loss parameter correlation of Reference 3 led to the conclusion that the prediction shown for rotor profile loss appeared extremely optimistic for diffusion factors less than 0.5. representing essentially the entire range of interest for this design. The floor level of the loss parameter curves had been shown as approximately 0.002. For this design, this was raised to 0.009 and new curves were created which passed through the values given by Reference 3 at a diffusion factor of 0.7, and were extrapolated to 1.0 for the rotor, and retaining the prediction of Reference 3 for the stator, reasonable results were achieved. The distributions used are reproduced in Figures la and lb of this report.

4. DESIGN PHILOSOPHY

a. Velocity Triangles

The choice of velocity triangles throughout the multistage compressor was most strongly influenced by the desire to achieve the maximum pressure ratio per stage consistent with reasonable off-design performance and the design efficiency objective. Since all rotors were expected to operate at relatively high levels of diffusion, high rotor relative Mach numbers and the associated shock losses were viewed as an acceptable penalty for the resulting performance. Although variable inlet guide vanes (IGV) might be desirable to expand the part-speed operating envelope, they were not desired from the point of view of altering the relative inlet Mach number of the first rotor, nor could significantly cambered IGV be tolerated at design point operation because of the high flow rate and resultant danger of choking. Consequently, a design approach was adopted which employed no IGV, assumed that the first stage stator would be a rigid structure supporting the front bearing and transmitting services, and assumed that satisfactory off-design performance could be obtained by variable stators in the second and later stages, and an articulated trailing edge in the first stator and/or bleeds if necessary. Furthermore, all stators were designed to turn the flow back to the axial direction.

b. Axial Velocity Ratio

Three factors guided the magnitude and distribution of axial velocity ratios selected for each blade row. First, the entire multi-stage compressor required an overall axial velocity ratio less than unity in order that the combustor inlet Mach number not exceed 0.40, one of the initial conditions. Rather than force just one or two stages to accept a particularly low axial velocity ratio, it was decided to allow the stage axial velocity ratios to gradually decline over the first few stages and then remain approximately constant over the balance of stages. A mid-streamline axial velocity ratio of approximately 0.98 was chosen for the first stage. The second two factors determined the distribution of axial velocity ratio between rotor and stator. Rotors have generally proven capabl of operating at nigher loading levels than stators having addal losses. This favored axial velocity ratios less than unity in rotors and greater than unity in stators. Also, as the axial velocity ratio across a rotor is reduced, the camber required to produce a given change in swirl velocity is also reduced. Consequently, since average rotor relative Mach numbers were much higher than average stator Mach numbers, low rotor axial velocity ratios tended to minimize supersonic turning angles, and consequently shock losses for a given level of solidity. The mid-streamline values ultimately arrived at for the first stage were 0.815 for the rotor and 1.206 for the stator.

c. Annulus Shape

The shape chosen for the compressor annulus represented a compromise between maintaining high enough blade speed to facilitate obtaining high pressure ratio per stage while at the same time not permitting the hub/tip radius ratio at the compressor exit to become too high. There were also mechanical considerations involved such as ease of maintaining tip clearance and stresses in the last rotor. The shape ultimately chosen incorporated a constant outer diameter over the first three blade rows. The outer diameter was then reduced somewhat across each stator starting with the second stage. All rotors downstream of the second maintained a cylindrical outer diameter for ease in controlling tip clearance, although these diameters were progressively This choice of contour produced an adverse aerodynamic condition with respect to the effects of streamline curvature on aerodynamic loading. However, this

aerodynamic effect had such small impact on loading levels and losses that it was considered a desirable trade-off against better control of tip clearance.

d. Aspect Ratio

The choice of aspect ratio was governed by four factors, not all of which were always important in any one stage. the first stage, the most important factors were hub ramp angle, mechanical stresses, and aerodynamic stability. High aspect ratio tended to minimize stage weight and rotor root stresses but tended toward steep hub ramp angles, greater flutter sensitivity necessitating part-span dampers, and less stall margin. Lower aspect ratio improved these last three conditions at some sacrifice in the first two, but if carried too far, could lead to unacceptable rotor root stresses due to increasingly acute angles between rotor blade and hub near the trailing edge. Downstream of the first stage, ramp angle and blade stresses became progressively less important and a fourth factor, manufacturing cost, became more important. Lower cost favored lower aspect ratio in later stages. The computer program of Reference 1 employed an aspect ratio based upon the ratio of leading-edge span to the axial depth of a blade row. Using this definition, a value of 2.0 was selected for the first rotor, which resulted in an initial hub ramp angle of approximately 30 degrees and appeared to offer reasonable prospects of not requiring mid-span dampers. The aspect ratio of each of the next several blade rows was chosen strictly on the basis of adjusting the axial length of each blade row such that the hub ramp angle declined monotonically and smoothly from the inlet value to nearly zero. An aspect ratio of 1.0 was chosen for the last few blade rows as representative of the minimum value offering an acceptable ratio of blade span to circumferential spacing.

5. RESULTS

The final results of the preliminary design pertaining to the first compressor stage and its immediate environment are shown in the following pages of computer printout. The information presented is sufficiently complete that, with the aid of Reference 1 and the associated computer program (available from COSMIC), anyone so inclined should be able to duplicate the results.

One of the input requirements of this computer program was a nondimensional spanwise total pressure distribution in the exit plane of each rotor. For the first few design iterations, total pressure leaving each rotor was assumed constant as a matter of convenience. As soon as the design began to evolve, however, it became necessary to increase the total pressure leaving the hub of each of the first few rotors in order to compensate for stator hub losses and to obtain a reasonable

balance of conditions throughout the compressor.

The diffusion factor at the rotor tip proved to be the limiting parameter in the first stage. This reached the specified limit of 0.52. The resulting Mach number relative to the stator hub was barely supersonic at about 1.02 and dropped rapidly with increasing radius. The stator hub diffusion factor was somewhat high at about 0.55, but the predicted losses were acceptable and this appeared to be a necessary compromise for the benefit of subsequent stages downstream. The mid-streamline axial velocity ratio of 0.815 across the first rotor kept the relative turning angle across the rotor tip down to 2.4 degrees. This was thought to offer good prospects of minimizing rotor shock losses and deviation The solidity variation in the first rotor assumed for the preliminary design (a linear variation from approximately 2.0 at the hub to 1.3 at the tip) proved eventually to be somewhat low. This solidity was increaesed during the detail design procedure discussed later in this report.

The performance predicted for the first stage was a total pressure ratio of 1.93 at an isentropic efficiency of about 84 percent. Reducing the aerodynamic loading would have led to slightly higher efficiency and substantially less design risk in this stage. However, it would have required higher loading in downstream stages and/or a higher discharge Mach number from the last stage, neither one of which was viewed as desirable from an engine design standpoint.

A matter of practical interest to users of the computer program associated with Reference 1 concerns the tolerances applied to portions of the iteration scheme. Most of the tolerances recommended in Reference 1 were found satisfactory. However, for this design, much less difficulty was experienced with the program when the loading limit tolerance was increased from the recommended 0.01 to 0.033.

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******* FINAL FLOW PARAMETERS FOR STAGE MUNBER 1 *******

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SECTION III

DETAILED AERODYNAMIC DESIGN

1. COMPUTATIONAL METHOD

The detailed aerodynamic design of the first compressor stage was accomplished with an early version of the computer program described in Reference 4, and employing the "streamline curvature" method of computation. Although conceptually similar to the method employed for the preliminary design, much greater precision was incorporated into the detail design by the addition of many more axially-distributed computing stations to define the flow path, including four stations within the interior of each blade row. The detail design program permitted the use of curvilinear computing stations, and these were adjusted periodically to insure a high degree of coincidence with blade-row edges. Twenty-one streamlines there employed for the detail design in contrast to the eleven employed for the preliminary design.

A solution was obtained through an iterative numerical procedure according to which the equations of momentum, continuity, and energy are simultaneously solved at each computing station in sequence throughout the compressor. After each "pass" through the compressor, the streamline geometry is updated and the procedure is repeated until the changes occurring from one pass to the next fall within a specified tolerance, whereupon the solution is considered to be "converged." The most significant assumptions are that the flow is axisymmetric and can be described by a series of concentric streamsurfaces across which no mass or momentum is transferred. Within this framework, the "full" radial equilibrium version of the momentum equation is satisfied at each streamsurface/computing-station intersection whereby effects of streamline curvature and entropy gradients are included. For the computations made within a blade row, blade force terms are included in the momentum equation in the form of a body-force field assumed to act in a direction everywhere normal to the three-dimensional surface formed by the stacked camber lines of each blade row. correction for the meridional entropy gradient was included according to Reference 5.

An allowance for boundary layer blockage was incorporated to account for boundary layer development on both blades and annulus walls. The absolute value of blockage was estimated according to a simplified formula for a turbulent boundary layer on a flat plate, with meridional velocity and length substituted for absolute velocity and path length. The method used is substantially as described in Reference 6 and, although relatively crude, it has produced reliable results

under a variety of circumstances. The resulting total blockage calculated at each computing station is linearly distributed from hub to tip as a function of radius and is introduced as a factor in the continuity equation. Within the interior of blade rows, the additional blockage resulting from the finite thickness of the airfoils is also taken into account.

2. AURIOIL SELECTION AND OPTIMIZATION

When a design is accomplished involving computing stations internal to a blade row, some optimization criteria must be specified according to which the most efficient airfoil geometry can be selected from among a variety of possible designs satisfying the same end conditions. The axial distribution of static pressure along each streamsurface, as computed by the axisymmetric flow analysis, was selected as the most appropriate parameter to optimize for this design. This was chosen on the basis of being the parameter most closely related to blade surface boundary layer behavior which could be calculated with some degree of accuracy. minimum static pressure gradient along each streamsurface would obviously occur with a linear variation between leading and trailing edge. Since this condition could probally not be realized in practice, high deviation angles and losses would be the probable result. The "optimum" axial distribution of (circumferentially averaged) static pressure along each streamsurface has been defined as one which is approximately linear over the first three quarters of a blade row and then declines smoothly to nearly zero at the trailing edge in deference to the Kutta condition.

Two basic design approaches are feasible in conjunction with the optimization criteria described above. In the more traditional approach, one can assume the blade geometry, solving for the equilibrium flow field using specified relative flow angles as input to the aerodynamic program. this design approach, the parameters defining the blade geometry are adjusted through a series of iterations until the optimization criteria are achieved over as much of the blade surface as possible. This technique has two shortcomings. First, one does not have infinite flexibility to adjust the shape of blades of a specific geometric family, so the optimization criteria can rarely, if ever, be achieved over the full span of a blade. Second, the use of specified relative flow angles as input to the streamline-curvaturetype aerodynamic analysis program can lead to numerical instabilities and convergence difficulties in the calculation procedure at high subsonic through-flow Mach numbers. The design approach using arbitrary airfoils avoids both of these difficulties and was chosen for this design. Using this technique, the designer must assume the work distribution (total temperature or enthalpy) along streamlines through the

rotor and the swirl velocity (or preferably radius times swirl velocity) distribution along streamlines through the stator. The aerodynamic flow field analysis then produces a set of relative flow angles to which airfoils must be matched. The technique and computer program described in Reference 7 were developed for this purpose. This procedure is iteratively repeated until the optimization criteria are met over the full span, airfoil metal blockages used in the aerodynamic analysis are mutually consistent with those calculated by the blade generation program, and the computing stations used to represent blade leading and trailing edges are a close match to the envelope of the stacked airfoil. pursuing such a design approach, it is absolutely essential to insure that the distributions of work through rotors and radius-times-swirl-velocity through stators vary smoothly both along streamlines as well as along computing stations. Any lack of smoothness in these distributions will be directly translated into peculiarly shaped airfoils having undesirable mechanical and probably undesirable aerodynamic properties. A point of practical interest to designers is that linear distributions of these variables along streamlines provide an excellent starting point for a design. adjustments away from the linear distribution required to achieve the optimization criteria are usually not very large.

3: INTRA-BLADE AERODYNAMIC ASSUMPTIONS

In conjunction with a through-the-blade-row design technique such as described above, some assumption must be made for three critical meridional distributions within each blade row. These are deviation angle, blockage, and losses, listed in decreasing order of importance. At high relative flow angles such as encountered near the tip of a high-speed rotor, the performance is extremely sensitive to changes in relative flow angle. There is virtually no experimental data available to define a reliable correlation applicable to the interior region of a compressor blade row. Furthermore, few if any reliable analytical techniques are currently available to predict circumferential average relative flow angles through a transonic blade row. Consequently, distributions were assumed which met the following criteria:

- (1) Deviation at the leading edge must equal the incidence angle
- (2) Deviation at the trailing edge must equal the value predicted by conventional empirical deviation angle correlations
- (3) Deviation angles in the covered portion of the passage should be extremely small

(4) The rate of increase of deviation angle approaching the trailing edge must approximately equal the rate of change of camber in that region in order to approach a Kutta condition at the trailing edge.

The distributions chosen for this design are presented in Figure 2.

The absolute level of blockage at each computing station was calculated according to the crude boundary layer model mentioned earlier in Section III.1. Although the computation was originally conceived as an annulus wall blockage model, it was employed here as a wake blockage model and linearly distributed spanwise. The ratio of hub blockage to tip blockage within each blade row was set equal to the ratio of hub solidity to tip solidity. The distribution is shown in Figure 3.

The aerodynamic calculation was least sensitive to the meridional distribution of losses within each blade row. Also, viewed in the meridional plane, the rotor shock system covered most of the axial depth of the rotor. Consequently, total pressure losses were simply linearly distributed through each blade row.

4. ANNULUS SHAPE

When designing a compressor incorporating blades of a specified geometric family, e.g. multiple circular arc, etc., coupled with a through-the-blade-row design approach, it is usually found necessary to adjust the annulus wall contour within the blade passage in order to satisfy optimization This frequently results in locally undesirable pressure gradients due to streamline curvature effects near the walls. With arbitrary airfoils, such as employed for this design, this situation can be largely avoided since the airfoil can adjust to meet optimization objectives over its entire surface, independently of the wall contour. Consequently, a specific objective in laying out this design was to maximize the radii of curvature defining the hub flowpath. As a result, the spinner contour is a circular arc tangent to the rotor hub, the rotor hub was made conical, and the hub flowpath from the rotor trailing edge to the exit plane is a single circular are tangent to the rotor hub and to a cylinder about half a stator chord length downstream of the stator exit plane. A reflex curvature in this contour was deliberately avoided. The tip flowpath consisted of a circular-arc bellmouth tangent to a cylinder which extended past the stage exit plane.

5. ROTOR ASPECT RATIO

Whereas the preliminary design employed only a single, radial computing station to represent both the trailing edge of one blade and the leading edge of the following blade, the detail design used individual curvalinear stations to represent each edge as well as intermediate locations. axial depth of the rotor at the hub was selected as the more important axial dimension to preserve without change from the preliminary design, since it directly affected rotor hub ramp angle. During the course of detail design iterations, it was necessary to reduce the inlet hub/tip radius ratio from the preliminary design value of approximately 0.35 to 0.31 in order to eliminate choking problems. At the rotor trailing edge, the hub/tip radius ratio was similarly reduced from 0.54 to 0.52. These hub changes caused the final ramp angle to rise to 32.5 degrees, the axial depth having remained constant. Final rotor aspect ratio was 1.32 based upon mean rotor span and the average of the chord length of blade sections on streamlines 1, 11, and 21.

6. STATOR ASPECT RATIO

The stator aspect ratio was decreased somewhat from the preliminary design, primarily as a result of the choice of hub flowpath contour described in Section III.4. The stator exit-plane area was preserved from the preliminary design, fixing the hub radius at this location. This radius intersected the circular arc defining this contour about twenty percent farther downstream from the rotor than in the preliminary design. The resultant final stator aspect ratio was 1.255, based upon mean blade span and the average of the chord length of blade sections on streamlines 1, 11, and 21.

7. ROTOR SOLIDITY AND THICKNESS

Rotor solidity and thickness are discussed together because of their relationship from a structural standpoint. Maximum section thicknesses of 6.0 percent chord at the hub and 2.5 percent chord at the tip were selected as the minimum This subsevalues likely to be acceptable structurally. quently proved adequate. Preliminary centrifugal stress calculations also indicated that rotor airfoil crosssectional area should increase by a factor of approximately two from tip to hub. Rotor hub chord was already established within narrow limits on the bases of flow area contraction ratio and ramp angle, as discussed in Section III.5. These constraints fixed the tip chord length at approximately 4.0 inches. Aerodynamic considerations dominated the choice of tip solidity, with no constraint placed upon maximum hub solidity. It was desired that the tip solidity be high enough so that a weak oblique passage shock extending from

the leading edge of one airfoil to the suction surface of another would be fully captured within the passage. This was felt to enhance aerodynamic stability. A tip solidity of approximately 1.5 was chosen so that such a shock would intersect the suction surface at about 90 percent chord. This tip solidity plus the chord length set the number of rotor blades at 20. An even number was chosen for convenience in balancing the rotor. The resultant hub solidity was approximately 3.2. Because of the high shock losses which were potentially possible near the tip and the danger of choking near the hub, leading edge wedge angles were minimized by locating the position of maximum airfoil thickness relatively far aft. A linear spanwise distribution was specified, varying from 56 percent chord at the hub to 70 percent chord at the tip. The airfoil leading edge radius was initially fixed at 0.005 inch, spanwise constant, in order to minimize shock losses. However, high leading edge stresses near the hub subsequently caused the leading edge radius to be flared to triple this value within the last fifty percent of span approaching the hub. This distribution is shown in Figure 4. During the first few iterations of the detail design, linear spanwise distributions of chord length and thickness were specified. However, the resultant solidity at about two-thirds span appeared to be dangerously low from an aerodynamic standpoint. The final configuration was achieved by specifying the solidity distribution shown in Figure 5, increasing the chord length and decreasing the thickness near two-thirds span to preserve the satisfactory, nearly linear area distribution. The final spanwise distributions of thickness-to-chord-ratio, and streamsurface-section and cartesian-section area are presented in Figures 6 through 8 respectively.

8. STATOR SOLIDITY AND LEADING-EDGE SWEEP

The stator solidity distribution was defined purely on the basis of aerodynamic considerations related to loading, operating range, and leading-edge sweep. Sweep was used at the hub to minimize shock losses and to maximize incidence The locally high hub solidity also reduced the diffusion factor at the hub relative to the preliminary design, which had shown an increase in that region. Chord length was approximately fixed according to the considerations related to aspect ratio and hub flowpath contour described in Section III.6. An odd number of blades having no common divisor with the 20 rotor blades was desired to minimize the chance of exciting any resonant frequencies in the rotor through rotor-stator interaction. A minimum solidity of approximately 1.6 was selected because of the high turning required of the stator (varying from 40 to 50 degrees) and the high average Mach number level varying from about 0.7 to 1.0. These conditions were satisfied by 31 stator blades.

Initially, the stator trailing edge was a radial line coincident with the stacking axis. However, this resulted in a tip solidity of about 1.48 which appeared risky in relation to the turning, Mach number, and incidence variation which this region would experience over the expected operating range. Tip solidity was increased to 1.62 by slanting the trailing edge linearly aft from hub to tip with respect to the stacking The leading edge at the hub was located as far forward as mechanical clearances permitted, resulting in a hub solidity of 2.8. The angle of sweep was chosen such that the component of Mach number normal to the leading edge was approximately 0.4, the Mach number below which no further increase in low-loss incidence range has generally been observed in cascade experiments. The sweep with respect to the approach flow was smoothly reduced to zero at a radius near mid-span where the Mach number had dropped to about 0.85. The leading edge then swept slightly forward toward the tip simply to maintain adequate solidity at the outer radii. The final chord length and solidity distributions are shown in Figures 9 and 10. Maximum thickness was located at fifty percent meridional chord and its absolute value varied approximately linearly from 4.0 percent chord at the hub to 6.0 percent chord at the tip. Leading and trailing edge radii were approximately constant at about 0.0055 inch.

9. INCIDENCE ANGLE

The use of arbitrary airfoils allows greater design freedom in choosing incidence angle than exists with airfoils of a specified geometric family. Using a through-the-blade-row design approach and arbitrary airfoils, any reasonable distribution of incidence can be assumed and an apparently satisfactory solution obtained. Particularly with supersonic sections, the adequacy of the initial assumption should be tested by analyzing several sections in the cascade plane.

The initial assumption made for this rotor was a constant 1.0 degree of incidence with respect to the suction surface. Because the relative inlet Mach number to the rotor is supersonic over most of the span, flow through the rotor is controlled primarily by the wave pattern propagated upstream. A cascade-plane analysis using an inviscid, time-dependent calculation technique showed the initial rotor design to be about four percent deficient in the flow at both hub and tip. This corresponded to approximately one degree of incidence with respect to the suction surface. The final design assumed a constant 2.0 degrees of incidence with respect to the suction surface. The corresponding spanwise distribution of incidence with respect to the camber line is shown in Figure 11.

The stator inlet Mach number varied from approximately sonic at the hub to 0.7 at the tip. Because of the sonic Mach number and high solidity at the hub conducive to choking and also the

incidence tolerance presumably offered by leading edge sweep, a positive incidence of 5.0 degrees with respect to the camber line was assumed for the hub. Zero degrees of incidence with respect to the camber line was assumed for the stator tip. This was selected on the basis of high cambered subsonic cascade sections favoring low to negative incidence angles and also the expectation of high incidence angles occurring here as the stage was throttled toward stall. The spanwise variation from hub to tip was made linear and is also shown in Figure 11. No subsequent checks or adjustments were made to this distribution.

10. DEVIATION ANGLE

Deviation angle was predicted for both rotor and stator according to the method developed by NACA and described in Reference 8, Equations 269 and 271. A shape correction factor of 1.0 was used for both blade rows. However, the values predicted for the rotor were increased by 2.0 degrees at all radii, based upon examination of a few examples of potentially relevant recent data. The design deviation angle distributions for both blade rows are presented in Figure 12.

11. AIRFOIL FILLET RADII

The treatment of fillet radii at the rotor hub and both hub and tip of the stator merits mention because the approach was unconventional. For decades great attention has been paid to the design of fillets at the juncture of an aircraft wing and fuselage. Poorly designed fillets, or no fillet at all, can lead to large interference drag penalties. Also, it is well known that in diffusing passages, boundary layer growth in corners is greater than on adjacent surfaces and boundary layer separation will generally occur first in a corner under an adverse pressure gradient. However, common practice in turbomachine design appears to favor the smallest possible fillets for aerodynamic reasons, mitigated only by manufacturing and structural desires for larger fillets. fillet geometry chosen for this design is patterned after the aircraft wing-fuselage model, although somewhat simplified. A radius of 0.25 inch was employed over most of the chord length; a rather large value in relation to most significant dimensions of this 17.0 inch diameter stage. The fillet radius declines smoothly from 0.25 inch to 0.06 inch over a distance of 0.75 inch approaching the leading and trailing edges of the rator and the leading edge of the stator, and over a distance of 0.5 inch approaching the trailing edge of the stator. Note that the stator is hub-shrouded and the fillet treatment applies to both platforms.

12. STRUCTURAL IMPACT ON AERODYNAMIC DESIGN

A stress analysis of the steady state centrifugal and gas bending loads was performed for the rotor as part of a mechanical design and fabrication contract. Small adjustments to the section centroid locations with respect to the stacking axis were required and the leading and trailing edges approaching the hub platform were thickened before satisfactory stress levels were achieved. All of these adjustments were recycled through the aerodynamic design calculation so that the final aerodynamic design was fully consistent with the structural design. A peak combined stress level of about 68,000 psi was predicted to occur at the leading edge at a radius of 6.5 inches at 20,000 revolutions per minute operating speed. The predicted rotor untwist distribution is shown in Figure 13. Correction for untwist was made by restaggering the cartesian airfoil manufacturing sections an equal and opposite amount.

Vibratory tests of sample airfoils were also performed under the above mentioned contract in order to establish natural frequencies and mode shapes and to determine strain gage locations and dynamic stress operating limits. Three gage locations were chosen corresponding to points of maximum sensitivity for the three lowest order modes of vibration. These modes were 300 Hz (first bending) 1050 Hz (second bending), and 1400 Hz (first torsion). The first eight modes of vibration were mapped and stress ratios defined for the three gage locations. The eighth mode was a complex mode at 4900 Hz. An operating dynamic stress limit of ±20,000 psi was chosen.

SECTION IV

FINAL DESIGN RESULTS

1. STAGE DIMENSIONAL CHARACTERISTICS

Stage Outer Diameter (constant)	17.00 inches
Rotor Inlet Hub/Tip Radius Ratio	0.312
Number of Rotor Blades	20
Number of Stator Blades	31
Static Rotor Tip Clearance	0.027
Design Point Rotor Running	
Clearance	0.016
Rotor Aspect Ratio	1.320
Stator Aspect Ratio	1.255

2. DESIGN POINT SPECIFICATIONS

Flow Rate	62.60 lb/sec
Flow Per Unit Frontal Area	39.715 lb/sec/ft ²
Flow Per Unit Annulus Area	43.995 lb/sec/ft ²
Rotor Total Pressure Ratio	1.966
Stage Total Pressure Ratio	1.912
Rotor Tip Static Pressure Ratio	2.169
Rotor Isentropic Efficiency	0.869
Stage Isentropic Efficiency	0.830
Inlet Corrected Tip Speed	1500 ft/sec

AERODYNAMIC CHARACTERISTICS

The details of the aerodynamic flow field throughout the stage are presented in the following pages of printout from the aerodynamic design computer program. The numbers and arrangement of computing stations are presented in Figure 14. For convenience, the computing stations defining blade row edges are also defined below.

Rotor leading edge - Station No. 11 Rotor trailing edge - Station No. 16 Stator leading edge - Station No. 18 Stator trailing edge - Station No. 23

The final streamwise distributions of total temperature through the rotor and radius-times-swirl-velocity through the stator are presented in Figures 15 and 16 respectively. The resultant streamwise static pressure distributions within both blade rows are shown in Figure 17. Figures 18 through 23 present a variety of spanwise parameter distributions of common interest. Rotor and stator relative inlet Mach number, diffusion factor, and total-pressure loss coefficient distributions are presented in Figures 18 through 20 respectively. Distributions of rotor-exit and stage-exit total pressure ratio, meridional velocity,

and isentropic efficiency are presented in Figures 21 through 23 respectively. The manufacturing dimensions of the annulus are shown in Figure 24.

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	23.4603	Q.	65.283	ċ	518.7	518.3	1521.60	1517.25	+659+	0.036	-1.394			000 • 0
	24-2003	9	65.253	É	511.7	518.3	1521.38	1217.25	105.44	0.000	0000			0.00

STATION 2

				6 29	GENERAL FLOW	H PARAMETERS	.KS						
Agius	317"DS68	OCITI	TAMGENTL.	TEMPERATURES FOTAL STATE	ATMES STATIC	PRESSURES TOTAL STA	SURES STATIC	MACH	MAIRL ANGLE	St. OP 2 Angle	RABOOF CURVIREO	STATIC	INCIDENCE DEVIATION
00000	\$0. 921	43.921	0.300	518.7	518.1	1521.63	1515.41		9.000	0.000	0.00	6460	0.000
2.1753	\$6.733	60.703	0.333	518.7	518.1	1521.00	1515.44	. 07 24	0.030	-3.141	2167.75	.0549	0.300
4.3633	50. BIO	63.313	000.0	513.7	518.2	1521.00	1515.54		0.00	661.9-	+272,29	3550	0.00
5.4631	79.470	73. 470	0.00	\$1.0.7	518.2	1521,00	1515.61		3.000	-7,058	******	6450.	00000
6.5631	78.600	73.803	0.000	516.7	518.2	1521.63	1515.70		3.000	6+0.6-	-1597.00	. 0549	0.00
7.6532	27. 438	77.939	3.4.30	516.7	519.5	1521,00	1515.81		3.000	-10.350	-710.32	. 0549	000.0
6.6572	77.061	77.001	0.000	516.7	516.2	1521.00	1515.93		00000	-11,561	-405.00	6460.	0.000
6246.6	75.339	75.953		518.7	516.2	1521,00	1515.07		0.000	-12.647	-260.16	6450 •	00000
11.0925	74.750	74.793	6.360	515.7	518.2	1521.00	1516.23		0.000	-13.594	-179.89	6460 •	00000
12,2582	73. 638	73, 433	0.136	510.7	516.2	1521,00	1516.40		0.000	-14.379	-130.37	6450.	000 0
13.4426	724 337	71. 937	3.000	513.7	516.3	1521.00	1516.58		3.000	-14.375	-98.85	6+60.	0.000
16+6433	70.299	73.233	0.000	518.7	518.3	1521,00	1516.78		3.000	-15,353	-76.35	.0540	000.0
15-8733	000-000	64.533	0,000	518.7	518.3	1,521,60	1516,99		000.0	-15.475	-61.15	6450.	0.000
17.1385	36.536	05.530	0.00	516.7	516.3	1521,00	1517,22		00000	-15.295	-43.61	6450*	000.0
18.4232	04.430	6***33	0.100	518.7	516.3	1521.03	1517.46		0.030	154.757	-40.91	6450*	0.000
19.7535	52-110	62,113	050*0	516.7	510.4	1521,00	1517,71		00000	-13.787	-34.25	.0549	00000
21.1225	59.571	53.571	3.000	516.7	510.4	1521,60	1517,97		090.0	-12,289		. 0549	00000
21.6229	58.211	55.211	2.300	518.7	518.4	1521.00	1518.11		0.00	-11.301		6 750 .	00000
22,5353	56.735	55.755	000.00	518.7	510.4	1 52 1 . 63	1516.25		0.000	-10.128		6460.	0.00
23.2637	55.286	55,285	0.300	518.7	516.4	1521.00	1519.39		0.000	-8.746		6450.	0.000
24.4600	53.717	53.717	000.0	518.7	518.	1521.00	1518.54		0.800	-7.125	-22.52	6450.	000.0

GENERAL FLOW PARAMETERS

STATION 3

45	RADIUS	A930_UFE	OCITI MERIDAL.	TANGENTL.	TEMPER TOTAL	TEMPERATURES OTAL STATIC	PRESSU TOTAL	URES	NUMBER	M+ IRL Anglē	SLOPE Angle	LAD.OF CURVTRE.	STATIC	INCIDENCE DEVIATION
-4	6.000	135. 336	105.309		516.7	517.7	1521,00	1511, 36	.6953	0.000	0.000	00.00	. 0547	00000
*	£ 26.4.7	107-029	167.023	•	516.7	517.7	1521,000	1511.23	9960•	0.000	-3.295	-754.13	.0547	0.000
m	3,7853	106.656	105.665	0.000	510.7	517.7	1521.30	1511.30	* 0957	3.030	-b.013	-370.58	.0547	600.0
*	+-7323	106.357	106-357	•	510.7	517.8	1521.00	1511.41	+ 0951	00000	*8.263	-283.15	.0547	0.000
J	£299°5	105,176	105-175	_	518.7	517.8	1521.00	1511.57	* 98 * 3	00000	206.6-	-222,03	• 0548	0.00
•	6.6407	133, 392	101.962	_	516.7	517.8	1521.00	1511.78	. 6933	0.000	-11,527	-177.32	• 0548	0.00
~	7.6083	102,672	162.472	_	518.7	517.8	1521.00	1512.04	• 0919	00000	-13.136	-143.48	.0548	0.000
•	6.5633	160.631	100.631	Ī	510.7	517.8	1521.63	1512.36	• 09 02	0.000	-14.725	-117.29	.0548	00000
•	9.5875	79**BF	95.444	_	518.7	517.9	1521.00	1512.73	. 0663	000.0	-16,289	-96.67	. 6548	00000
=	12.6073	95.632	95. 832	_	510.7	517.9	1521,00	1513, 16	. 08 60	0.00.0	-17.823	-86.23	.0548	00000
멸	17.6547	956 726	92.35-	_	510.7	516.0	1521,00	1513.63	.0833	000.0	-19.320	-66.37	.0548	0.00
Ŋ	12.7157	49.607	63-607	_	516.7	518.0	1521,00	1514.15	.0803	3.900	+22.0%-	-56.16	• 0549	000.0
2	13.0594	\$5.65¢	65.624	_	518.7	716.1	1521.60	1514.72	• 07 69	0.000	-22,175	-47.28	. 0548	0.00
*	15.0325	61, 574	61.57*	_	518.7	516.1	1521.00	1515, 32	. 87 31	00000	-23.513	-39.91	.0548	0.000
10	16.2700	76, 823	75, 823	_	510.7	518.2	1521.00	1515.96	• 06 89	00000	-24,776	-33.73	6450.	0.000
	£7.5451	72.527	11.527	_	216.7	518.3	1521.00	1516.63	. 06 41	0.000	-25,952	-28.50	6450.	0.000
<u></u>	19.0003	65.630	65.633	~	510.7	518.3	1521,00	1517.32	+ 05 88	0.000	-27.030	-24.02	6450 •	0.00
=	19.7537	62.434	62.+34	_	518.7	518.4	1521.60	1517.67	• 05 60	000.0	-27.529	-22.00	6450*	0.000
	20.5423	59. 556	53.056	•	518.7	518.4	1521.00	1518.02	• 05 29	000.0	-28.003	-20.11	6450*	000.0
2	21.3721	35.480	D44 . A40	_	518.7	518.4	1521.00	1518.37	.0497	0.000	-28,455	-18.34	6450.	0.00
<u></u>	22.2550	51.64	51.0564	_	518.7	518.5	1521.00	1518.72	.0463	0.000	-28.891	-16.60	6450.	000.0

NON NO	KA3Ius	4 2 4 3 2 4 3 5 3 5 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	G C I T I	r s ratestr	Temperal Fotal	STATICES STATIC	PRESSURES TOTAL STAI	STATIC	MACH	M41RL Avgle	SLOPE Angle	LAD.OF CJRVIRE.	STATIC JENSITY	INCIDENCE
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~ (3 :	143.44	103. 447	200	213.7	216.2	1521.00	1+90.15	٠	200	0 + 0 + 0	, e	* 0.0 *	000 • 0
Na i	1.7623	130.710	£03.7£5	30F*3	513.7	510.4	1521.60	1-97.30	7	. 300	-3.+60	+25b.1	•	000.0
~	3.0293	154.155	101.155	0.160	715.7	515.3	1,721,00	1+30.97	•	. J.J.:	-0.961	1748+3	**50*	900°0
* 1	3.7753	106.373	105+373	3	116.7	510.3	1521,60	1+90.91	•	.000	-6.733	1420.1	* + + + + + + + + + + + + + + + + + + +	0.000
ıa v	1125**	158, 236	101.232	0. ac	135.7	516.3	1521.00	1+90+95		3.030	-10.533	1290.54	* 0244	0.000
، م	5.268.	157.723	107.725	9	526.7	510.3	1521.00	1.97.09	•	. DJ ü	-12,304	1293.0	****	0.00
٠.	0.11/3	20 m = 10 m = 1	155.540	3 . J	515.7	510.4	1221.03	1+97.35	•	. 00.	-14.233	1454.	* 0.00 + 4	0.00
• •	12//5	105.402	152.652	7 J	2.516	510.4	1525.00	1.97.73	•	. 03¢	-16.143	1962.9	* 024	000
* ;	1.0342	105.04	103.2-3	300.0	513.7	5.16.5	1521.00	1-90.23	٠	700°	-18.107	+749.1	+ 620+	0000
2:	7007	300 0101	191. 15.	3 (11016	v	1521.69	1+96.57	•	300	-26-12+	D * D + S + -	9,	000.0
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					9	GENERAL FLOM	H PARAMETERS	.kS						
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NOI	7	ABSOLUTE	17.	AVERATE	TOTAL STAT	STATIC	TOYAL STU	SIATIC	NUAS 33	AVGLE	ANGLE PNGLE	CURVIR.	DENSITY	DEVIATION
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٠,			454.923	1. SEE	2.010	212.7	3047763	1+50.56	• 20 12	020	0000		9	000.0
٠.	10000		520-607	900	215.7	511-7	1521.00	1+50.00	. 20 12	000	-2.054	40.01	2	000
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~	1.6853		250.247	9.710	516.7	511.9	1521.00	1452.12	22.82	000	(2,531	74.95	3	0000
•	5.273+		164 52	3000	518.7	512.3	1541.00	1-52.95	. 2566	300	-14.124	69.00	9	00000
σ,	5.073.		222.150	0.333	515.7	512.1	1521.00	1-54.04	.25+5	.00:	-15.449	64.37	Ş	000 0
a ;	6.4872		121 * 6.22	909	716.7	512.2	1521.03	1450.45	. 25 17	000.	-17.906	60.73	. 0533	0.000
4	1.1003		273.237	30.0	215.7	512.4	152 . 33	1+57.2	.24.81	000	-20.038	58.12	5	000.0
21	7.7.664	2/0,320	270.323	0000	518.7	512.0	1521.00	1423.40	. 2436	200	-22.226	56.30	.0534	0.000
2	96.0		754 1 20	9 7	7100/	6.214	1251	1+02+29	. 23 80	000	24.0.42	55.33	3	000
::	6275.6		200.557	200	510.7	513.2	1521.00	1+02+20	. 2510	900	-27 -0 13	55.00	5	000.0
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5	12,2653		193.541	0.00	518.7		1521.00	1487.15	1730	9 6	101 to 10	95.28	5.00	
20.2	12.7659		133.153	4,350	21.8.7	10	1521.01	1640.00	7	000	110.01	76.7	5	0.00
	13,5033		174.971	9,300	510-7		1521.03	1.95.00	1572	000	41.8	216.77	5	0.000
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LOCA T TON	RADZYS	V £ L ABSOLUTE	OCITI MERIONE, 1	L S TANGENTL.	TEMPEKATURE TOTAL STAT	TURES		ES	HAGH NUMB ER	H4IRL Angle	SL OPE ANGLE	RAD. OF CURYTRE.	STATIC	INCIDENCE DEVIATION
ina 4#4r = 4#400						######################################	1521-00 1521-00 1521-00 1521-00 1521-00 1521-00 1521-00 1521-00	1377-00 1334-82 1334-89 1334-89 1334-89 1337-72 1293-86 1255-86 1255-86 1255-86 1255-86	50 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		24	0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	44444444444444444444444444444444444444	
zanaz Zanaz		610,000 611,200 611,200 621,500 621,510 625,010	Property of the state of the st	300.00 300.00 300.00 300.00 300.00		4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1521.00 1521.00 1521.00 1521.00 1521.00	1232, 19 1225, 57 1222, 26 1216, 94 1215, 59			-114-625 -114-703 -126-803 -17-000	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	6470 0470 0470 0470 0469	# <b>0 0</b> 0 7 8 <b>8</b> 0 0 0 0 0 7 0 0 0 0 0 <b>9</b> 0 0 0 0

STATION 6

					**	HIRAL FLO	STALRAL FLOW PARKMETLRS	.R.		-				
TION	RADIUS	A 1 PASSOLUTE	TEATTON.	I seconte	Temple fotal	Timp_Ratures Otal static	PREDSURES TOTAL STAT	SURES STATIC	MACH MUNHER	H4IKL Avgle	St. JPL Argle	RA 0.0F CURVIRE.	STATIC	INCIDENCE DEVIATION
4	1.6211	333. 456	333. +10	19	¥14.7	525	1521.60	1392,78	3276	0.00	30.796	16 6 10 10 10 10 10 10 10 10 10 10 10 10 10	.0516	0.00
cu.	1.7727	18. C.J.	-1333	4.000	21.6.7	1000	1521+60	1370.57	. 35.03	0000	27.95	5.30	. 0512	000
-	2.4333	经保持 医院乳中	473+ DJ	**	520.7	7.005	1521,00	1330,19	+317	3.000	19.072	7.31	.0502	000
4	₹.603±	147.739	+47.23)	٠.	510.7	640.1	1522,03	1319.93	1+0+.	3.000	15.715	8.55	1640	000.0
W	3.1773	\$19.50	514.201	7.7	518.7	496.2	1521.00	1302,76	16740	0.000	12,327	9.73	• 0+92	00000
خ	3.2527	\$ 55. 324	513,333	***	510.7	434.2	1221.4	1280.57	05.64.	0.600	10.556	10,79	.0488	000 0
•	3.930.	507.032	16.0 . Lake	***	510.7	4.35.4	1221,00	1271.20	.5423	00000	8.482	11.71	+ 0+8+	0.00
•	4. 5192	5 75.156	\$75.143	3	516.7	-91.2	1>21.63	1250.53	\$20.8	3.000	6.055	12.49	.0480	00000
ø	*.703.	W-118 A	2-4-164	***	516.7	*59.0	1,221,03	1242.45	. 54.55	30000	**932	13,13	.0476	000-0
<b>0</b>	5.0024	63%.378	363. A74	13	520.7	400	1521.03	1226.82	. 56 đó	0.000	3.307	13.58	• 0472	000
₩ <b>+</b>	5.0000	271.7-1	021.7.1	179	513.7	\$ 56.0	1,521.93	1215.47	. 57 52	3.000	1.307	13.32	6940.	000
77	5.6497	£ 16, 133	515.353	G	1.614	4.42.	1521.00	1202,16	15037	0,000	35.25	13,31	. 0469	00000
m M	5 - 6 325	\$ > 1 · 1 2 5	992+929	-39	513.7	433.4	1521.63	1165.55	.6042	0.000	762	13.52	. 6461	000.0
₫ :	b.6271	636. 237	565.237	-3	516.7	631.7	1521.00	1174.22	• 0195	0.00.0	-1.399	12,37	1640*	0.000
ψ. 100	7.6327	612-206	275.02-		<b>526.7</b>	6.674	1 321.03	1150.34	66800	4.030	-3.165	12.13	.0453	0.000
9	4 CON .	7 20.336	763.645	7	2:0.7	£77.8	3 52 h = 68	1101.16	1+00.	3,606	-4.337	11.23	.04+8	000.0
7	7.775	721.297	721.237	13	514.7	**5.2*	1521,00	1120.67	.0751	0.000	-5*+70	10.15	. 0442	0.00
#	7.9701	7 52. 232	722. 5.12	•	516.7	474.9	1521,60	1109.42	.6003	0.000	-4, 35	9.01	£ + 0 +	0.000
<b>6</b>	4.16.7	7 * 5 * 7 4 5	743.234	133	516.7	472.2	1521.03	1395.35	.69.47	0.030	*D.000	9.00	. 0435	00000
70	0.3572	745.524	7034 334	•	510.7	*7G.3	1521.53	1003-10	.7133	3.000	-7.163	8.32	+ 0432	0.000
z	\$ 55.50 \$	773.70.	713.1.	<u>د</u>	513.7	6.90*	1521.00	1967.91	.7232	00000	-7.772	6.00	.6427	000-0

### STATIO 4 9

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4 0C4	esto tus				TLMPERA	A 1 URE 5	PRESS	1U255	AACH	# 4 I Kit	S. 09 .	440.0F	STAILC	INCIDENCE
5		10000 m		14.65.41	1	**	TO 7 4 L	SIVI	40340 F	4.46LE	ANGLE	CJRVIRE	JE 4SITY	DEVIATION
-4	1.55.1	4+3.2-4	+93.2.3	3376	213.7	4.88.	1521.60	1323.04	. 42 08	3.030	39.926	*6 *	.0498	000
•	2.2211	を はなる かりか	437 - 164		\$3.4.7	** 75.*	1524.00	1510. 00	. 45 65	0.000	33.160	-135.07	9640	000
<b>~</b>	2.76.5	中文章 医后角	520.132		520.F	445.7	1521.00	1247.30	. 4622	3.000	24.222	15.25	. 0491	0.00
•	1.030.	1 62 42 43 1	546.23		512.7	49m . 2	1521.00	1204-17	. 4978	3.036	20.757	13,33	.0487	000
<b>\$</b>	3.4242	Soc 200	100.430	_	516.7	6.3.5°	1521.03	1269.00	.5153	0.000	17.062	12.54	. 0483	0.000
•	3.7721	£ 25 °6 4 6	シャン・ログル		526.7	1.05	1521.00	1252,55	.5341	3.000	15.365	12,15	.8479	0.00
	4.1255	12. T. A.	54.1.023		510.7	430.0	1521.30	1235.27	. 55.35	0.000	13.208	12.29	. 8474	00000
•	279***	614.77	41.4.2.43		7.014	4.40.4	1521.63	1217.74	.5723	3.000	11,253	12.75	6940.	000.0
•	400000	6 20- 528	635.223	_	514.7	9.534	1521.00	12002	.5915	6.033	9.472	13.46	*940*	000.0
•	6.5823	636.8-5	6+5 et 64.		S. S. S. S.	402.3	1521.69	1163.08	.00.35	0.000	7.836	14.42	.0460	0000
<b>~4</b> :	5.5553	573.92¢	¥73.062	_	216.7	5 × 7 5 4	1521.00	1107.78	.6253	00000	50.30	15.57	.0455	000.0
N.	4.3123	いれたののかな	ちょう ちょうい		7. B. 7.	5.615	1521.03	1152.91	.6.19	00000	+06++	15.93	.0451	000.0
7	6.2793	475.4	7.00 M		¥14.7	477.0	1521,53	1139.19	. 62 52	0.000	3.717	16.52	. 0447	000 0
	0.045	7.5.479	7250 xl 5	_	* 50.4	10.1	1521.03	1126.54	•6695	00000	2.599	20 • 37	***0.	0.00
9	7.0673	740.456	725. 933	_	7.61.4 7.14.7	476.7	1521.03	1115,24	.6603	0.000	1.612	22,53	. 0441	000.0
٠	7.37.37	F 57 - 357	757. 537	•	\$ 50° 7	*73.	1521.63	1104.92	·60.15	00000	4760	25.10	.0438	000
_	4 4 450	1 40 - 244	70 X 2 X 4	•	N - 64 A	47243	2221.60	1095.56	. 76 13	3.600	8+0•	25.23	.0435	0.0CJ
	7.9355	7 10. 954	722. 522	•	514.7	4.4.4	1521,00	1391,26	.7655	0.000	-,257	30.05	4540.	00000
•	6.121)	724. 325	754, 929	_	2.016	.71.3	1521.03	1367.14	1607.	00000	1200-	32+10	.0433	000.0
2	CHURTON .	725.758	7:5.7.3	•	518.7	470.6	1521.00	1363.21	.71.37	0.000	762	34.45	.0432	000.0
::	4.5003	4269	102. 101	Ī	514.7	*7E . 3	1521.00	1079.46	.7175	3000	962	37.06	0 2 7 0 *	000 •0

ATATION SO

SHILDAR FLOW PARAMETERS

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110%	KADIOS	4 2 t	40454 F. 1	7 × 5 14366.476.	16.90 Ex.	ardess States	PHZ3SU TOTAL	STATIC	AACH AUMBER	AAIRL	SLOP C Angle	2AD.OF CURVIRE.	STATIC DENSITY	INCIDENCE DEVIATION
-4	2.5347	\$40.734	*69.7.	***	414.7	*32.5	1321.03	1:68.91	. 5156	9000	35.268	-6.21	2.640.4	000
~	2.531.5	ないのいなかべ	炒中路 旧游池城		510.7	6.44	1521.63	1273, 19	• 51.06	0.000	31.762	-12.08	9890	0.003
*	4.0513	A > 2 . 7 + 6	545.7 . 5	.09	7.0. V	432.	1521.00	1257.35	0010	3.006	25.625	31.50	E840.	0000
*	3 - 310 -	5.5.346	475. 530	-	#1 G . 7	3 - 7 6 "	1321.60	12565	. 22 36	3.00.6	23.103	16.38	0.840	0.00
¢ì	3.623.	A 15. 15. W	593.763	966.0	21.8.7	e39.	1521.63	12+0+59	54.70	300.3	26.705	13.32	. 0475	000 0
¢	\$4.50°E	€ E×+ # L G.	中国 中	•	V.414	2019	1 521.03	1221.75	4 C 4.	0.000	16++30	12.33	0.470	0.00
	4.23.27	6 57. 433	637.547	•	V. 4.7.4	4.44.	1 >21.00	1201.02	6040.	3.000	40.309	12.8+	.0465	0000
•	4.6342	D 39. 41.	146.600	•	410.7	4300 W	E 5.2 2 . 6.3	1179.32	14100	3.000	1 ** 322	13.29	6429	000 0
<b>.</b>	4.4775	5.37. AKY	633.947	•	21.7.7	4/6.0	1521.63	1157.38	*0372	0.030	12.454	14.16	0492	000 0
0	S - 1223	136.018	750.057		41.0.7	217.2	1221.03	1135,90	.65.35	3000	16,031	15.53	9540	0000
11	5.00 M	745. 453	7230 455	479	× 40 14	4.00	1 >2 1 - 44	11120.75	. 580-	0.000	3.033	17.04	.0441	0000
iş H	6.457+	7 and 9 kg	744. 550	<b>.</b>	118.7	472.0	1921.03	1397.35	.6993	360.0	7 * + 7 5	20.00	. 0436	000.0
"	6.151.	7646 F.S.	702.73	***	\$10.7	.70.5	1 521.63	1031+25	. 71.97	0000	6.000	24.32	0+31	000*0
4	£.7623	773.479	173.474	6	7.4.7	4.00.4	1921.53	1,107.69	. 72 33	3000-	702	31.	. 9427	000
5	7.0517	7.54. 1.42	Fee Laz	8	212.7	407.4	1521.03	1157.17	.7 - 31	3.030	*6**	+1.31	.042*	000.0
2	7.4832	7.5.7.2	192.145	*****	514.7	***	\$ 52 1, 63	1343.35	.7+50	3.036	2.415	66.43	• 0422	0.000
*	7.7515	10000	743.741	7	V****	4.66.4	1 52.1. 0.3	136.016	. 7 > 53	0.030	20473	96 . o 2	. 6420	0.000
ei ei	7.4202	7 14. 1.2	7.94 - 3u2	•	210.7	5.25	1521.00	1362.47	.7550	3000	1,052	135.34	.0420	0.000
<b>4</b>	C+1 140	7.17	*** ***	73	42.8.2	かんない	1 121.60	10-1.33	. 7502	3,00,6	9000	212,52	. 0420	00000
<b>8</b>	4.4173	ゆうひ シング	432. 340	**	414.7	京 中央の事	1521.00	13-0.68	.7200	3.000	0 M 2 C	448.49	. 0413	00000
<b>.</b>	V604.4	がたからのつび	かんだ " かいお	•	4444	するながま	1>21.00	13.0.47	. 75.70	00000	00000	0.03	.0419	000.0

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FLOW
FO - K-02
s.

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100	20104a	4 2 K	***	1	12. MP2. 42.7 TOTAL X	4103014 814110	TOTAL	PRESSUALS LUTAL STATIC	MACH	#41%L #466.	St. 3Pr. Angle	RADOF	STATIC	INCIDENCE
•4	2.4524	\$ 5 ** \$ \$	\$2 K . \$ 23		7.50.7	-	£ \$22.00	127 - 35	50.32	00000	3262	******	.0465	0000
*	2.2173	5434 324	シング・ナイグラ	4. 304	× 2.4. 7	6.36.4	からないのの	127 0. 36	-51.49	00000	31.00.52	31.89	1010	0000
<b>~</b>	3.2431	132.753	\$44.02¢	#37 · 0	424.7	#30°+	\$ 20.4.00	1253.01	. >373	999.9	27.548	14.07	.0476	0.00
	30.9151	433.270	403.2 244	94.0	5:4.7	4.44.	1521.43	1232.14	.5270	3.096	25.+28	12.37	B 240 .	000 • 3
<b>*</b>	3.407.3	660. 563	625.513	\$ 4 4 6 6	7.414	4.00	1521.00	1211-10	. 57 39	0.000	23.212	11.57	.040.	000.0
•	** \$ \$ \$ £ 2	18 CA 18 28 28 28 28 28 28 28 28 28 28 28 28 28	512 - 174	明しなるが	2 424	* 53.4	1521.60	\$1.50.28	04,70.	3.630	21.013	11,37	.0461	00000
	4.4.24.4	017.423	477.434	4.300	V +4 44	次・心がす	2 721 . 50	1163. 30	.6303	3.036	10.001	11.25	.0454	0000
-	4.7.65	123, 3.9	40 A Sec	ゆうか・カ	514.7	W. 7 V.	1921,60	1130,56	52.00	3.000	16.422	11.35	2440 *	000 • 0
•	4 2 6 5 2 4 4	129. 4.27	723.442	0000	2:4.7	*/**	1521.00	1112.30	.6033	3.000	1+.659	11.50	0 440	000
2	£ * 4 £ £ 4	*** *** *** **	今後のこのなん	967.0	5.54.7	172.2	1521-03	1.165.53	.7113	0000	12.37"	11.94	.0432	00000
**	5.1324	7.52.734	. 42. 73.	90.00	21.5.7	V. 7 Ca	1.923.60	1,54.64	.7330	30000	11.17+	12.43	.0425	000
~	6.0711	647. 319	* 17 · 1/54	964.9	7.4.7	1.14	1521.00	1532.50	.7551	2.036	¥.451	13,33	.0417	0000
2	540700 ·	432,512	220 · 15 #	0.00 C	410.7	401.2	1521.03	1335.17	.7537	0.000	7.791	24.33	.0410	000 • 0
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STATION 12

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FLOW PARAMETER	PRE TOTAL	1695.19 1732.35 1775.05 1775.05 1775.05 1777.65 1802.49 1801.45 1833.41 (643.29 1865.86 1865.86 1865.97 1861.97 1861.97 1861.97 1861.97	#ACH NO.S OUTLET .6408 .65408 .6554 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251 .7251
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### OFERALL PERFORMANCE PARAMLTERS

N-PARAMETERS MEAN PARAMETERS STATION-TO-STATION INLET-TO-STATION 1 SENTROPIC PHENSURE RATIO 1.2052 1.2052 1.2052 1.2052 1.2052 1.20501 1.20501 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001 1.05001	L395.	٠	•	٠	•	•	٠	٠	٠	•	99.046.	•	•	44.	•	•	٠	٠	03 68426	•	23 - 6136	STATION 13
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STATION-T PRESSURE RATED	1.11%	1. 1217	1. 1330	1.2+53	4.1555	1.1656	1.1755	1.1851	1. 19.3	1.2324	1.2893	1.2151	1.2134	1. 223	1.2257	1.2507	14227	1. 2252	£0.22.33	1.2222	\$- 2284	
81822# -CIME	**	N	×	*	•	•	•	•	•	•	3	75	77	**	<b>S</b> 3	=	17		*	2	Z	

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	5.3893	7.2.528	650.697		554.3	508.4	1912.75	1413.22	+67 21	26.781	32.461	0.00	.0521	630.0
	5.5233	754.252	664.109		555.7	\$09°	1923.13	1412.33	. 66 27	25.239	32.936	-262.64	.0521	0.1.0
	3-6717	779.457	692,652		55.00	505.8	1972.86	1415.30	. 7056	27 - 369	27.361	-67.65	.0522	200.0
_	4.0453	794.635	706.051	360.750	562.1	508.5	2003.49	1+20.71	.7184	25.939	25,322	-45.34	.0523	0.00
	4.3387	827.976	721.790		565.0	510.6	2037,29	1429.83	.7297	25.735	23.218	-36.93	• 0525	0.063
	6.5963	619.347	734.238		567.0	511.9	2069.92	1+40-18	.7390	25,337	22.086	-31.75	.0528	0.00
•	4.6542	027.736	744.541		570.4	513.3	2099,67	1452,01	*7.55	25.908	18.982	-27,20	.0530	0.003
	5.1339	432, 251	751. 43.3		572.7	515.	2420.22	1466.36	*40+1*	25.476	16.980	-25.60	<b>• 0534</b>	0.00
e CA	6644°S	435° 254	755.733		574.9	517.0	21+9.75	1462,25	.7487	25.045	15.103	-24.95	.0535	0.000
	5.7047	634.475	755.762		576.9	518.9	2170.52	1+98.17	.7475	54.599	13,351	-24.70	.0541	0.00
-	5.9937	634.133	Tu1. 3+4		528.7	520.4	2146.23	1512.64	*7.460	24 - 123	11.653	-25.86	. 0545	000.0
N	6.2365	432,334	762.379		580.4	522.7	2242.30	1526.68	.7429	23.659	10.6A1	-29.32	.0548	9.00
49	6.5834	828.325	761. 181		501.9	524.8	2212.04	1540.65	.7379	23.228	8.541	#35 · 0 9	. 0554	0.0
	6.8852	£21.626	757.124		583.2	527.0	2216, 87	1554.07	.7303	22.854	6-858	-42.57	.0353	000.0
w)	7.1929	611.946	743.610		564.5	529.6	2217.34	1570.09	.7200	22.501	5.361	-46.21	.0556	0 . T . O
	7.5675	799.256	733, 120		545.8	532.6	221 + 66	1587.10	+7067	22 - 368	3.608	-42,30	• 0559	9.00
	7.8302	763,832	725.253		587.1	535.9	2213, 34	1605.47	60691	25,292	2,320	-34.76	. 0562	0.00
4	7.4966	775.5%	717.546		547.3	537.7	2208.06	1616.75	• 68 25	22.291	1.028	-32.52	.0564	<b>4.03</b>
	6-1611	767-132	763.710		566.5	539.5	2205.74	1627.07	.67 40	22.308	966*	-33.88	. 0566	000.0
	8.1237	754.932	762.848		2002	541.3	2203.34	1636.47	.6657	22.328	844.	-45.21	.0567	0.00
	4.5.800	752, 154	6.85. 0.34		590.0	542.9	2200.78	1644.47	65 49	22.310	0.000	00.0	. 1568	0.000
!	1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1												

STATION 13 IS AT THE EXIT OF A ALAGE ROW ROTATING AT 20222.0 RPM.

### STATION 14

LOCA	rad Ius	ABSOLUTE		I L I FONL, T	E S #HGEMTL.	TEMPER TOTAL	TEMPERATURES OTAL STATIC	PRE: TOTAL	PRESSURES AL STATIC	MACH.	H4IRL A4GLE	SL OP E ANGLE	RAD. OF CURVTRE	STATIC . DENSITY	INCIDENCE DEVIATION
- a a p s a a a a a a a a a a a a a a a a	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	6672, 907 66672, 907 66672, 907 66672, 907 6677, 907 677, 907 677, 907 677, 747 675, 674 775, 674 775, 874 775, 874 775, 874 775, 874 775, 874 775, 874 775, 874		666 666 666 666 666 666 666 666 666 66	508.369 508.369 508.369 508.369 508.369 508.369 508.369 508.369 508.369 508.369 508.369 508.369 508.369 508.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 608.369 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K 1 E	RELAI OPT.IN	101 101 101 101 101 101 101 101 101 101	AM OCT   1   1   1   1   1   1   1   1   1	RELATIVE INLET 693.916 714.9763 754.9763 795.201 899.906 899.906 899.906 899.906 1105.198 1105.939 1126.203 1304.636 1136.636 1136.636 1136.636		N	INLETATIVE TO A CONTROL OF CONTRO	#ACH NO.S OUTLET .6249 .6249 .6345 .6775 .7316 .7316 .7316 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512 .7512	COEFF 0 2023 0 2023 0 2027 0 2027	DE HALL BEALL BEAL	ATT	UPELTA P 0 D O O O O O O O O O O O O O O O O O O	INL ADDRESS OF THE PROPERTY OF	SPEEUS 6659.7 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 7330.2 73300.2 73300.2 73300.2 73300.2 73300.2 73300.2 73300.2 73300.2 7	2 STRE N LINE N

### OVERALL PERFORMANCE PARAMETERS

CTREAM	•	AQ-MATTACTO-CT-201-12.50	PADE ATTEND	TMI - T-TO-	STATTON-6	SAST STATES TATES AND TERS	MEAN DARAGETERS	STATION-TO-STATION	MOITATA-CI-TAINI
-LINE	-	DELTA T	ISCALADOIC	PRESSURE	BELTA T	ISENTROPIC	PRESSURE RATIO	1+1629	1.6560
		7 10	EFFICIENCY	RATIO	<u>2</u>	ZFF1015NCY	DELTA T ON T ISEN. EFFICY.	######################################	. 1725 . 8983
•4	1.132.		.9573	1.42.1	.1075	.9459			
~	1.1336	:	.9653	1.4377	.1113	9496*			
<b>**</b>	1.1365		. 3313	1.4707	.1201	9096.			
•	1.1462		-986-	1.5093	•1270	,9786			
*	1, 1553		.9794	1.5488	. 1363	.9763			
•	1, 1525		.9773	1.5821	.1436	.9732			
•	1.1637		.9732	1.6065	1436	.9639			
•	1,1529		.9667	1.6243	* 121	.9634			
•	1.1596		. 3575	1.6392	+ 156+	9566			
27	1.1535		1546.	1.6547	.1630	0646*			
4	1.1616		. 9327	1.6708	.1679	* 9401			
77	1.1645		0026*	1.6861	.1739	.9302			
73	1,1562		<b>966€</b>	1,6989	.1778	. 9191			
4	1.1717		.9016	1.7078	. 1621	• 9066			
3	1. 17 42		. 5930	1.7118	.1861	• 6914			
3	1.1.42		.6763	1.7097	.1695	• 6719			
Ħ	1,1598		.6415	4.7000	• 1935	1548			
7	1.1553		. 6146	1.6916	.1953	•6293			
£1	1.1593		.7 622	1.6612	.1972	.6109			
2	1.1521		.7 427	1.6569	.1991	6064			
12	1.1441	.0559	.7 005	1.6554	.2011	.7698			

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LOCA	RADIUS	4 ≤ L ABSOLUTE	G C E T 1	E S TANGÉNTE.	TEMPER TOTAL	NTURES STATIC	PRESS TOTAL	PRESSURES TOTAL STATIC	HACH	WHIRL	SLOPE Angle	RAD.OF CURVTRE.	STATIC DENSITY	INCIDENCE DEVIATION
**	4.000		724.568		656.0	518.2	2513,66	1507.08	• 38 30	43.054	32.461	******	• 0545	0.000
8	4.1697		722+574		691.9	950.6	2544.55	1528.81	. 6652	43.033	31.009	71.66	.0551	000 *0
140	4.4587		720.257		607.0	526.0	2615,01	1583.07	.6781	+3-120	27.442	25.13	.0564	000.0
•	6+6349		722. 829	674.48%	610.6	529.2	2663,53	1613.94	.8773	43 - 036	24.883	34.05	.0572	0,000
*	4.6 305		725. 793		614.3	532.7	2714.69	1647.83	.8756	42.859	22.430	65*44	.0560	0.000
ف.	5.8393		725.177		617.5	536.7	2753.69	1687.43	. do 68	+2.568	20.106	50.03	.0590	0.000
Po	5.2584		722.60E		420.5	5.0.9	2795,12	1728.56	.8583	42.379	17.856	64.19	• 0599	0.000
•	5-4-550		718.96		623.0	545.1	2825.07	1769.39	.8456	42,015	15,660	91.41	• 0609	00000
•	5.7193		71.00		625.3	. 4.645	2648.33	1809.74	. 8319	41.642	13.528	158.12	.0618	0.00
7	5.9607		709.644		627.5	553.5	2868.02	1546.53	. 61.87	41.226	11.470	1449.47	.0626	0.000
#	6.2083		707.063		629.5	B. 160	2684.63	1479.71	• 80 69	40.761	9.548	-213.92	.0633	00.00
7	6,4630		70+.090		632,1	501.1	2898.25	1910.18	4562.	602 • 0+	7.798	-105.84	.0638	000.0
23	6.72.4		700.295		634.4	565.6	2903, 86	1939, 30	.7638	39.912	0.235	-73.89	• 0644	0.000
#	6.9946		695, 315		636.6	569.1	2915.90	1967.23	.77.19	39.591	4.854	-63.73	.0648	0.00%
2	7.2723		688. 415		639.4	573.4	2913.56	1993.45	.7590	39 . 378	3,627	-71.05	• 0652	0.000
2	7.5591		676.739	٠	642,1	578.0	2913, 37	2016,45	.7446	39,311	2,529	-145.90	• 0654	0.480
23	F-8571		664.930		645.0	583.3	2033.27	2034-33	.77.77	33.454	1.533	209.37	• 0654	0.000
47	6.0111		653.758		646.5	5.96.2	2876.15	2040.73	.7177	39.538	1.076	92,39	. 0653	900-0
<b>:</b>	6.1632		644.943		648.1	589.3	2854.26	2045.40	.7068	39.906	.653	70.89	.0651	0.00
7,5	6.3313		632.403		649.8	592.6	2828.25	2048.71	.6947	40.262	982.	85.10	.0648	000 0
ij	8.5866	£15.469	618, 127		651.5	596.2	2793,02	2051.12	• 66 16	<b>*0.712</b>	0.000	00.0	.0645	0000

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E0S. TL.ET	39.	786.8	852.5	4.689	9200	10.89.4	1051.9	1095.6	1140.5	110000	1283.3		1366.5	1413.7	1441.0	1500.0		64.	. 8891										, j.r			•	i	
	659.7	735.0	609.1	85%.2	0.3501		•		1126,0			0	<u></u>	<b>.</b>	<b>.</b>			ATION INLET													i			
DELTA P UPON Q	.1030	1694	1700	.1784	1650	1941			1549	7.436					2260	•		-T0-STAT; -1305 -0410	* 202*												-			
FFUS CTOR	00	0000000	0	0000-0		3 (4	000000	0-0800	000000000000000000000000000000000000000		00000		2			900		STATION-TO-ST 1-1305 00410	-														•	-
HALL	1.045	973	.961	946	700	916			912		914	.914	.913	216	1 C	606*		PARAMETERS URE RATIO I T ON T	EFF LUT.											٠				
•	. 1276	,0353	4620.	0640	0045°	. 0579	.0643	.0717		1000	1131	• 1301	. 1528	1670	7000	•2190	ETERS	MEAN PARAMETER PRESSURE RATIO DELTA T ON T	INER. EP			-			-					,				
MACH NO.S OUTLET	60 60 60 60 60 60 60 60 60 60 60 60 60 6	6537	6099	. 567.8	6889	.7024	.71.19	. 7.47	1997	A1 47	.8479	• 6765	8405.	91100	9500	6656	IANCE PARANETERS	ETERS ITROPIC CIENCY	9882	986	7286	9795	9722	.9673	9613	9450	9368	9548	8972	6796	8572 8228	9608	212	
RELATIVE	. 6249 . 6358	6775	. 6945	.7119	7512	*7749	. 7985	. 8242	65516	4116	*9427	•	1.0078	1.0245	1.0594	9	LL PEXFORMANCE	TIOX-PARAN LTD T ISEN H 7 EFFI	.1566	. **	•	• '	•	•	•	• •	• •	•	.2278	•	2379	•	•	1963
VELOCITIES OUTLET	725.926	735.638	747.476	758-100	787.115	662-909	829.831	450.044	555-515 522-615	956: 236	394-955	1032-619	1070,759	1069,613	1128-499	1148,517	OVERALL	INLET-TO-STATION-PARAMETERS PRESSURE DELT# T ISENTROPIC RATIO OM 7 EFFICIENCY	1.6559	672	7193	1.7512	345	1183	1574	1456	5968	*9855 * 255	.9176	-9195	1.9154	•		1.8482
LATIVE	707-616	757 - 334	776.180	799,816	54.8.509	677.317	987.879	949.000	424-476	1049, 336	1066.985	1130-015	1172.569	11344863	239.76	1263.445			2965		<b>D</b> (	7841	87.58	9656		17.5	9	9136			<b>.</b>	7555	2621	
ANGLES JUTLET	14. W	-11-191	-17.04	-16,946	-24.8±8	-27.680	-31.202	34.516	-46.637	-63.666	-46.219	-48.905	519 615	100000		M)   Jr		TOM-PARA	745	6445	•	24.00	•	•	* /545	***					•	•	•	
w .	-17.534			-27.623					- 424-44-				-26+436		716	426		TO-STAT DELTA ON T		·.•	•	• •	•	•	•			• (		•	• •	•	•	• •
RELATIVE GA OPT-IN- INLET	¥ • • •	77	?	77	179	7	7	7		1	3	**		h 4		4		STATION-TO-STATION-PARAMETERS PRESSURE DELTA I ISENTADPIC RATIO ON I EFFICIENCY	1.1628	1.1636	10 S 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4.4524	10266	2. S. C. C.	101419	1-1195	1-1351	101181	1.1229	1-1214	##Z1*X	1-1170	20 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1.1117
STREAM LINE O	-1 <b>(1)</b> (1	• •	<b>6</b>	<b>.</b>	•	•	7	1	24	3	53	97	h d		12	Z.	53	STREAN -LINE	wi	•	₩.	e u	•	<b>~</b> 1	<b>*</b> •	<b>.</b> =	<b>4</b>	<b>1</b> 2	14	<b>S</b> :	15	*	21	ia

STATION 16

GENERAL FLOW PARAMETERS

LOCA	PARTESS	14	1 3 8	. W	TLMPER	TURES	PRES	SURES	HACH	HAIRL	St. OP E	RAD. OF	STATIC	INCIDENCE
TION		ABSO, UTE	HERIDM.	TANGENTL.	TOTAL	STATIC	TOTAL	TOTAL STATIC	NUMBER	AVGLE	ANGL E	CURVIRE.	DENSITY	DEVIATION
. <b>W</b>	5.6612	1172,697	713.683	930.519	6+0,6	526.2	3163.85	1588.28	1.0433	52.513	32.461	*****	• 0566	0.000
•	4.5378	1155.206	712, 106	913	5.0.49	528.6	3158.05	1614.89	1.0276	52.060	31.031	-51.15	. 0573	000 • 0
**	6.7653	1116, 232	704 . 604	865	639.9	536.2	3139.91	1690.60	.9838	50,851	27.234	-13.18	.0591	000.0
- 48	355.0	1041.433	703.650	934	639.5	540.4	3126.58	1733.52	.9581	49.856	25.406	-366,99	• 0602	0.000
•	50 W W W	1071.038	707.793	603	639.2	543.8	3112,28	1766.40	.9373	+9 • 635	23,253	31.62	• 0609	6.000
•	5.2811	1051,648	710.529	775	638.9	6.946	3096.99	179b.29	.9177	47.497	20.789	36,16	.0616	000 00
~	5.46.6	1031, 302	710.225	7.47	638.7	550.2	3080.48	1926.97	.8972	45.475	18,399	49.15	.0623	000.0
•	5.6573	1010-493	707.654	721	638.5	553.6	3063.20	1957.67	. 67 64	45.549	16.113	49.72	.0629	000.0
ď	5.8612	990.093	703.97*	696	638.5	557.0	3045.69	1867.03	.8561	4++682	13.944	45.48	. 0635	000.0
01	6-0759	971.036	769.250	672	638.8	560.3	3028,59	1913.61	.8372	43.855	11.917	30 . 38	.0641	000 •0
<b>.</b>	6.3035	954,039	695.927	651.	639.3	563.6	3012.03	1936 63	. 8201	43.072	10.024	24.21	* 10644	0.00
73	6.5403	938.604	693.462	632	6+0.2	556.9	2995.60	1956.53	. 8045	42 • 369	8.272	21,56	* 0647	000.0
**	6.7850	924.357	665.923	615	641.5	570.4	2975.60	1974,30	. 7896	41.797	6.670	21.01	• 0649	000.0
3	7.0403	909.865	682.235	601,	643.1	574.3	2969.43	1991, 09	.774F	41,411	5.223	22.41	• 0650	000 •0
15	7.3857	962.569	672,752	590,	645.5	578.7	2942.27	2007.98	• 7595	41.286	3.943	26.00	.0651	000.0
46	7.5813	681.350	560.033	564	546.8	584.1	2926.15	2025.01	.7442	41.508	2,827	34.31	.0651	000 •0
7.7	7.6713	666. 4+0	1643.457	583	653.5	590.8	2914,19	2046-18	.7291	42.186	1.839	56.38	. 8656	0.000
7	8.0215	862.476	633.433	585	655.6	534.7	2910.17	2057,30	.7217	42.735	1.377	85.53	6490*	000 0
57	6.1760	656.493	021.935	568	669.1	599.0	2900.72	2069.17	.7141	43.430	.919	153.20	• 0646	000
2	6.3353	850.074	663.734	593	0.450	603.8	2902,65	2081.71	.7060	4++267	•456	368.65	• 0647	000.0
# 54	6.5603	642.842	593.531	598.418	668.1	609.0	2897.64	2094.71	.6970	45.235	0.000	00.00	• 0645	000.0

# STATION 16 IS AT THE EXIT OF A BLADE ROW ROTATING AT 20222.0 RPM.

STREAN-LINE	<b>₩</b> 6	i m	4	w	φ	~	•	Φ	10	11	15	13	7,7	15	<b>1</b> 6	17	27	5° <del>1</del>	50	77
SPEEDS	787.3	841.0	870.2	900.9	931.9	964.3	4.866	1034.3	1072.4	1112.4	1154.2	1197.5	1242.5	1289.2	1338.0	1369.0	1415.6	1442.8	1470.9	1500.0
BLADE Inlet	721.5	786.8	817.9	852.5	4.588	928.0	968.0	1009.4	1051.9	1095.6	1140.5	1186.8	1234.3	1283.3	1334.0	1386.5	1413.7	1441.6	1470.3	1500.0
DELTA P UPON Q	.1637	.2079	. 2229	. 2112	.1851	. 1588	. 1346	• 1096	. 0877	.0687	.0511	. 0352	.0219	+ 0121	. 9073	. 0063	.0112	. 0154	. 0207	• 0263
OIF-US FACTOR	000000000000000000000000000000000000000	00000	0.0000	00 00 *0	0.0000	00000	000000	000000	000000	0000.0	000000	0.0000	0.0300	0.0000	0.0000	000000	0 00000	000000	0.0000	000000
DE HALL NUMBER	1,003	.967	• 956	• 956	. 360	• 963	• 965	• 369	. 971	.974	.976	.977	.977	•975	.970	.963	• 958	• 953	946*	940
LOSS	.0329	****	25+0	• 0+96	1460.	• 0600	.0658	.0724	.0803	.0895	. 1006	.1136	. 1292	. 1479	.1704	.1991	.2157	.2338	.2534	.2740
HACH NO.S OUTLET	6476	6213	.6185	. 6252	6429	• 6450	.6591	. 6753	. 6950	.7182	.7437	. 7704	.7970	. 8226	. 6460	. 6658	. 67.39	6099	. 6870	. 6926
RELATIVE INLET	.6508	0.000	.6537	• 6099	. 6678	.6764	.6860	• 7028	.7199	.7447	.7651	. 7922	. 8197	. 8479	. 8765	9406	.9186	.9323	.9461	9600
VELOCITIES	727.902	705-035	704,580	724.634	727.587	742.591	159.924	750.941	806.204	935.506	\$67.724	301.534	935.356	969.730	1001.992	1631.250	1044.358	1056.538	1368.832	1079.409
RELATIVE INLET	725, 335	725.936	736.847	747.473	756.096	770.918	767-101	605.253	823.674	858-027	683.283	922. 865	958.203	994.930	1032-611	1070.777	1.369.847	1103.058	1128.575	1165.610
Asc. ES outlet	19 M 9 M	2,004	-2.923	-7. 615	-12. +31	-16.955	-21.375	-25.652	-29.707	-33. 474	-36,949	-40-172	-+1.205	-46.076	6.797	-51, 332	-52.657	-54. Bits	-55.253	-56.542
RELATIVE GAS OPT.IN. INLET	-X-51		-11.136	(の) 日本の			_	-27.678	-31.200		-37.651		V44.64	**6.216	10010			0.00 m	076 - 45-	
STREAM -LINE	***	N M	. 4	· WA	•		•	•	16	#	2	<b>3</b>	4	\$	3	1	<b>.</b>	5	2	Z

### DALMALL PLRFO-MANGE PARAMITURS

STREAM	Statiou-fo-statiou-page Pagesur, Ollia 1 1587 Patto On 1 HFF	0-5745104 02174 T 04 T	を表現を行う。 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 の。 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 のでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ののでは、 ので	PRISSUAL PRISSUAL PRISSUAL	STATION-S OLLIA I ON I	IME.I-10-STATION-PARAM.TERS PRISSON. OLLTA I ISENTROPIC RATIO ON I EFFICIENCY	PRESSURE RATIO DELLA TON T	STATION-TU-STATION 1.0495 1.0199	INLET-TD-STATION 1.9659 2449	TION
**	1.2352	.9677	5.4.4.	1060.2	.2321	. 9897	* 25.40		n 0 0 •	
N	11-2-1	0.00.	6184.	2.0703	-2347	• 9855				
**	1.2337	M+1.70.	. 4315	2.06-4	.2376	E-986.				
<b>.</b>	1.1739	42-E.	P.49.4	2.0550	.2335	9396.				
₩.	1.1455	90-5.	. 3433	2.0402	.232-	.9763				
	1.1222	. 2325	. 3043	2.0303	.2310	.9711				
~	1.1017	£629*	. 3325	2.0223	+231+	6496.				
•	£ - G 2 - 3	6.24.	0686	2.0139	.2311	. 4576				
ø	1.0543	* 120*	. #1.+×	2.002-	.2311	06%6*				
70	1.0555	9/10.	. 5751	1.5912	.2315	. 9357				
77	1.0442	1514.	.6222	1.9803	• 2325	. 9263				
23	1.0330	.6129	.7.335	1.9045	.23.3	.9225				
17	1.6233	. 6111	20044	1.9553	.2367	6269*				
1	1.0149	6404.	- + 27.5	1.940.	.2394	. 6730				
15	£ 400 - \$	.3095	. 2334	1.93.	.2444	. 5463				
91	1.00-1	*710*	• 129•	1.3233	.255t	.6191				
11	1.0072	* 3 T.32	. 1555	1.4100	.2003	.7846				
3	1.0213	.3126	. \$15ª	2.4133	.2659	.7556				
£ 7	1.6134	.9125	1242.	1116.1	.2720	.7451				
2	1.625+	91200	. 3-1.5	10000	.2531	.7237				
ಪ	1. 6352	.3255	. 3 43.3	1-06-1	,2551	. 7015				
			•			STATION 17				
-	•			-						
			;		. Se 18 3. 6	GENERAL FLON PARAMETERS	#LT.RS			
20	GAATES	***			T. Chill Am Sept. 7		STATE STATES AND	700 10 10177	STORE STRATE BOOK	TAICT

LOCA	SA STUS	 ***	T 1 0 0		TA HOPER	&TUPES	PRES	SURES	HOAL	M4IRL	SLOPL	₹40.0F	STATIC	INCIDENCE
1104		4925c Jie		Thicken of La	TOTAL	STATIC	TOTAL	STATIC	4Uत्रड हे.र	AVGL	ANGLE	CJRVTRE.	DENSITY	DEVIATION
*4	4.553.	1157, 034	123.214		3-6-6	523.1	3105.35	1519. +3	1.9270	÷1.908	32.12-	120.90	.0574	0.000
•	21414	15.42. 5.56	752. 123		540.40	531.7	315 3, 05	1040.00	1.0114	51.435	30.035	-22.16	.0581	0.000
<b>*</b>	4.8543	1114.037	72.5.01.		6.4.6	535.6	3133,91	1095,61	. 95 15	43.53c	20.05	22.03	• 0592	0.000
*	サルスカッカ	16 39. 452	732+0+4		639.5	536.9	3125.58	1710.93	. 4055	+3 . 255	22.103	-23.38	.0598	0.000
<b>S</b>	5.1741	1011-3-3	147. 743	7 32 . * 54	639.2	5-1.9	3112.25	1745.37	. 94.63	+7 - 125	23.152	-12.77	+000.	0.000
J	7 - 35 - 7	1351.543	135+251		6.33. J	1.653	1390.99	1775.21	. 3279	+5 + 987	20 .7 69	-20.00	.0611	0.000
~	5.5335	19-2- 320	7450 + 31		6.55.7	5.0.3	3930.43	1304.99	. 96 84	42.048	16.471	-42.36	.0617	00000
•	2.57.6	1623, 159	735.175		036.5	351.3	3383.20	1931, 67	.6699	*** 631	16,298	-125.53	* 0623	0000
<b>#</b>	5.9373	1836. 322	735.003		630.5	550.3	33-0-63	1055.25	. 57 23	45.074	14.272	363.41	.0628	0.000
<b>4</b>	6-1-3-	44.4° 4.50	732-747		634.8	257.3	3023.53	1373,62	. 6553	42.219	12.430	123.77	.0632	00000
77	6.3634	973.233	725, +33		639.3	20.0.5	3012.63	1599.93	. 53 89	+1.495	19.713	77.12	.0636	00000
<b>24</b>	6.3473	\$27.324	723 4+		5.500	4.80%	2 395.00	1,421,03	. 6227	4d • 915	8.102	55.27	• 0639	0000
2	6.63.5	301.722	712.135		041.5	567.6	2374.63	1341.35	• 6006	41.433	7.560	43.50	.0641	00000
**	7.2627	425° 414	705, 735		0.3.1	571.3	2岁2,43	1361.05	.7932	+0.252	6.154	37.57	.0643	00000
5	7.3375	926. 534	64 215		18 + D	570.5	23.2.27	1460.68	• 77 37	642+#*	4.812	35,17	• 0644	00000
#	7.642.	4-32-5-6	E00. 331		600 B.A.	552.1	2425+18	2301+24	.7572	+3 0 574	3.540	39.14	. 0645	0.00
44	7.6033	651.3-5	541. elt.		053.5	548.3	2 -1.4-13	2324.03	.74.03	+1 = 346	2.334	49.63	. 0645	0.000
#	6.6331	674, 31.7	653.232		656.5	543.0	2910.17	2330,55	*7327	+1.9+7	1.742	61.07	• 0644	00000
**	4.1835	251, 155	11* - 150		660.1	547.5	2935.72	2050.35	.72+1	42.704	1.157	64.25	.0644	000.0
2	6.5333	470.402	\$22.352		00000	6.2P9	2962.85	2ubj. 22	.7146	+3.021	.575	146,30	.0643	000 0
Z	6.5003	0 10.716	604.050		665.1	607.3	2537.64	2001.38	.76+1	+++703	1000	0.00	. 0642	000.0

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GUNLARL FLOM PARAMETLES

PA JAMETERS
FLOM
GENERAL

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400	RASIUS	316.02FA	2 C I T 1	TANGENTES	TEMPLE FOTAL	STATIC	PRESS TOTAL	UR.S STATIC	HACH	H+IRL Angle	SLOPE ANGLE	RAD. OF CURVIRE.	STATIC DENSITY	INCIDENCE Deviation	
**	1526-9	1015.726	744 . VV		0.0.0	542.5	3063.20	1725.98	. 95 13	33.354	26.589	-7.39	.0597	0.00.0	
	5.0355	1079.570	963. 323		6.0.4	5-3.4	3967,21	1736.92	. 3451	33.142	25.639	-6.31	6650*	000 • 0	
*	5.2004	1656.532	\$92.714	\$74.523	639.9	5.6.3	3075.91	1769.50	. 9260	32,673	23.180	-10.17	.0608	000 0	
	¥ . 3.22.3	1847.351	45 973		034.5	5.5.5	3072-14	1791.29	. 9129	32.427	21.057	-12.11	.0613	0.00	
<b>4</b>	#654 · G	1613, 339	573.055		033.2	550.3	3055.54	1314.60	\$660.	32.147	20.02	-15.48	.0618	000.0	
•	5.6035	*52-5101	463.277		038.9	5,2,0	3053.11	1.838.57	.6849	31,796	18.360	-21.65	• 11624	00000	
_	5.7573	10.24. 3.3	\$27,35-		036.7	7.456	3051.00	1361.52	. 47 88	31,379	16,599	-34.97	• 10629	0.000	
•	S-2527	9 12. 513	650.235		535.6	556.6	33-1.23	1362,40	. 1571	30.920	15.069	-63.83	• 0634	0.000	
	6.1251	977.347	G15.514		530.5	259.0	3023.74	1900.99	. 84+0	39.462	13.478	-120.67	.0638	0.00	
•	6.3173	955.150	\$35.577		636.6	501.J	3010.92	1317.74	.6314	30 - 057	11.931	-174.11	.0641	0.000	
**	6.513.	932-710	427 . 560		639.3	503.6	3002.95	1933.38	. 5185	23,722	10.440	-140.65	. 1643	0.00	
Ņ	€121.9	920.056	c15. +35		5.0.9	500.7	2957.02	1.540 BS	6500	23.466	9.020	-92.60	• 0645	0000	
"	W-44-0	926.512	484. 15×		041.5	570.0	2971.31	1304.85	.7920	23.269	7.000	-65.22	• 0546	0.000	
	7.1747	912+116	753.243		6-3.1	573.9	2953.31	1301.07	.7770	29.195	6.42+	-51.79	• 4648	000.0	
•	7.4153	6 10-5/0	7.52.503		645.5	578-5	2935.63	2306.26	.7509	23.213	5.233	-42.54-	. 0648	000.0	
	7.05+1	6×1.29C	757,587		643.8	254.1	2915-31	2020.76	.7441	23.338	4.087	-44.67	6490 •	000.0	
	7, 3321	600.735	752.040		653,5	531.0	290++9+	2342.60	.7276	23.791	7.964	-41.5+	* 0 6 4 8	000.0	
**	6.6655	600-445	7 577		656.6	595.0	249 1. 83	2053.50	•7199	\$3.079	2,277	-53.76	.0647	0.00	
g)	4.2634	603+336	733-157		1000	2.666	2045.21	2065. 41	.7116	30.450	1.002	-70.41	9490.	000 • 3	
o.	6 3 3 3 2 2	8-6-5-8	725.373		00.00	504.3	2843.04	2070.37	.7028	30.914	. 453	-124,32	• 0645	0.000	
<u>-1</u>	6. ¥ GGG	636.145	72:32		1.990	609.6	2883.5+	2092-35	.6928	31 + +71	000.3	00+0	• 0644	0.00	

				STATION 1	9 IS AT TH	E EXIT OF	A BLADE ROM	ROTATING	IG AT	0.0 RPH	•			
STREAN -LINE	OPT-IN- INCET	-	MGLES OUTLET	RELATIVE Inlet	VELOCITIES OUTLET	RELATIVE INLET	E MACH NO.S OUTLET	LOSS COEFF	DE HALL NUMBER	JIFFUS FACTOR	DELTA P	BLADE	SPEEDS OUTLET	STREAM -LINE
wi	er W			1169-595	1085.726	1.0164	.9513	.0489	***	.00	• 0589	•	•	+
eu i	16 I			1140.941	1079.578	•	1946	.0470	946.	90	. 0573	•		ત્ય
** 4				229*1211	1060.532	3885	9250	.0416	976*	50.	.0614	•	٠	M .
<b>.</b>				1096-521	1833.505	3619	8991	.0335	770		0600	• •		t K
*	3			1879.563	1419.234	1946	6485	.0279	***	8	. 0727			, o
•	**			1063.459	1304.34X	.9300	.6708	.0.23	\$40.	.00	.0751	•	•	~
•	2			1046.845	991.063	.9131	. 6571	.0172	196.	900	. 0756	•	٠	•
•	4 6 9 J		704.0	2 8 3 Us Z 3 US	740-176	. 0 % D .		. 0129	00 00 12 10 13 10 14 10		97.20	•	•	σ <b>,</b>
13	e e		9.722	996-115	352.718	. 5635	+ 6138	.0078	955		.0703		•	1
() 10	M.	39.213 2	59,462	982.470	340-056	. 8473	6 £ 9 8 *	• 0069	156.	0	• 0675	0.0	0	27
P)			9.249	966.775	326.612	. 8310	•7920	.0067	• 958	8	. 0652	٠	•	13
4;	91		9,135	950.767	912-116	. 6142	.7770	• 0068	959	9	• 0640	٠		41
n d	9 #		7. 7. 7. 7. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	754.601	0.00	3767.	609/	9 0	966	96	• 0641	•	•	£ ;
::	P 64		7.200	57. 6 - 5 X B	367.428 866.798	\$ 75 L	1247	<b>ə</b> ç	000	3 6	, UD 5 / C	•	•	97
			0.079	A40.110	A60-445	• •	7199	9 C	100.	3 5				<b>à</b> 5
3	3		4.450	892-053	653,936	7670	.7118	.0128	136		9665	• •	9 0	9 5
2	2		416.0	883.696	846.648	۰,	.7026	9176	956	90	. 0621			200
22	M.		2.474	673, 102	838-195		.6928	.0165	960	3	. 0576		0	ಸ
67					CVERALL	ALL PERFORMA	MANCE PARAMETERS	ETERS						
STAEAN	STATION-TO-STATION	0-STATE	OM-PARA	TERS	INLET-10-51	ATE	ON-PARAMETERS	MEAN PI	RAMETERS		7	ATION IN	_	LATION
LINE	PRESSURE	DELTA	TSE			4	ENTROPIC	PRESSU	RE RATIO		<b>366.</b>		1.95	9
	RATIO	*	EFF			ON T EFF	TCIENCY	DELTA	DELTA T ON T	•	0000		200	2649
•	49764	000		- 13	2.6310	2351	. 9541	•	• 101				•	•
	.9776	6.00		-	2-0297	.2347	9566							
**	. 9866	0.000		- 60	2,0243	.2336	6956							
#1	.9826	0.000			2.0198	.2330	* 9544							
	9880	# 0 · 0		е 1	2,6155	.2324	• 9536							
Þ Þ;	VE 0.00	900			2,0068	2316	.9564							
•	.9928	6.600			1.9995	.2311	8346							
• (	**************************************	900		•	1.9919	.2311	.9411							
	1966				V. 444.4	2315	6328							
2	+266	000		- 23	1.964	2343	9116							
3	. 9976	0.000		-	1.9535	.2367	.6903							
4	. 2976	0.000			1.9417	.2399	9698			-				
2 :	6.455°				7.929.1	*****	3448							
12	8958			. 41	6505	2590	7.806							
	. 9965	0.000		0000	1.9066	.2659								
2:	. 996	0000		-	1.9835	.2726	740							
3 %	1866			-	1.9961	.2801	•7183 -6957							
ł I		, ! !				! .	1							

### STATION 20

	ABSO_UTE	j.	ekidri. Tang	ENTL.	TEMPER TOTAL	TEMPERATURES OTAL STATIC	PRE TOTAL	SSURES	MACH C NUMBER	M4IRL R A4GLE	SLOPE Angle	RAD. OF CURVTRE.	STATIC	INCIDENCE
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### OVERALL PERFORMANCE PARAMETERS

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~	+9772	0.000.0	0.000	1.9555	.2347	.9263			
14	¥ 950 ¥	99864	6.0040	1.9852	.2336	.9258			
•	. 9833	3.3400	6.0000	1.9356	.2333	.9266			
ĸ	. 9853	0.0000	\$.000G	1.9659	. 2324	*9316			
•	. 9872	0.000.0	6.4560	1.3655	.2315	.9332			
~	. 9893	2.9000	0.0000	1.90.5	+231+	.9343			
•	. 9315	3.0000	C. 1663	1.9625	.2311	.9342			
•	6966.	3.0000	6.0000	1.9796	.2311	• 9320			
91	. 9957	3.4000	0.000	1.9751	.2315	. 9265			
77	+368*	0.3050	0.0100	1.9651	.2326	. 9171			
ä	÷266 •	4.0000	4.9333	1,9593	.2345	.9038			
7	. 937b	8.0000	0.200	1.9-33	.2307	.6866			
**	. 9976	0.0000	6.5 303	1.9370	.2339	. 8661			
25	. 9375	3.3560	0.0000	1.9249	. 2 - + +	. 6413			
16	. 3373	3.0000	0.0000	1.913%	.2508	.8117			
7.7	- 9353	2.0000	0.000	1.9637	. 2600	. 7764			
21	. 435.	0.9030	6.4665	1.8997	.2659	*1564			
67	9366	0606.0	6.0000	1.0833	,2720	.7351			
2	.9355	3-9600	6.000	1.6916	,2501	.7128			
ม	. 3351	3.00.00	<b>9.</b> 0000	1.4365	.2081	6689			
•-		-				STATION 21			

LOCA	SOTOFA	4 5 L	OCITI HERIDAL	E S TANGENTL.	TEMPERA TOTAL	ATURES STATIC	PRESS TOTAL	PRESSUKLS TOTAL STATIC	MACH	W1IRL Angle	SLOPE Angle	RAD.OF CURVTRE.	STATIC	INCIDEACE Deviation
-4	5.3755	1020-119	370.623	241.364	3,040	557.3	23+5+63	1909.42	.8647	13.934	16.771	-7.32	. 0609	00000
•	5.4170	996, 670	907.351	240.791	640.4	557.7	2951,00	1516.33	• 86 14	13,978	14.348	-6.21	.0611	0.000
*	50.5.353	985. 371	955.921	237.573	639.9	579.0	2953,63	1343.69	. 65 10	13,943	17,183	+0.0+	.0619	00000
•	5.0254	976, 320	943.605	235.287	639.5	6.655	236**95	1360.84	. 64 33	13,910	16.394	-9.00	. 0623	00000
•	5.7312	970.221	961.95-	232,449	639,2	500.9	2971.58	1079.93	0686.	13.862	15.501	-10.22	.0629	0.000
•	F. 851's	961.702	934 · 664	228.319	638.9	502.0	297 3. 13	1900.50	. 8279	13,765	14.521	-10.93	• 11634	0.000
•	9.0450	955-656	925+639	22459	638.7	503.2	2936 . 09	1921.76	. 81.92	13.628	13.470	-11.80	. 064 B	00000
<b>~</b>	6.5327	943.055	917 . 124	219.071	633.6	204.0	2331,25	1343,05	. 8100	13,470	12,358	-12.88	3 <b>06</b> 40	0.00
•	6.2917	932-921	907.717	224.352	636.5	556.1	2993.41	1363.60	. 80 01	13,323	11,201	-14.23	• 0651	000.0
=	6.4623	921.752	697.320	210.460	634.9	568.1	2991.29	1983.52	. 78 32	13,224	10.012	~15.98	.0655	008.0
#	S. 6 63 C	909.736	なるがのはない	247. +93	639.3	570.4	2984.00	2001.80	17773	13,183	8.812	-18.31	.0658	0.000
23	6.8357	697.147	673.475	204,727	54049	573.2	2372.29	2018.41	.7647	13,131	7.622	-21.45	10650	00000
갩	7,0332	小大 マッテの母	463.675	202,357	041.5	576.4	2950.88	2033+27	.7515	13,231	0.459	-25.06	.0662	0.000
<b>4</b>	7.25.0	671.1.9	647 . 643	200.169	643.1	550.0	2939.03	2046.43	.7332	13.284	5.329	-31.24	• 0662	0.004
ij	7.5463	658.835	<b>#35.668</b>	194,364	645.5	254.1	2320.37	2058.03	.7252	13,356	4.233	-38.87	.0661	000.0
=	7,7133	847.839	624.533	197.423	646.6	589.0	2962,34	2066.32	.7129	13.465	3.159	64.03-	. 0659	000.0
<b>~</b>	7.4677	633.242	215.510	137.916	653.5	694.9	2666.28	2075.92	.7022	13.634	2.097	-73.69	.0655	00000
=	84654	636-157	612.207	193.691	656.6	9.965	2573,24	2080-42	. 69 75	13.7.6	1.571	-95.30	.0652	0.000
\$	B.2284	833°473	603, 123	149,971	560.1	602.3	2672.25	2063.64	. 6931	13.682	1.050	-139,21	6+90 •	00000
2	6.3620	830.734	465.975	201, 549	664.2	506.5	2864.62	2026-64	• 6 8 3 4	14.040	.528	-265,49	• 0645	B. 000
컶	6.9003	627.653	\$65.582	243, 391	658.1	611.1	2355.77	2083, 32	46.80	14,216	0.000	0.00	.0541	0.000

				STATTON 2	21 IS AT THE	EXIT OF	A BLADE ROM	ROTATING	IG AT	0.0 RPM				
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<b>(4</b> )	,	-	13.973	-	496.870	. 5978	4664	.1373	. 965	8	. 50.4 10.4 10.4 10.4 10.4 10.4 10.4 10.4 1	٠	•	N +
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9			H	343.734	\$51.72	• 8496	. 8279	. 6368	.976	63	. 0145		•	•
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•	4.381.	912-209		99. 469	102.782	638.5	59.5	2975	1.990	52 .78		1.6	-13.53	. 065	
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<u>ب</u>	4000 O	676.9%		671.345	400.405	2.04.9	576	2964	2050	22 .74	'n	6.247	-20.10	• 1066	0
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•	B. 5.5.00	416.261		345.00	97-270	9.959	632	2859*	2116	56 .67	10	1.217	-65.10	065	
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### SVERALL PERFORMANCE PARAMETERS

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STATION—PARAMETERS OELTA T ISANTROPIC ON T EFFICIENCY -2347 .8614 -233 .8650 -233 .8736 -233 .8736 -2319 .8925 -2311 .9140 -2315 .9140 -23
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### STATION 23

RADIUS	NUSOLUTE L	OCITI	i e S Tangente,	ICHPERAT TOTAL	ATURES STATIC	PRESSURES TOTAL STATIO	SURES	HACH	#HIRL Avgle	SLOP É ANGLE	RAD.OF	STATIC DENSITY	THCICENCE DEVIATION
5.6314	835.051	695.051	9.000	ó*3.	573.9	2805.88	1310.20	.7524	3.000	10.903	-7.93	.0624	0.000
5.6663	634.678	894.673	0.000	4.0.0	573.8	2313.49	1319.20	.7522	0.000	10.716	-8.05	. 0627	000.0
5.1787	331. 316	\$9£. 415	0.390	639.9	573.7	2553.71	1944.05	.75 99	3.006	10.159	-8-43	.0636	000.0
5.6573	649.+38	\$64.458	0.300	639.5	573.7	2470.91	1962.28	.7579	0.000	9.752	-8.79	,0642	0.000
5+355+	646. 339	465 + 939	0.000	639.2	573.7	2893.98	1982,25	. 75 56	3.930	9.262	-9.27	, 3648	00000
6,0606	833,363	\$03.653	0000	638.9	573.9	2317.76	2303,74	.7529	0.000	8.70B	+6.6-	. 8655	0.000
6.1813	679,755	473.756	007.0	633.7	574.3	2933,68	2025.93	.7492	00000	8.075	-10.85	• 1662	000.0
6.3140	E74.222	374. 222	200°0	638.6	574.9	2357.44	2048.04	2442	0 * 0 0 0	7.403	12.07	. 0568	00000
6.4577	866,715	460.715	9.000	<b>638.5</b>	576.0	2964.62	2069.42	.7363	0.000	D.704	-13.63	. 9674	0.00
6.6121	656.731	162. 131	0.000	638.8	577.7	2971.39	2083.02	.7275	000 * 0	5.990	-15.58	.0678	00000
6.7773	8+4-837	4-4-637	0.300	639.3	579.9	2900.bB	2106.33	.7160	00000	5.291	-17.37	.0682	00000
6.9534	8 51. 7 38	631.733	0.000	643.2	502.6	2350.48	2125.38	•7032	0 • 200	4.593	-20,95	• 0684	0.00
7.1464	516. 445	515. +38	0.000	641.5	565.7	2943,24	2140.60	<b>* 69 02</b>	0,000	3.499	-24.93	.0685	0.000
7.3386	835.206	203.206	0.000	643.1	589.5	2327.51	2153.79	.6770	000 * 0	3,203	-30.92	. 1686	000.0
7.5463	792-237	792.237	0.000	645.5	593.2	2303,09	2184.77	.0638	0.000	2+509	78.04-	• 0684	0.000
7.7583	779.678	773.878	0.000	6.0.5	5.96.3	2668.68	2173.48	.6507	3 • 060	1.830	-58.94	. 1681	0.00
C-0013	76% 239	763, 239	0.000	653.5	604.3	2565.30	2180.06	.6386	0.00.0	1.188	-93.53	. 3677	0.00
612148	754.333	764.903	0.600	656.6	607.9	2858.74	2182, 66	.6331	000+0	.878	-127.20	.0673	0.00
5.245.8	760.938	763.894	0.000	660.1	611.9	2649.16	2164.79	.6278	3.000	.575	-197.06	.0670	0.00
6.3712	757.189	757.152	0.000	66** 0	616.2	2839,00	2186.47	.6224	0.000	.282	-408.75	• 0565	0.00
6.5300	793, 173	753.173	0.400	1.690	550.9	2627,61	2167,73	.6166	00000	0.000	00.0	. 0661	0.00

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91		÷	c; C;	823.7	779.575	1969.	•	60	256.	.036	.3877	•	0 * 5	16
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STATION 25

•		-			3	מינטאר ברנ	GENIGAL FLOW PARAMETIKS	ŔS						
L 05A T 20%	REDING.	A T POR SE	3 C L T )	E S S ATE.	TEMPERAT TOTAL	ATURES 5T4T.LC	PKESS	STATES	MACH SUMBER	M4 I 3L ANGE É	SLOPe ANGLE	RAD.OF CJRVTRE.	STATIC DEMSITY	CHCIDENCE
#1			512.723	3.3.	6.43.6	542.5	505	2050.10	.6853	. J. d	5.537	100	690	0.00
N: •		. 6	614.433	19 6 19 6 19 6	* 00 00 00 00 00 00 00 00 00 00 00 00 00	5.65.2	619	2350, 31	• • • • 7 0	3	5.475	넉 *	990	2000
• 4			3 M C - 4 M M	10 mil	0.00	54.7.7		2045-63	F 00 0	9 6	2 10 10	, M		
, ex		-	553.532	9	639.2	583.2	333.	2034.03	.0933	3	10F.	-	190	000-0
•		21.4	621.013	4.20	6.650	552.7	7	2113, 38	.69	.00	4.736	~	-	0.000
<b>~</b> 1		م وس	622,300	9.0	P 4000	552.4	43.	2126.15	* 0.9.74	70.	4.407	_	990	000
•	4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.		117.77. 117.77.		0 - 0 - 0 0 - 0 - 0 0 - 0 - 0 0 - 0 - 0 0 - 0 -	5.000	0.307.04.5 0.904.50	2157.03	*****	<b>3</b> 3	# • A = A = A = A = A = A = A = A = A = A	115.44	7690	00000
2	C. 0 414	-	311.742	9	636.6	100	37.1.	2170.29	.6853	00.	3.580		•	0.000
77	1219-0	33, 3	663.030	37.0	639.3	545.7	90.2	2152+3+	+ 47 72	90	3.232	•	690	0.000
2	10001	43.	793. 139	(1) v	2***0	# 1. P. S.	400	2192.97	.00.75	9	2.872		~ /	0000
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2 %	7.5713	3 4	104 - 4-5V		7 C	426.0	200	2215, 35	5300	3 0	1.692		06.4	
2	7.7823	5 4 5	751.628	3. 10	ç	601.9	3	2219.64	. 6253	0	1.275	77.4	- ^	000.0
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i zi	4.9663	23.6	72 5. 211	9.7.	1.830	623.0	2327.61	2224.43	6555	9,000	0.000	0.0	. 0669	00000
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LOCA TION	eaotus	4 ± 1.	3 C I I 1	TAMSTATES	TEMPERATU	ATURES	PRESS FOTAL	SSURES	MACH	MAIRL	SLOPE ANULE	RAD. OF	STATIC	INCIDENCE
wi		~~~~	Š		9.00	553.2	40 3 • C	2097.07	. 65 48	9	1.323	-	. 0567	_
•	.\$₹	17.5.	-		3.5.4	514.4	31.3.	2133.22	10	.03	1,372	•	€9€9	•
<b>-</b>	100 T	£0 - 25	÷.		6.39	557.0	850	2107.54	. 67 14	60.	1.0465		+ 0673	•
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• •	i i	40 . W. W	362. ±37.		0 4 0 4 0 4	2.25.4	\$ 2.	2134.72	1060	90	1 .062		9 6	- C
* 2	6	75.57	423,519		618.6	5.52.7		2154.36	69.37	90	1.591		699	•
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#### 4. ROTOR GEOMETRY

Rotor airfoils were defined on all streamsurfaces and stacked close to the centroids of the manufacturing sections on cartesian planes. The manufacturing sections were determined by mathematically passing a spline through common points on all streamsurface sections and determining the intersections of these splines with cartesian planes normal to the stacking axis. The computer program used to accomplish this was that described in Reference 7, previously cited. However, the interpolation technique and calculation of mechanical properties were taken from Reference 9 which discusses this subject more fully. The computer printout on the following pages presents detailed data on all streamsurface and manufacturing sections. Except for the normalized data defining the streamsurface blade sections, all dimensions are in inches. On the first few pages appear sundry constants and a definition of the 21 streamsurfaces. The streamsurfaces are defined at eight axial locations which coincide with eight of the computing stations used for the aerodynamic design calculations. The origin for the axial locations of the stations is the same as was used for the aerodynamic analyses. The input data printout is completed with a table defining the geometry of each section. Next are shown details of the 21 streamsurface sections. Only the "normalized" data have been reproduced; the equivalent dimensional data would be derived by scaling the nondimensional quantities by the meridional chord of the section. Finally, details of 13 manufacturing sections through the blade are shown. These plane sections, perpendicular to the stack axis, are spaced 0.50 inch apart, and extend slightly beyond the blade in both directions. The "Z" coordinate is measured along the stack axis from the machine axis. The origin for the section coordinates is the stack axis. The "X" direction is parallel to the machine axis, and "X" increases in the direction of flow. The "Y" direction is perpendicular to the "X" direction, and the "Y" coordinate decreases in the direction of rotation. "XS" and "YS" define the suction surface of the section, and "XP" and "YP" define the pressure surface. "XSEMI" and YSEMI" define the leading edge radius. The trailing edge is a straight line joining the pressure and suction surfaces. The manufacturing coordinates shown in this report have not been corrected for blade untwist and represent the blade as it should exist when running at design speed. The actual machining was accomplished with these coordinates rotated about the stacking axis an amount equal and opposite to the predicted angle of untwist as described in Section III.12. No corrections were made for any changes in camber-line shape. Figure 25 shows superimposed plots of developed streamsurface sections. Figure 26 shows a similar view of the manufacturing sections. The larger change of section visible in Figure 26 is due to extrapolation of the airfoil beneath the hub ramp.

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111	· 25435	ī	22.673	• : • 653		.29888	* .1478	. 27783	ĭ	
<b>J</b>	4 MO 347	i	-25-378	. 34963		.X 1132	1529	. 28991	2	
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Ž.	4 X2469	i	-23.644	+ 05207		. 3 3522	1626	. 3141	ĭ	
*	. 33653	i	23.234	* C5212		. \$4727	1673	. 32634	ř	
e i	16895	i	-22.549	27 750		. 35523	17.73	433854	ŧ	
N I	27.136	ï	614-12-			37126	1767	. 55076	ĭ	
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0,	我們的學者。	ř	225 - SEC.	* 46445		.53103	2153	. 48562	ï	
7.4	* 500 UK	i	180.458	- 05166			- ,2181	. 49786	ĭ	
3	52729	ï	-17. 674	4 061.83		22449	6, 22-	. 51009	ï	
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23	. 63716	i	19.69	2000 BAD 8		VE.	2459	. 63215	ï	
75	. 64916	i	-9.253	4 000000		40	2482	. 64442	ï	
	* 66116	ř	24.2.6-	のはないので		₩.	-2534	. 65672	i	
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24	.757LA	i	-3.297	. 05068		-	2644	. 75572	ï	
	. 76915	ï	19402-	19670		.77023	2655	.76814	i	
	· 76119	ì	214-1-	- 04842		.7 61.81	- ,2666	.78057	ï	
<b>6</b> 5	. 79129	ř	-	9874D •		•	•	• 79299	ŧ	
9	· #05/0#	i		. 04562		.60575		. 80521	ï	
	1111	1062	3	1044G+		•	٠	. 61941	i	
2 4	. 64179		261.2	44240		*****	• •	10250	i	
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		N ( ) ( ) ( )	P # 4 P P		21000	44.3000	• 77 004	24/62*
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Ž,	. 93356	27733	11,667		.93113	26412	. 93659	29054
77	• 94665	- 27 455	12.792		.94391	26251	94938	28650
<b>9</b>	* 95944	** 27152	13.916		.95675	26367	. 96212	- 28237
79	. 97 222	2000年1	15. 338		<b>+9696</b>	25860	97481	27784
C: 40	. 98511	1. 化色色细胞	15.157		.98259	- 25629	498744	27384
81	. 99783	1 80 0 Z *-	17.272		.9956	- 25373	4.10000	-26788
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## STREAMSURFACE GEOMETRY ON STREAM INE NUMBER 2

### FOLLOWING REFER TO ABLADE HERDIONAL CHORD OF UNITY  ###################################		AX IS =-16.497	SURFACE COORDINATE DATA  YS  YS  YS  YS  YS  YS  YS  YS  YS  Y
(BLADE INLET ANGLE.) (BLADE OUTLET ANGLE.) (BLADE LEADING EDGE RAI (BLADE HAXIMUM THICKNE: (BLADE TRAILING EDGE HAXIMUM THICKNE: (LOCATION OF HAXIMUM THICKNE: (LOCATION OF HAXIMUM THICKNE: (HERIDIONAL CHORD OF SI	JE TO LEADING EDGE	CENTRGID PRINCIPAL AXIS TO "X" AREA ABOUT CENTROID (AT-16.490 WITH "Y" AXI	0.9)100-35.362 00614 -0.1920-35.162 01021 -0.1920-34.926 01021 -0.12764-34.926 01021 -0.1566-34.413 01635 -0.1566-34.413 01635 -0.1566-34.928 01637 -0.15644-33.829 01637 -0.1516-33.184 02234 -0.19356-32.469 012823 -0.19356-32.469 012823 -0.19765-32.186 02993
=-35,332 = 16,145 = 0.392 = 0.392 = 0.3721 = 0.3721 = 3,3313 = 3,3313 = 3,3313	= 1.9335 E =-16.932 =-51.527 = .34555 CENTROID RELATIVE	= .51374 =23664 OF AREA A = .009276 =09378 ND HOMENTS	R X X X 200 200 200 200 200 200 200 200 2
BETA1 ==35 BETA2 = 16 YZERO = 1 YONE = 2 COR? = 2 COR? = 3 COR? = 3 COR? = 445 COR. = 44	BLADE CHORD STÄGGER ANGL CAMBER ANGLE SECTION AREA LOCATION OF	XBAR YBAR SECOND MOHENIS IX IX IX IX IX ANGLE OF INCLI PRINCIPAL SECO	NUM NUM NUM 2 2 4 4 6 6 6 6 111 121 121

100		C	* +	CHECKO		ATE OATA	
NUMBER	: <b>&gt;-</b> : ;	ANGLET	HICKNESS	XS	YS XP		4. 4.
*	17469 11	325-31.2	. n33£1	0339	26960*	. 16600	-
15	8782 12	115-50.8	+33524	19685	3602	. 17879	7
<b>1</b> 6	5334 - 12	691-30.3	• [3693	21028	.11298	. 19161	٦,
<b>:</b>	1637 1	8	. 93657	22365	1,001	34402	
e e	. 23855 15	5033-28-944	. 04154	24859	13217	22.852	- 16994
200	-	28	. 24293	26101	.13518	. 24057	7
21	26313 1	6.73	• 64425	27340	-14405	. 25267	. ⊷
<b>2</b> 5	1:-	4.12-	• 94556	28576	1.4980	• 26419	7
23	-:1	-26.8	. [ 4681	2809	415541	. 27 594	19717
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9.6		Ç O	. 25026	33491	17145	. 51.357	Ņ
, e	155546 13 14872 21		. 05232	5177	4 5 2	33814	,,
62	36396 2	23.2	. 35326	37146	18623	35046	. ~
33	. 2	-22.5	. 5415	36356	18:61	. 36282	14.1
31	30545 2	-21.6	. 05497	39568	9536	. 37 522	2
32	39769 2	-21.1	• :5574	46774		.38764	C)
<b>3</b> .1	2.	-20.4	• 15645	1977		60007	ď,
<b>#</b> (	2198 2	19.6	. 05713	3160		. 41236	~
<b>3</b> 2	33 ~ 2	18.9	• 55768	4347		42464	Ņ
36	446.16 2	18.3	. 5621	12653		. 43693	N C
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0 0	20 20	46.6	10594	1000		CT 24	•
\ <del>(</del> )	49427 2	15.9	.5971	53246		. 48608	2
7	50632 2	- 15.3	. 35994	51427	.23232	4983	N
75	537 2	-16.8	. 2601.3	52609	. *23543	5106	N
Νŧ	345 2	- 14 . 4	. 06023	3791	.2384	. 52293	7
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<b>•</b> !	2- 900	13.1	• 0501.)	24576	2/42	25.50	
* 1	551 - 2	2	• 15994 • 1010	12696	5.47		7,
n o	324		1.7560 •	59713	70200	700	7
, 6	65482 23	3721-11-949	70650		25.83	63871	,
51	62632 2	11.6	. 05865	63282	.2613	621	7
55	63973 2	-11.2	. 95816	64468	26365	633	۳,
53	113 2	-10.7	. 05761	2695	26623	w	~
t t	324 2	-12.3	. 5703	6833	.2687	8	<u>ب</u>
v ,	67534 - 2	6	, 95632	66012	3	67.05	
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20	376 - 3		. F5299	72737	.2799	7234	מונ
6	556 3)	9	. 55293	73877	2818	7329	
61	797 33	2.5.5	. 05095	2045	.2835	4	
29	337 - 31	d2 -4.7	19616	6213	.2051	8	۳,
63	218 - 31	5. 5.	. 548.57	7379	-2869	8	m i
t u	76429 51	,,,	****	70742	700	7057	? •
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POINT	7 W	1 1 1 1	0 W	ATA	SURFACE COO	RDINATE DI	ITA
NUMBER	×	<b>&gt;</b>	ANGLE T	Y ANGLE THICKNESS	XS YS XP	×	ΥÞ
76	. 85937	31129	3.719		.85812291	•	133026
71	. 87196	- 31015	4.833	• 03665	.8704229189	•	8735132841
72	- 98456 -	3.896	5.961		.8827529164	64 . 18637	32628
73	.89715 31752 7.393	3)752	7.393	•	.8951229118 .8991932386	18 . 8991	3 32386
74	- 97906 •	-, 31583	8.226	•	.90753290	51 , 91196	5 32115
75	. 92234	3 1388	9.361	•	.91999289	62 . 9247	3 31814
76	- 76426 •	-+3:167	10.497	•	.93253288	50 .9373	3 31484
77	. 94754	23921	11.632	•	.94506287	17 . 9500	1 31125
7.8	. 96313	- 23649	12.765	•	.95767285	61 . 9626	1 3:737
79	. 97273	29356	13,895	• 31995	.97033283	82 . 9751	2 30318
00	<b>.</b> 98532	23026	15. 322	•	.98305281	80 . 9875	1 29871
4	00700	- 28674	46.446		076 48500.	SE 4 1000	70706 1

## STREAMSURFACE GEOMETRY ON STREAMINE NUMBER 3

CHORD.) Ords.) Etion of Chord.) I of Mean Line.)	RD PROJECTION OF UNIT FURE-ERFECTED SERVER		·	•		E DATA
(BLADE INLET ANGLE.) (BLADE OUTLET ANGLE.) (BLADE LEADING EDGE RADIUS AS A FRACTION OF CHORD.) (BLACE HAXIMUM FHICKNESS AS A FRACTION OF CHORD.) (BLADE TRAILLING EDGE HALF-THICKNESS AS A FRACTION OF CHORD.) (LOCATION OF HAXIMUM THICKNESS AS A FRACTION OF HEAN LINE.) (HRRIDIONAL CHORD OF SECTION.)	HAVING A HERIOTOWAL CHO			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	SIX (SIX	SURFACE COORDINATE DATA
(BLADE INLET ANGLE.) (BLADE OUTLET ANGLE.) (BLADE LEADING EDGE RADIUS AS (BLADE HAXIMUM FHICKNESS AS A (BLADE TRAILING EDGE HALF-THIC (LOCATION OF HAXIMUM THICKNESS (MERIOIONAL CHORO OF SECTION.)	NORMALISED RESULTS - ALL THE FOLLOWING REFER TO ASLADE HAVING A MERIOTONAL CHORD PROJECTION OF UNIT Bus sesses sees the sesses consenses the sesses the se		LOCATION OF CENTROID RELATIVE TO LEAVING EDGE  YBAR = .50532 YBAR = .26926 SECOND MOMENIS OF AREA ABOUT CENTROID	IX = .00337 IY = .00655 IX =	PRINCIPAL SECOND MOMENTS OF AREA ABOUT CENTROID  IPX = .00134 (AT-20.362 MITH 'X' AXIS)  IPY = .00285 (AT-20.382 MITH 'Y' AXIS)	M L I N E D A T A Y ANGLE THICKNESS
н 326.531 н 10.9531 н . 05600 н . 05600 н . 5760	= ALL THE F	10000000000000000000000000000000000000	= .50532 = .26926 OF AREA ABO	# .002337 # .00852 # .00091	MD HOMENTS OF E . 00334	ж ш Т
9ETA1 9ETA2 YZERO T YONE Z CORO	MORMALISED RESULTS	STABER ANGLE CAMBER ANGLE SECTION AREA	LOCATION OF CENTROID KELATIVE TO LEAU  YBAR =26926  YBAR =26926  SECOND HOHENTS OF AREA ABOUT CENTROID	IX IX IXA	PRINCIPAL SECO	POINT

. 13121 -- 0 .2551 . 02552 -- 0 1345 . 03770 -- 1369 . 04989 -- 0 1557 . 05210 -- 0 1557 . 07432 -- 0 1653 . 0863 -- 0 1656 . 13112 -- 0 1656 . 12375 -- 1454 . 14810 -- 12569

.01521 .01251 .01661 -.01078 .01536 -.01259 .01536 -.01259 .01506 -.04275 .016538 -.05145 .01968 -.05145 .11196 -.01646 .12522 -.01679 .13646 -.0336

. 00321 8.91030-38.531 . 01599 -- 11011-38.2 5 . 05255 -- 12011-35.2 5 . 05453 -- 02939-37.556 . 05453 -- 02975-37.256 . 05738 -- 05931-36.868 . 05738 -- 14339-36.868 . 10540 -- 0757-35.75 . 13394 -- 08571-35.35 . 13394 -- 039572-35.30 . 14371 -- 13560-34.505 . 15649 -- 11335-36.197

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SE COORDINATE YS XP	မွာ မြိမ့်မြိမ့်မြိမ့်မြိမ့်မြို့မြိမ့်မြို့လိုလိုလိုလိုလိုလိုလိုလိုလိုလိုလိုလိုလိုလ	45.
S URFACE XS	**************************************	8462
A T A HICKNESS		376
N L I N E. D.	12486-33,781 -12476-33,781 -114697-33,781 -114697-33,987 -11466-33,987 -114686-33,987 -114686-33,987 -114686-33,987 -114686-33,987 -114686-33,987 -114686-33,987 -114686-33,987 -114686-33,987 -114686-33,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987 -114686-39,987	.36679 -1.4
* ×	. 16926 . 227759 . 227759 . 227759 . 227759 . 226737 . 226737 . 226737 . 226737 . 319375 . 319375 . 319375 . 319375 . 556869 . 556869 . 56869 . 77175 . 56869 . 771835 . 771835 . 771835 . 771835 . 771835 . 771835 . 771835 . 771835 . 771835 . 771835	
POINT NUMBER	\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$	69

DATA	ΥΡ	026 38503	318 38399	60738279		893 - 38114	89338114 17337931	89338114 17337931 45037719	89338114 17337931 45037719 72237480	89338114 17337931 45037719 72237460 90837213	89338114 17337931 45037719 72237460 96837213	89338114 17337931 45037719 72237460 96837213 25036919	89338114 17337931 72237719 78837480 98837213 5063696 7563696
COORDINATE D	XS YS XP	.•34899 • 860Z	.34396 .8731	.35374 .8860	0000		.35177 .9117	.35177 .9117 .35202 .9245	.35135 .03117 .35177 .9117 .35202 .9245	.3517 .9117 .35202 .9245 .35209 .9372	.35135 .9309 .35177 .9117 .35202 .9245 .35209 .9372 .35197 .9498	.35135 .0304 .3517 .9117 .35202 .9245 .35209 .9496 .35167 .9626 .35119 .9750	.3517 91173 - 31173 - 33510 93173 - 33510 93728 - 33510 94968 - 35157 96251 - 35157 96756 - 35152 96756 -
SURFACE	X	•86052 -	-87282 -	.88515 -		- c07C9*	- 505000.	. 492995 - . 92241 -	. 64723 . . 98995 . . 98241 .	. 64745	. 50000 . 00000 . 00000 . 00000 . 00000 . 00000		. 64753 55155 . 91995 35177 . 93492 35219 . 94747 352197 . 96019 351197 . 98548 35152
ATA	HICKNESS	. 63601	• 03404	. 03198	10000	COR71+	.02759	• 02759 • 02526 • 02526	• 02759 • 02759 • 02526 • 02283	• 023 0 3 • 025 2 6 • 022 8 3 • 020 3 0	. 02759 . 02759 . 022526 . 02033 . 04768	. 027 59 . 027 59 . 027 59 . 027 58 . 047 68 . 044 68	. 02759 . 02759 . 022826 . 02683 . 01498 . 01495
o w	ANGLE T	410	.619	1.651	2.683	772	3.717	3.717	3.717 4.753 5.783	5.717 4.750 5.783 6.815	3.717 4.753 5.783 6.815 7.844	3.717 4.750 5.783 6.815 7.844 8.871	4.753 5.783 7.883 7.883 8.845 9.894
Z Z Z	X Y ANGLE THICKNESS	36700	36697	35672	- 46.62E	いようつつ	- 35554 - 35554	- 35554 - 35461	. 35555 . 35555 . 35451	- 35561 - 35661 - 35346 - 35246	- 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		91384 - 35554 92348 - 35554 923617 - 353346 94868 - 35215 95129 - 35543 97391 - 35658
L) E	×	• 86039	. 67393	. 88561	. 49823		91984	92345	. 91345 . 9345 . 93617	91184 92345 93617 94868	911384 923453 93537 94558 95129	911384 92345 93517 94868 95129	. 9011001 . 9011001 . 901001 . 901001 . 901000
POINT	NUM BER	7.0	7.1	72	73		74	75	4 2 2 2 2	7824	775 77 78	727 722 733 733 733 733 733 733 733 733	9333435 9334 9334 9334 934 934 934 934 934 934

#### STREAMSURFACE GEOMETRY ON STREAM, INE NUMBER 4

(BLADE DUTET ANGLE.)	(BLADE LEADING EDGE RADIUS AS A FRACTION OF CHORD.) (BLADE MAXIMUM THICKNESS AS A FRACTION OF CHORD.)	(9LADE TRAILING EDGE HALF-THICKNESS AS A FRACTION OF CHORD.) (LOCATION OF HAXIMUM THICKNESS AS A FOACTION OF HEAN LINE.)	(MERIDIONAL CHORD OF SECTION.)
x-49.329	# .07254 # .05400	* .00175	* 3.2970
BETA1 BETA2	YZERO	YONE	CORD

# 1.0751 BLADE CHORD

STAGGER ANGLE #-21,546

15£36. = SECTION AREA

=-45.811

CAMBER ANGLE

LOCATION OF CENTROID RELATIVE TO LEADING EDGE

XBAR = .50351 YBAR = -.25573

SECOND HOMENTS OF AREA ABOUT CENTROLD

DX = .00942 IY = .00236 DXY = -.00395

ANGLE OF INCLINATION OF (OME) PRINCIPAL AXIS TO "X" AXIS =-21.969

PRINCIPAL SECOND HONENTS OF AREA ABOUT CENTROID

(AT-21.989 WITH 'K" AKIS) (AT-21.989 WITH 'Y" AKIS) = ,00033 = ,00277

SONT AGE COUNTING IN THE WAY WE AVE	.01469 .01219 .01019711228 .01751101752 .01276101323 .0175201703 .02456101323 .0175201703 .02456101323 .0175601254 .01756101520 .0554401564 .05619104614 .0554401564 .05619104617 .1053510564 .0556410575 .1212001765 .05564108627 .1212001956 .1314314855 .1469410815 .11945108657	19632 - 14340
K E A E I A E U A I A K AMGLE THICKNESS	. 2027 3 0. 31000-40.029 .00546 .8151+ 01037-39.769 .007546 .92754 02065-39.497 .06938 .93755 04085-39.213 .91132 .05525 04085-38.613 .01324 .0716 05045-38.619 .01515 .07716 05046-38.619 .01515 .10197 08955-37.607 .02074 .11518 08955-37.607 .02255 .12618 08955-37.607 .02255	.1515911726-36.362 -32782
POINT NUMBER	40 m 40 m 6 m 6 m 6 m 6 m 6 m 6 m 6 m 6 m 6 m	12

POINT	MEANLESS DATA	SURFACE	COORDINATE DATA
NUMBER		SX.	XP YP
91	12623-35.665 ."	.172631	.155391
u	- 1 TGAG-18- 0-1	P. P. CESS P.	16741 1
1 5	0 1275-34-785 - 1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	40 - 516614	17946 1
13	7.15230-34.321 . C	-21989 - 1	. 191531
4.5	-, 16067-33, 846 .0	.223581	. 237631
19	15890-33,364 .3	1 4235241	. 21569
23	17697-32.874 .0	2.40881	. 22732 -
7	18490-32, 377	7	- 53836
22	13267-31.671	1- /04/20	52273
23	20029-31.358	*- 28663 - 1	. 28433
4	- 21/16-30-637 ·	1. 1166.20	- 669/2
<b>%</b>	21507-30-396	40 - 971106 401106 - 0	. 2555
S I	: 111.62-52222	2* 1 Q1#2**	* * * * * * * * * * * * * * * * * * * *
` .	- 01608-03-63-665 - 0	20 TODO 04	12572
50	25277-25,113	3.4145	33805 -
H	-24930-27.540	247363 - 22	. 35043 -
11	25558-26.961 . 0	.386182	. 36283
25	25190-25.374 .0	.398512	. 37526 -
<u> </u>	-, 26795-25, 778	•41382 - 12	. 36771
ň	27367-25.200 . 0	20- 212240	. 39980
35	27924-24.631 .0	** 3663 - *Z	. 41193
9	28467-24-979	No I make to	10424
'n	** 256996-21-516	7	****
ID (	23511-22.976	2 - 61624*	
T C	- 5 1013-22-646 - 21662-26-634	79 1 7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	42044
3		25.05.64 25.05.64	. 48475
	-, 31442-20,907 .0	2° - 151150	- £696÷
19	31895-20-417 .	.52927Z	. 50912
3	32335-19.939 .0	.541062	. 52131
45	-, 32765-19,472 . 1	.552853	. 53351
9	33164-19.317 . O	.564633	54571
24	3359.2-18-575	.575413	. 25792
<b>9</b> 0 (	57916 - 33998-18-145	1 15 15 15 15 15 15 15 15 15 15 15 15 15	57014
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4 6	- 15561-15-175 - 0	6.3564	61976
1 10	6-863 - 35-856-15-680 - 8	.64773	. 63227
25	36197-15.362 .0	.659631	. 64479 -
2	36527-15.621	+67151 + a	.65733
9	- 15664-14.256 · C	20 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	- 55989
ž	47147-13-666	50000 P	2000
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9	-, 38222-11, 378	.142523	.73286
29	38455-10.376 .n	8°- 28491°	. 74548 -
63	38664 -9.638 . O	.76612 3	.75813
<b>.</b>	- 1000 - 1000 -	- 167774	.77073
Ç2	- 100020 -0-030 ·-	24-176074	. 78535
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NUM 9E R	×	Y ANGLE THICKNESS	ANGLET	HICKNESS	X	¥5	S YS XP	٩
e	. A5 24 A	39742	-3,767	63573	.85435	37959	. 65201	41525
7.	66651	-33819	-2.874	03349	.86735	38147	. 86567	41492
1.	67984	67984 - 39876	-2.301	. 63113	.68038	38320	. 67930	41431
. M.	89317	39912	-1.129	. 02864	• 8 9345	36488	. 89289	41344
1.		82668	258	. 02602	991656	38627	4906.	41229
7.	0.40.00	3000	612	62327	.91971	-,38761	96676	41088
7.	93316	39995	1.481	62038	.93293	38881	. 93342	
1	04540	3985		. 01735	-94614	38989	•	48722
. «	45.082	39791		01418	.95942	39383	•	
2.0	97315	39796		. 01086	.97277	39164	. 97 354	743247
) ć	GASER	33561		0.0739	.98616	39233	•	39969
	99991	99981 - 39476	5.782	.03376	-99962	.9996239289	+	39663

## STREAMSURFACE GEOMETRY ON STREAM INE HUNDER S

BETAL	11日本の日本	(COLADS INLET ANGLE.)
BETA2	* .664	(BLASE OUTLET ANGLE,)
VZ 8.00	21206 - *	(SERVER LEADING EDGE RADIUS AS A FRACTION OF CHORD.)
-	£ .35255	(BLADE MAXINGW THICKNESS AS A FRACTION OF CHORD.)
YOME	69306* *	COLADY TRAILING EDGE MALF-THICKNESS AS A FRACTION OF CHORD.
•	4.664° a	(LOCATION OF MAXIMUM THICKNESS AS A FRACTION OF MEAN LINE.)
50.50	s 3.2991	(NEXI) IONAL CHORD OF SECTION.)

NORTALISED RESULTS - ALL THE FOLLOWING REFER TO ASLADE MAVING A MERIDIGNAL CHORD PROJECTION OF UNITY PROFESSORES CONTRACTOR CONTRACT

* 1.0335 BLASE CHORD STAGGER ANGLE x-23.843

CAMBER ANGLE =-+2.379

SECTION AREA . . 04352

LOCATION OF CENTROID RELATIVE TO LEADING EDGE

7348 = .53650 7348 = -.31169

SECOND HOMENTS OF AREA ABOUT CENTROLS

IX = .03257 IX = -.00257

ANGLE OF INCLINATION OF TONE! PRINCIPAL AXIS TO "X" AXIS 8-21,956

PRINCIPAL SECOND HOMENIS OF AREA ABOUT CENTROLO

(A1-23.956 WITH PX* AXIS) 19230 - a Kel

POINT	RESTREE OSTA	SURFACE COORDINATE DATA	
म् अत्य क्ष	K WAGLE TAICHESS	XS YS XP	
•4	3. 2:020-61.615	. 90174	_
۰.	. 11451 - 11071-41,241 . 18655	. 71234	
**	. 32669 32133-46.973 . 30646	01.614 . 02391	
3	٠	02795 . 03549	_
ĸ	٠	94708	_
ۍ		. 15868	_
	. 975-2 96293-39, 949 1596	.0885435681 .0702996905	
•	•		
<b>9</b> *	٠		
C.	. 11147 19336-39, 331 . 02138	.1187308476 . 105241.137	_
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COORDINATE CATA IS RP YP	.12'42 .1521J -14278 .12933 .1538615281	17566 -	- 69661	. 22.125	23568	. 24780 -	25994 -	. 28430 -	- 29652 -	39877 -	. 33335 -	34568	37.242	36283 -	10162	00000	43005	10075	.46718	.47928	- 60 MAG -	51563 -	. 52776 -	. 55205	. 56420 -	. 56682 -	- 60130 -	.64380 -	63883 -	.65138	5961 .555393	7681 .68907 -	1036 . 70166	0387 •71426 ·•	- 29584 - 6506	9381 .75289	1000 .7777 - 445	3328 . 79143 4	0645 . 60547448	9952 . 6197 £ 449
SURFACE KS KS	22 .16931 -	. 19446	- 521974	1 24250 1 2425	- 52220	*2703.	.25258 .25258	- 30795	* 6400 M	17 33292	.3577.	- 37016	2620C*	. 40717	F 10644	- 000000	4.5453	46994	- 16684	- 50168 -	* ************************************	58985	- 734484 - 124484	.57212	3000 S	63755	-61953	53 - 63150 - 54150 - 74150 - 75	***************************************	.66730	- 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19° - 1,26,19°	.70298	- 71486 -		************	.75228	- 74474.	- 179916 -	- 81241 -	n -
A H L T M E D A T A Y A A A A A A A A A A A A A A A A	-, 13160-37	- 15009-36 . 91 . 0	** 15815-15.895 .0	C. CC4.CC-201/1	- 13430-44-683	20271-33.989 - 3	21897-33.486 21807-33.486	22731-12.+56	21479-31-924	1. 24242-35. 35. 35. 1. 2. 2. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3.	25716-30,264	- 56429-29.569	-, 27 80%-28, 505	23467-27.896	- 29391-27 355	C1/43-C0-/ CC	31472-25.561	. 31436-25-023	12522-23.936	. 33046-23.408	. 16453-22.893	. 34539-21.847	. 15012-21-403	. 15925-20-473	. 35 366-20.022	. 36795-19.587	. 1764n-18.665	. 13052-18	. 39435-17.235 . 0	0、 36201-16.7%。	0. 395.41-816.204 10-816-44-44.5	*1130-15-11#	** 1580-14. 556 . C	TOTAL		61766-12-173	2	-, 42497-18.168	42732 -9.446 .0	· 271.9- 85624 ·-
POLSE A E	. 16373 . 17289	19726	2	•			•	• •		からない ・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・		•				* *	•	•	45844						20440	0.00000						* 6%63	. 7662	44684°		. 7572				95228

POIN	<b>Z</b> :	W 	æ ω	4 ×	SURFACE	COORDI	NATE DA	⋖
NUMBER	×	>	ANGLE T	X Y ANGLE THICKNESS	XS YS XP	Ş	Α A	ΥP
7.3	18648	-, 43333	-7 . 25E	. 03626	.85217	41534	. 84758	45133
7.7	. 66352	~ . 43498	6.529	* 0.3404	.86545 -	41839	. 86159	45188
72	. 6771.	43646	-5.802	. 03169	.87876	42724	. 87557	45218
73	. 69061	. 69081 43775	-5.376	. 62905	.8921342328 .	42328	. 88953 45222	- 4 5222
2	. 90446	4.3688	4.352	. 62636	- 99566	42574	. 90346	- 45202
75	. 91810	4 3983	-3.629	. 02353	.91885	42839	. 91736	45157
76	93175	44.361	-2.908	+ 02054	.93227	43 35	. 93123	45387
11	. 94543	*. 44122	-2.189	. 61740	.94573	43252	90450	44591
<b>1</b> 5	* 95934	44165	-1.472	. 11411	.95922	43460	. 95886	44871
79	. 37.269	44192	757	. 01966	.97276 -	43659	• 97262	44725
93	. 98634	44202	1.045	• 0 17 0 4	- 98634 -	43850	. 98633	44554
•	* CO CO	30000	7 7	2020	90000	4000		

### SIREAMSURFACE GEOMETRY ON STREAM INE NUMBER 6

The state of the second with the second

s-42.649 (8LAGE INTET ANGLE.)  4 -4.217 (GLAGE GUTLET ANGLE.)  4 -5.145 (GLAGE MAXIMUM SOGE RADIUS AS A FRACTION OF CHORD.)  5 -5.145 (SLAGE MAXIMUM THICKNESS AS A FRACTION OF CHORD.)  6 -5.147 (ELAGE FRALING EDGE MALF-INIONESS AS A FRACTION OF CHORD.)  7 -6.12° (LOCATION OF MAXIMUM THICKNESS AS A FRACTION OF NEAN LINE.)  7 -6.12° (LOCATION OF MAXIMUM THICKNESS AS A FRACTION OF NEAN LINE.)  7 -6.12° (RERIGIONAL CHORD OF SECTION.)	MOSMALISEO AESILIS - ELL IME FOLLOMINS REFER TO ABLADE MAVING A MERIOTOMAL GNORD PROJECTION GF UNITY begardere entres casastates casastates accessors conserved by the American casastates and the Choro as a casastate an	2 + 1 2 6 + 4 5 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	man de la companya de	LOCATION OF CENTROID MELATIVE TO LEAGING EGGE  ESAR - S3374  TSAR 53724	SECOND YOMEN'S OF AREA ABOUT CENTROIS	Superior of the superior of th	INCLINATION OF CONES PRINCIPAL AXIS TO "X" AXIS 4-26.482	second homents of Area addi' centrolo	: # .059)3	REARLURE OATE CURFACE COORDINATE DATA RATE TARGET MICHIESS XS YS XP YP
	1 - 411 THE 	*-26.463	Hends .	MERCIO MEL. M 53374 M 53374	OF AREA &	190000 B	MATEON OF	NO MOREHTS		
62 1 4 1 05 1 4 2 05 1 6 2 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	NOS MALISEO AESULTS ************************************	STAGGER ANGLE CANBER ANGLE	SECTION AREA	LOCATION OF CE	SECOND 40MENTS	****	SHOLE OF INCLI	THE PAL SEC	x 61	Tr IOS

POINT NUMBER	# G G G G G G G G G G G G G G G G G G G	A T A MECRMESS	SURFACE COORD	10080 INA TE OA TA	٩
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40	,	100 m	•	17543	17077
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PCINT	HEBRLINE DATA	SURFACE COORDINATE DATA
NUM BE &	X Y ANGLE THICKNESS	XS YS XP
7.5	+5+80.00 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 2	.8557966137 .8491449567
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7.8	.95967 43453 -6.137 .01363	.9683948776 . 958965J131
19	*97738 - 49588 -5.428 .01633	497356 - 49174 .97259 - 50102
<b>60</b>	.98548437'8 -4.822 . 1068B	
<b>T</b>	. 99988 - 43814 -4.217 . 18328	

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ANGLE OF INCLINATION OF 10HI! PRINCIPAL AXIS 10 'X' AXIS =-29,301

PRINCIPAL SECOND MONENTS OF AREA ABOUT CENTROLO

(AT-29.3)1 HITH "Y" AXIS)

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SURFACE COORDINATE DATA

HEANLINE DATA
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X E	. 65733	- 87.025 -	. 65319 -	- 93965 *	- 60606 •	. 92214	- 66926 -	- 46246 •	- 96989 -	. 97354	- 62986.	+ 42666
Pul Mi NUMBER												

# STREAMSURFACE GEOMETRY ON STREAMLINE HUNGER &

Charles But ...

	AS A SACTION OF CHORD.)	AS A FRACILUM OF CHOKUS.)	(LOCATION OF MAXIMUM THICKNESS AS A FRACTION OF MEAN LINE.) (MERIDIOHAL CHORD OF SECTION.)
(SLADE IMLEY ANGLE.) (SLADE OUTLEY ANGLE.)	COLLAGE LEADING EDSE RADIC	COLADE TRALIMOR INICAMENS (SLADE TRAILING EDGE MALF.	(LOCATION OF MAXIMUM THIC (MERIDIOMAL CHORD OF SECT
100°04°1	# . 0325#	544:40 a	* 5.17 %
8E741	7759.0	YONE	2 23 23 <b>~</b>

MORTALISEO RESULTS - ALL TWE FOLLOWING REFER TO ASLADE MAVING A MERIDIONAL CHORD PROJECTION OF UNITY

F 1.1820 BLADE CHORD

STAGGER ANGLE #-32.235

**=-31.051** CAMPER ANGLE . 3431)

SECTION AREA

LOCATION OF CONTROLS RELATIVE TO LEADING EDGE

X34K = .52636 Y342 = -.39833

SECOND HOMENTS OF AREA ABOUT CENTROID

IX = .03.94 IY = .66232 12 = .40232

ANGLE OF ENCLIMATION OF CORD PRINCIPAL AXIS TO "1" AXIS =-32.230

PRINCIPAL SECOND MONENTS OF AREA ABOUT CENTROID

(AT-32,23; MITH "X" AXLS) (AT-32,23) MITH "Y" AXLS) \$2000 = Xol

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## STRIAMSURFACE GEOMETRY ON STREAM INE NUMBER 9

E 14:		CBLADE TELET AMORE.
E 1 42		COLADE CUTLET AMOLE.)
72520		(SLADE LEADING EDGE RACIUS AS A FRACTION OF CHORD.)
		(BLADE REMINUM INICAMESS AS A FRACTION OF CHORD.)
OK	. 83553	(BLADE TRAILLING EOGE MALF-THICKNESS AS A FRACTION OF CHORD.)
		CLOCATION OF RAXIMEN THICKNESS AS A FRACTION OF HEAN LINE.
5,65		(MERIDIDHAL CHGRO OF SECTION.)

MORMALISED RESILIS - ALL THE FOLLOWING REFER TO ABLADE: MAVING A MERIDIONAL CHORD PROJECTION OF UNITY WAS SECRETED RESISTANCES OF CHORD PROJECTION OF UNITY

MADE CHORD # 1.2216

STAGGER ANGLE #-35.810

CAMBER ANGLE #-27.353

SECTION AREA # . \$9314

LOCATION OF CENTROLD RELATIVE TO LEADING EDGE

THAN # . \$3957

THAN # - . \$3957

SECOND MORENTS OF AREA ABOUT CENTROLO

IX = .46212 IX = .46212 IX = -.65265 ANGLE OF ENGLINATION OF COMES PRINCIPAL AXIS TO "X" AXIS =-35.892 PRINCIPAL SECOND NONENTS OF AREA ABOUT CENTROLO

19 x x . 60662 (41-15-190 MITH "X" AXIS) [AT-25-690 MITH "Y" AXIS)

\$10.0 \$10.0	¥	*************	A T &	SURFACE	E COORDI	SURFACE COORDINATE DATA	≤
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ø	. 86524	86545-45.719		.16356	06124	. 06092	-+06966
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7.3	867.5	.8674565144-22.322	.03116	.8733763733	٠	66585
71	87945	65631-21. 869	. 2923	.8848964276	٠	8740166986
72	69110	65138-21.438	. 92714	.89641648+4	• 38649	67371
7	36.345	30345 65574-21. 128	1848	.9179365438	. 89897	67739
7.5	92.545	67833-26.641	•	.9194565969	٠	68095
25	92745	67478-20.277	•	.9309766526	. 92393	- e68430
75	93969	93945 - 67917-19,936	•	.9424867181	•	68754
77	95145	63349-19-619	•	.9539967634	•	- • 6 90 63
7.8	36365	63773-19.325		.9655168186	•	6936
7.3	97546	63190-19, 356	•	.9770168738	•	69643
, eq	987.44	98744 69502-19-511	. 09663	.9685169290	. 98638	69914
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# STREAMSLAFE GEOMETRY ON STREAM INE NUMBER 10

HADIUS AS A FRACTION OF CHORD.) HESS AS A FRACTION OF CHORD.) HALF-THICKNESS AS A FRACTION OF CHORD.) THECKNESS AS A FRACTION OF MEAN LINE.) SECTION.)	NOMINISCO RESULTS - ALL TMF FOLLONIMG REFER TO ABLADE KAVING A MERICIONAL CHORD PROJECTION OF UNITY est encaractere of experience encaractere escape							592-KS-2 SING FX		AXIS	SURFACE COORDINATE DATA KS YS XP YP	.04295 .00117 .19046001117 .0153401193 .0125501539	02502 . u24840 03819 . 037038			10316 .09607	11031	
INCET ANGLE.) CUTLET ANGLE. LEADINE ENGE TRAINUM TRIENT TOM OF MAXIMUM ENGAL	S SEFEN TO ASLADE H			EAGTHG EDGE		0104			ASOUT CENTROID	141-171-760 HITE 'X' BKI	ME O 4 1 A MACLE THICKNESS	のないなか。					6.406 .01795 6.297 .41947	
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## STREAMSURFACE GEOMETRY ON STREAM, INE NUMBER 11 exectment

ETAL	8-67.736	(SLADE INLET ANGLE.)
5142	E-27.346	(SLADE DUTLET ANGLE.)
2593	a .01134	(BLADE LEADING EDGE RADIUS AS A FRACTION OF CHORD.)
	337:3	COLADE MAXIMUM THICKNESS AS A FRACTION OF CHORD.
311C	Contract of the Contract of th	ISLADE TRAILING EDGE MALF-IMICKHESS AS A FRACTION OF CHOKU.)
	a . 5349	(LOCATION OF MAXIMUM THICKNESS AS A FRACTION OF MFAN LINE.)
Cav	F 7.447'E	CAROTOTOMA: CHORD OF AFCITOM.

MORTALISSO ASSULIS - ALL THE FOLLOWING REFER TO ABLADE HAVING A HERIOIUNAL CHORD PROJECTION OF UNITY SEL COCCOCCESSORS CONTRACTOR SELECTER SELECTED OF UNITY.

F 1.3753 MADE CHORD STAGGER ANGLE =-+ 3.159

E-27.462 CAMBER ANGLE F . ASSA SECTION AREA

LOCATION OF CENTROID RELATIVE TO LEADING EDGE

7348 = .5147: 7348 = -.51129

SECOND HOMENTS OF AREA ASSUT CENTROLD

IX = .34168 IX = .34235 IXY = -.34197

ANGLE OF INCLINATION OF COME) PRINCIPAL AXIS TO "X" AXIS =-40.234 (AT-45,234 WITH "Y" AXIS) PRINCIPAL SECOND HOMENTS OF AREA ABOUT CENTROLD

SURFACE COORDINATE DATA MEANLINE DATA 901 of 1894 95 R .03707 - 04545 .04928 - 06637 .16148 - 07633 .16148 - 07633 .16391 - 11.583 .99613 - 12033 .14316 - .04:04 .05653 - .05394 .06991 - .06789 .16327 - .06157 . 76312 - 14275-45.343 . 35291 - 15715-45.457 . 76569

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# STREAMSURFACE GEOMETRY ON STREAMLINE NUMBER 12

TO THE PARTY OF TH

HORMALISED RESULTS - ALL THE FOLLOWING REFER TO ABLADE HAVING A MERICIONAL CHORD PROJECTION OF UNITY SER SECONDACIONS CHORD PROJECTION OF UNITY

84.40£ CHORD = 1.3554

STAGGER ANGLE s-+2,493

CAMBER ANGLE =-17,375

SECTION AREA # . 34372

LOCATION OF CENTROID RELATIVE TO LEADING EDGE

X342 = .51754 Y342 = -.53713 SECOND 40MENTS OF AREA ABOUT CENTROLD

IX = .03237 IX = .03237 IX = .03237 ANGLE OF INCLINATION OF (ONE) PRINCIPAL AXIS TO "X" AXIS =-42,553

PRINCIPAL SECOND HONGHTS OF AREA ABOUT SENTROID

19x x .73311 (AT-42,593 MITH 'X' AXIS) 19y x .73436 (AT-42,593 MITH 'Y' AXIS)

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WITH BER	×	X Y ANGLE THICKNESS	HICKNESS	ž	XS YS XP Y	ж С	Ϋ́
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· ~	35458	31455-48.932	. 19511	.01653	01287		.01265 11623
•	. 12732	. 12732 12924-49.179	• 03655	• 42963 •	+0.2710		03138
•	- 36036 -	34405-49.386	٠	.0431.0	04144	. 03702	04665
· Cr	. 15283	15895-49-556		.05643	- • 0 5589	. 04921	06202
. 40		.7 394-49.683		.36973	67341	. 06139	07747
	37.823	33899-49.785		.09333	18510	. 7357	99297
•	. 19113	79413 - 17458-49.847	• 01379	.09633	19963	.08576	.00576 1.0552
· œ	1:377	11919-49.972		.13959	.11-28	9626,	12409
	- 11652	13432-49.862		.12288	.12894	. 11016	13967
) (c)	12925	12925 14961-49.517	•	-13615 -	14359	. 12237	15523
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52	35924-46	•	28883	30307 3	ĸ
27	37203-46.	•	4141 - , 3593	315043	~
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62	39728-45.		66413838	339044	•
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6.5	74758-16	•	76241 - 7384	73684 7	
29	75702-36.	•	774617401	749957	
29	76637-W.	•	78719 - 27498	763881	-
3	77561- M.	. 039	19954 - 1759	77624 1	•
65	75476-35.41	.0386	811877690	789431	
•	79255-	.0373	23837782	7	8
<b>6</b> 7	3225-34.91	. 03501	8357678	i	<b>-</b>
**	- 1086- V	300	47667966	***	•
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סטד ועד	7	2 - 7	<b>0</b>	ATA	SURFA	SURFACE COORDINATE DATA	NATE DA	Ā
NUMBER	: ×	Y ANGLE THICKNESS	NGLE T	HICKNESS	XX	₹	X م	<b>4</b>
7	46266	86054 - 80781-34-188	60 61 51	63421	.87139	.8713981489	. 85393	84074
	87514	- A 46.16+3	3.817	12937	.88321	82336	. 85687	84836
100	48764	E-1044448-	3.548		+89501	83391	.87987	85585
, K	18008	89984 + 85261-33,283	3.283	•	e 3 3 6 7 9	- ,84232	. 89289	89289 - + 86319
2.6	0400	E-02030-	3.123	•	.91853	85102	<b>*6506</b>	87039
7.	92464	95872-3	2.760	•	.93025	.9302585999	91905	87745
7.2	20226	87666-3	2.594	•	.94194	.9419486896	. 93213	88437
22	96963	94943 88452-32-251	2.251	.01565	.95361	87790	• 94526	9452689114
. 42	95183	89231-3	2.331	.01289	.96525	88684	. 95842	89777
9 6	97423	47423 91002-31.754	1.754	66600	.97686	89577	. 97160	93427
) C	98663	93766-3	1.511	. 00694	*4986°	69406*-	. 98481	91062
<b>8</b> 0	. 9993	9993 - 91522-31-272	1.272	. 00375	1.00003	91362	. 99805	91682
i		1						

# STREAKSURFACE GEOMETRY ON STREAM INE NUMBER 13 Recesses assesses excesses

BETAL	164.64-2	(SLADE INLET ANGLE.)
BETA2	E-36.930	(BLACE CUTLET ANGLE,)
YZERO	e 33537	(BLADE LEADING EDGE RADIUS AS A FRACTION OF CHORD.)
-	- 13250	(BLADE MAXIMUM THICKNESS AS A FRACTION OF CHORD.)
YOME	* .63137	(BLADE TRAILING EDGE MALF-THICKNESS AS A FRACTION OF CHORD.)
	. 65833	(LOCATION OF MAXIMUM THICKNESS AS A FRACTION OF MEAN LINE.)
CORD	* 2.8351	(HERIDIONAL CHORD OF SECTION.)

#LADE CHORD = 1.4066 STAGGER ANGLE = -44.730 CAMBER ANGLE = -16.550 LOCATION OF CENTROID RELATIVE TO LEADING EDGE

E . 06417

SECTION AREA

XBAR = .52053 YBAR = -.57496 SECOND HUNDATS OF AREA ABOUT CENTROLD

IX = .00238 IY = .00241 IXY = -.33238 ANGLE OF INCLINATION OF CONE) PRINCIPAL AXIS 10 'x' AXIS =-44.645

PRINCIPAL SECOND MOMENTS OF AREA ABOUT CENTROID

(AT-46.845 HITH 'X' AXIS) (AT-44.845 HITH 'Y' AXIS)

IPX = .80001 IPY = .30475

TH TOO	TEASTHEE DATA	SURFACE COORDINATE DATA	ATE DATA
20 KO2		2	
**	. 60193 9. 63086-49. 491 . 69385	.00125	13046 00125
.∾	11495-49-619 ·	•	17564 01663
*		.0298302796 .0	0246103216
		. 0424004280.	03697 04784
•	06571-50-573	•	0491406365
· <b>v</b> ð			.0613007956
~	09176-50-894	•	37346 09556
•		10324 .	08562 11163
•	12314-51.377 .	11653 .	39779 12775
¥0	13887-51-118 .	13385 .	11996 14390
: :	15462-51.126	- 2491B .	12214 16006
12	. 14159 17436-51-160 .01865	- 15451 .	13433 17622
*	. 15429 18608-51.040 .01995	٠	16653 19236

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25	i	0-44.756	358	. 3 5148	• 3910	22463	564K4*-
•	ì	1-47.823	2	.36384		. 33664	42873
2	ì	1-47.588	5	.37617	.4173	34850	
-1	i	9-47.353	. 23823	6498£*	* 4299	. 36038	
~	•	7-47-110	• 03895	09004*	- +4427	. 37226	
*	ï	4-46.867	. 03963	•41309	4	30417	3
	ř	7-46.623	. 04028	.42534	- 1679	. 39607	
w.	. 42278 4345	0-46.379	. 04.393	.43758	かいのす。	. 43796	50861
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. 18	7	5	5	.55918		. 52791	w
	7	7-43.735	.04526	.57125	6112	. 53998	64393
_	7	6-43.464	S	.58332	- +6225	. 55207	65555
•		55346-43.224	*04556	.59537	6338	. 56417	66706
	7	6-42.983	. 04565	*60741	190	. 57629	67846
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78	. 65794	63581	.6578483581-37.330	. 03171	.86746	.8674687420	. 84823	8482389942
71	. 87366	83655	5-37.1175	-	.87963	88461	. 86165	90848
72	. 88349	91619	3-36.826		.89187	- 89500	.87510	91739
73	. 89631	-, 9157	3-36,585	. 02589	.90403	- ,90536	. 88859	92615
<b>5.</b>	. 99913	-, 9252	5-36,352	• 02367	•91615	.9161591570	. 90212	93476
75	. 92136	9346	3-36.125	-	.92824	.9282492632	. 91567	94323
<b>1</b> 6	. 93475	-, 94395	. 93478 94395-35.936		.94629	93634	. 92927	95156
77	. 94753	95321	3-35.695	•	•95231	94665	. 94290	95975
78	\$ 96 34 3	9523	3-35.492	•	•96459	.9642995636	95656	96779
62	. 97 325	97149	3-35.297	. 91032	.97623	.9762396728	. 97027	97027 97570
83	. 986 17	-, 98:55	3-35.139	. 90717	.98814	.9881497750	. 98401	98401 98347
81	. 99893	98952	99893 98952-34-930	. 00385	1.33003	1.3300398794	. 99779	99779 99110

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E 1.4633 BLAGE CHORD STAGGER ANGLE ==+6.934

CANSER ANGLE #-11.965

SECTION AREA # . 14439

LOCATION OF CENTADIO RELATIVE TO LEADING EDGE

X342 = .52365 Y842 = -.61537

SECOND HOMENTS OF AREA ABOUT CENTROLD

ANGLE OF INCLINATION OF (ONE) PRINCIPAL AXIS TO "X" AXIS = 42.855

PRINCIPAL SECOND HOMENTS OF AREA ABOUT CENTROID

SURFACE COORDINATE DATA KERNITEE OATE

(AT 42.858 HITH "X" AXIS)

IPX = . 29533 IPY = .00003

: DATA YP	10066 - 01128 01266 - 01709 02686 - 01709 03705 - 06925 76924 - 06557 77512 - 09858 78579 - 11525 09797 - 13199 11316 - 14568 13455 - 16565 13455 - 16565
SURFACE COORDINATE DATA IS YS XP	10.355
•	20 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
MERNITWE DATA	13 2.01079-50.346 13 -11542-50.346 13 -11542-50.346 13 -14681-51.025 13 -17861-51.956 13 -17861-51.963 14 -11276-52.123 13 -12764-52.403 14 -13764-52.403
POINT N HUMBER X	

DX 104	¢	•	SURFACE		ATE DATA	2	
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<i>5</i>	21006-52.416	12047	5	.2338	1589	~	
£ 4	-, 22555-52-361	02168	2	2193	1712		
1.5	2+299-52.276	18223	m	.2350	. 18344	2	
17	+. 25938-52.169 .	62403		.2520	. 1957 3	N	
13	27476-52-133 .	12512	•	•2673	. 20726	ņ	
5	23011-51.895 .	62618	ķ	.2823	22.88	ņ	
<b>5</b> 2	- 31537-51.754 .	62721	Ž.	•2969	. 23646	-,31379	
12	- 32054-52.603	(2823	N.	31177	. 24216	7	
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tr.	- 17454-42-193	16.61	0	66955	10595	٠,	
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	- B1085-43-959	66140	•	7.0	67.29		
	1 01252-65.718	44366		7958	68.55	•	
6.6	- 824-63-45-467	64326	-	-6387		. 40	
3	67626-43.236	04278		.8276	7133		
•	4-6-791-42-935	04222		.8324	7236		
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65	89338-41.748	13904	8	735	77.59	ਯਾ	
3	- 411267-4144	379	•	918	5	Ţ	
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SECTION AREA	t-1946 1	
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SURFACE COORDINATE DATA XS YS XP YP

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٠	785 - 22062-53.976 .0	•	7593 - 21	7651.	26
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17	511 - 27319-53.890 .0	÷.	2.55	1966	283
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9	62603-49.694	.23	4959361	•	-0
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\$	0+0. 086.44.954.6. 6.1	27	6- 0259	. 7572	ç
	78383 - 95688-44.659 .039	m	79764 - 94	1694	σ,
0 t	79/63 30/99-44-510 84664 08109-54-090	25	Ý 4	0K6 . 79776	5 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
5	2 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 -	4 6	8 3545 - A	. K117	
2	75-1-04-06-43-377 . 0	9	932 - 99		1

POINT	C BRITHE O	A T A	SURFACE COORDINATE DATA	NATE DATA
NUM BER	X Y ANGLE THICKNESS	HICKHESS	XS YS	ΥΡ
7.9	. 65 194-1, 32128-43, 137	en3281	.86215-1.01931	. 83973-1. 03320
7.1	. 86437-1, 13379-42, 858	. 03107	.87493-1.02241	. 35383-1.0451
72	. 87779-1. 14620-42.631	. 02917	.88767-1.03547	. 86791-1.0569
73	. 89122-1. 35852-42.427	. 02712	.90037-1.04851	, 88207-1.0685
7.4	.93445-1.07375-42.245	• 92489	+91332-1 -86154	. 89628-1.0799
75	. 91838-1. 38291-42, 387	• 02259	.92561-1.07456	. 91054-1.0512
92	.93153-1.19591-41.952	. 01992	.93816-1.0375C	. 92484-1-1324
11	.94493-1.1705-41.842	• 91715	.95365-1.13366	. 93921-1-1134
78	. 95836-1, 11986-41,756	. 31420	.96308-1.11376	. 95363-1.1243
79	. 97178-1.13103-41.694	.01104	.97546-1.12691	. 96811-1.1351
80	. 98521-1. 14298-41.656	• 60768	.98776-1,14312	. 98266-1.1458
1.9	. 99864-1. 15492-41.644	. 90413	1.10000-1.15339	. 33728-1.1564

# STREAKSURFACE GEOMETRY ON STREAMLINE NUMBER 16

VZERO E GOLDE LEADING ENGE RADIUS AS A FRACTION OF CHORD.)  1 1
TALL BO MOTIFIED COOLS INCOME A CHARACTER OF COURT AND CONTRACTOR OF CON

NDRMALISED RESILIS - ALL THE FOLLOWING REFER TO ABLADE HAVING A HERICIONAL CHORD PROJECTION OF UNITY RECESSORS SERVED SER

BLADE CHORD # 1.6314

STAGGER ANGLE E-51.6"3
CAMBER ANGLE E -7.573

SECTION AREA s . 34864

LOCATION OF CENTROID RELATIVE TO LEADING EDGE

K3AQ = .52394 Y3AR = -.71+39 SECOND SOMESTS OF AREA ABOUT CENTROLD

IX = .03426 IY = .10266 IXY = -.50236 ANGLE OF INCLINATION OF (ONE) PRINCIPAL AXIS TO "X" AXIS = 38.233

PRINCIPAL SECOND MONENTS OF AREA ABOUT CENTROLD

MEANLINE DATA
Y ANGLE THICKNESS

SURFACE COORDINATE DATA
XS YS XP YP

·	292, 29-604, 0.0 \$ 1000.	1:8427	.01382 .01131	
• ^	61103 -11677-52.783	200544	.0171501513	. 31282 81542
	1976 - 03384-53,229	. 03662	.0 304903135	.02519 03562
1 1	- 46469 - 155156-53-632	. 20783	.0436304885	.03755 05348
· u	145 454 - 1667 3-53, 995	60600	.0571836639	.04993 07138
٠.4	246.40 - 24653-55.	. 61621	.07354 - +08355	622508950
•	10707 + 1 1452-54-605	. 61141	.0039313122	. r7459 19783
. «	058 - FS - 02222 12550 - 1	. 01262	.0972611936	869412633
<b>o</b> d	100 00 00 00 00 00 00 00 00 00 00 00 00	01383	.1136213737	. 09928 14499
٠,	はいっとは、このなりです。とのなるです。	.61504	.12398 15521	.1116216378
? <del>.</del>	43165 - 17898-55-435	. 11624	.1373417347	. 12397 1325
10	14353 - 13675-55-523	.01743	.1506919182	.13632 2:169
11	.15636 21550-55.613	• #1862	*1640421:24	.1486722v76

POINT	MEANLINE D		SURFACE COORDINATE	DATA	
NUN BE &	ANGLE	THICKNESS	-	<b>d</b> ↓ d×	
3.6	23430-55.	•	77302287	16103	•
15	.1623625313-55.692	• 02096	*19072 - +24722	i	
97	-, 27196-55.	_	0404 2657	i	•
17	23378-55.	• 02324	1736 - ,2842	i	• •
M 4	-21976 - 31631-35-356 	12420	- 2362	.20474 - 63151	
7 6	16.126-95	62630	5457 - 33358		
12	36065-55	02726	6696 - 3529	24451	
23	37799-55	+02024	7933 - ,36	i	
23	39527-55.	-	91703869	26774	_
24	41247-55.		- 5040	•	_
52	15-0962-54-	• 63099	4207	i	_
<b>5</b> 2	44664-54.7	• 03166	•	i	<b>6</b> 11
27	0 46359-5- 0		.3410245413	31436	•
D (0	1000000			1777	0 ~
A 84	5 387-55	63507		979	
31	566 53034-53			36119	•
32	54674-53.	0	ŗ	i	.*
33	56300-53.	. 63718	ř	471	
3¢	1135 -,57874-57.	. 03761	5674	621	10
35	59436-53.	. 63841	ř.	i N	_ 1
36	7 6.986-52.	. 03896	ř	. 41924 6216	<b>m</b> 1
37	4648 62523-52-6	• 03952	ě.	43078 -	<b>.</b>
10 t	616 64350-52.	. 104040	7079*	2024	<b></b> .
) (	- 67074-524	14001	1 .0 4 30	200	
3	- 5.8555-51.	. 14139	- 67.78	47703	
2	7 ; 052-	.04178	•	48863	
7	71529-51.	. 64214	7021	53023	_
i	72998-51.	. 64247	7167	ï	.•
<b>6</b> 5	74458-51.	. 04277	7 311	i	er)
9	75911-51.	* 96304	7 455	i	en .
12	77.557-53	.04328	- 1599	i	
<b>8</b> (	75796-50	. 04343	120	25641	= -
J (	- 6727-56		4004	54222	- ^
, <u>.</u>	A 1.147-50.	, ,	- A17A	138	
25	64656-50	. 04398	- 6325	60655 -	
53	86117-50.			674	•
24	750 87570-	. 04402	8615	**	
ν.	89015-49	ω.	- 6759	64317 -	٠,
2 2	21.5 - 9.1450-49.	<b>5</b> 6	9 9	14229	u a
. «	91293-69.2		- 9167		n La
6.6	\$ 94699-49		9327	69229	•
9	2080 96093-48.	0	- *9467	. +94	•••
61	296 97477-48.	* 04253	<b>1096*</b>	702	<b>10</b> 1
<b>6</b> 2	272 98849-48	, 04203	-97.45	72944-1	
6.3 6.3	0 ) 208-46	* 04146	\$2506 U.S.7.	75647-1	* 11
<b>.</b>	160-1, 1, 2,22-4, 162-4, 1,2880-47,	.03998	7.0153	4-64	
9	518-1-04359-47	0369	0947-1 00333	78089-1.	•
29	873-1. 85813-46.	0378	2255-1 .0451	492-1.	_
99	1.07252-	. 03659	.63558-1.05995	960-1-085	<b>-</b> 1
63	3584-1, 08678-46, 3	351	4856-1.0746	513-1.056	'n

POINT	MEANLINE DATA	er	SURFACE COORDINATE DATA	NATE DATA
NUM BER	X Y ANGLE THICKN	NESS )	S YS	XP YP
7.0	.84948-1.17391-46.863 .73361		66150-1-08925	83730-1-11257
71	•		-87439-1-10381	455150 TITELED.
72	•		.8 d723-1 .11634	86579-1-13931
73	•		*9 J0 01-1 *1 3284	. 88812-1-15242
74	•		91274-1 14733	89451-1,16539
75	•		92540-1-16181	90895-1-17820
76	.93073-1.18359-45.004 .02059		•93801-1 •17631	92345-1-19087
7.7	•		95055-1 19383	93802-1,23341
78	•		.96303-1.29539	.95266-1.21583
79	•		97543-1.22000	. 96736-1,22814
83	.98495-1.23751-44.730 .03797		.98775-1.23458	98215-1-24033
81	•	1	1.00003-1.24942	. 39701-1-25244

# STREAMSURFACE GEOMETRY ON STREAMLINE NUMBER 17

= 53.457 (BLADE INLET ANGLE.)  = -47.621 (BLADE CUTLET ANGLE.)  = -03131 (BLADE LEADING EDGE RADIUS AS A FRACTION OF CHORD.)  = -03131 (BLADE LEATING THICKNESS AS A FRACTION OF CHORD.)  = -00131 (BLADE TRAITING EDGE HALF-THICKNESS AS A FRACTION OF CHORD.)  = -6880 (LOCATION OF MAXIMUM THICKNESS AS A FRACTION OF MEAN LINE.)  = 2.8593 (MERIDIONAL CHORD OF SECTION.)	NORKALISED RESULTS — ALL THE FOLLONING REFER TO ABLADE HAVING A NERIDIONAL CHORD PROJECTION OF UNITY Det exposes conscious exposes excesses excesses extracted experts experts expectative excesses experts experts	.O = 1.6855	STAGGER. ANGLE53.656	1£ = -5,837	EA c .05197	LOCATION OF CENTROID RELATIVE TO LEADING EDGE	XBAR = ~53337 YBAR = ~077215	SECOND MOMENTS OF AREA ABOUT CENTROID	IX = .06541 IY = .06284 IXY =05390	angle of inclination of (one) principal axis to "x" axis = 35.694
META1 META2 YZERD T T YONE 2 CORD	NORMALISED RES	BLADE CHORD	STAGGER. AN	CAMBER ANGLE	SECTION AREA	LOCATION O		SECOND HON	·	ANGLE OF I

. 30043 - 00131 . 01294 - 01934 . 03794 - 05538 . 05081 - 05538 . 05286 - 019458 . 0528 - 15375 . 1029 - 15375 . 11276 - 17372 . 12370 - 21428

01745 -01616 03691 -03379 04441 -03379 04741 -03379 06491 -07116 06491 -16771 06491 -1677 12543 -1654 13694 -1659 13694 -1659 15695 -21675

. 80.221 6.9000-53.457 . 01528 - 0.31778-54.800 . 02117 - 0.3574-54.404 . 054117 - 0.5578-54.346 . 05412 - 0.07275-55.740 . 05715 - 0.0157-55.740 . 05115 - 0.1552-56.321 . 1.011 - 1.6957-56.79 . 1.910 - 1.6957-56.79 . 1.5306 - 1.8046-56.57 . 1.5306 - 1.8046-56.57

SURFACE COORDINATE DATA

LINE DATA

Z > Z

*

POINT NUMBER

AXIS) AXIS)

(AT 35.894 MITH 'Y'

= . 50623 = . 66601

AA

AREA ABOUT CENTROID

PRINCI PAL SECOND MOMENTS OF

POINT NUMBER	MEANLINE DATA X Y ANGLETHICKNESS	SURFACE COORDINAT	TE DATA P YP
91	-, 24969-57, 334 , C19	794424451	6 - 255
45	8434 27017-57.392	.26448	•
16	3732 - 29048-57,425 - 0222	20641 - 28449	52.
) <del>.</del>	1011 - 1101-24-410 + 6234 2241 - 12012-42-401 - 0247	. 1980 - 1981 3244 - 1824 A	4
13	3425 - 34671-57-364 - 0255	4499 - 34183	
23	638 36762-57.329 .926	575336746 .	2 - 3
57	39650-57.265 . 3275	700737936 .	58°- E
22	41533-57.198 .n284	8259 - 39761	4. 4.
23	42411-57-123 - 0294	9513 - 41612 .	M T
* ¢	++CO3-2/+5C4 - 03303 	3/00 - 4/3/00	1 1
2 6		3257 - 47125	44
27	49854-56.687 . 0330	- 1505- 105t	M - 55 C
52	51694-56.	574850761 .	2 52
53	53524-56.397 .0346	699152564 .	45°- 8
5.	** 35362**56* 232	6233 - 54357 .	30.0
7.2		3413 - 530130 ·	ייי ער ו
33	- 61724-55-656 4376	1948 - 5956	x 6178
70	62414-55,455 . 1362	3129 61330 .	0 - 6349
35	64091-55.259 . 8388	430962984 .	76519
36	65756-55.373 .0394	548864628 .	5 6688
37	67410-54.886 .0399	6665 - 66260 •	56855
<b>1</b> 0	6 3052-54. 738 . 9404	7842 67883 .	8 7 022
55	7 684-54-537 - 6469	9017 - 69496 •	7.267
7 3	** / 2586**** * 1	. 66.171910	5 ( 354
£ 5	/ 3918-74-73 75524-54. 365	51354 - */2554 . 52536 - 74284	5 (514 5 7576
; pr		3706 - 7585t	7887
3	79702-53	5487577433 .	7997
45	81281-53.656 . C	. 8664 - + 4098	8 8156
9	81852-53.534 .1	7212 - 483558 .	88314
47	83417-53.421 .0	6376 62111 .	3 6472
<b>4</b> 0 (	8+975-53.315 . D	9543 \$3560 .	8629
<b>7</b> (	65526-55-21/ 65526-55-21/	60707655234 •	6765
ć	- 01170-170-170 - 1	1913 - ***********************************	0 1 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
25	41322-52. A81 .0	4319 - 89976 .	3 - 9266
53	92996-52,759 -0	65520 - 91554	97455
50	64944 94462-52.697 . 0	6671993125 .	19583
22	95049-52-455 · D	791694689 .	5 9741
<b>1</b> 0 (	. 97638-52, 291	69111 - 96245	- 9897
7	.99157-52.117 .044	7330497792 .	4-1-3052
0 0	16-360.01.	72682-43331	r i
, 5	4 JC TC 0 - JC 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	* X867-4-30021	2-4-0 47-7 3-4-0 54-8
61	. 35249-51, 335 . D43	5046-1,63893	2-1-0660
62	. 35743-54.972 . 042	76225-1.05395	7-1.0809
63	. 35224-50.627 . 642	77401-1-06686 .	5-1.1956
2.5	. 19692-50.568 .041	78571-1.08357	3-1-1131
e o	.11147-50.296 .945	9738-1.09636	585-1-1245
92	516-1.12769-49.990 .040	81046-1-11463	7984-1-167
) #	0007-1-7-1-00-00-00-00-00-00-00-00-00-00-00-00-0	2054-1-101111 - 1	3300 - 1 - 300 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
, d	700-1-10304-4364-000-000-000-000-000-000-000-000-000-0	0 - 14/41-1-6605	00101-1070 001014 4 870
7	5504-1:1:1/554-#5-1/G • 0.56	0 • 666 QT• T=066+	2

POINT	TEANLINE DATA	<b>A</b>	URFACE	NATE DATA
NCS BLK	X T ANGLE INIC	KNESS	SX St	Y.
73	.84935-1.19138-48.931	•03464	.86241-1.17962	.83629-1.20238
7.1		.03289	.87526-1.19564	. 85054-1.21734
72	•	, 03097	.88804-1.21150	. 86484-1.23212
73	. 88999-1. 23713-48.329 . L	• 62886	.90077-1.22753	. 87921-1.24672
74	. 90354-1, 25230-48, 167 . 0	. 02656	.91343-1.24345	. 89364-1.25116
75		• 02406	.92603-1.25935	. 90814-1.27545
76		. 02136	.93856-1.27527	. 92271-1.28958
77	•	01844	.95101-1.29120	. 93735-1.30359
78	•	61529	.96338-1.30717	. 95207-1.31746
79	•	01191	.97568-1.32319	. 96687-1.33121
83	. 98482-1.34237-47.635 . 0	• 60829	.98788-1.33927	. 98176-1.34486
81		. 00442	1.00000-1.35543	. 99674-1.35840

# STREAMSURFACE GEOMETRY ON STREAMLINE NUMBER 18 excesses e

The second second

(BLADE INLET ANGLE.) (BLADE OUTLET ANGLE.) (BLADE LEADING EDGE GADIUS AS A FRACTION OF CHORO.)	(BLADE HAXIMUM THICKNESS AS A FRACTION OF CHORD.) (BLADE TRAILING EDGE HALF-THICKNESS AS A FRACTION OF CHORD.)	(LOCATION OF MAXIMUM THICKNESS AS A FRACTION OF MEAN LINE.) (MERIDIONAL CHORD OF SECTION.)
ж∞54. 96 к≈49.333 к .03129	* .92588 * .01125	F 2.2813
8ETA1 8ETA2 VZERO	T	2 CORO

NDR-MALISED RESULTS - ALL THE FOLLOWING REFER TO ABLADE HAVING A HERIDIONAL CHORD PROJECTION OF UNITY BEG SECONDESSES BECOMES ASSESSED ASS

= 1.7321 STAGGER ANGLE =-54.734 BLADE CHORD

= -5.063 CANBER ANGLE SECTION AREA # . 15363

LOCATION OF CENTROID RELATIVE TO LEADING EDGE

X8AR = .53528 YBAR = -.83422

SECOND NOMENTS OF AREA ABOUT CENTROLD

IX = .03636 IY = .00292 IXY = -.35420

ANGLE OF INCLINATION OF (ONE) PRINCIPAL AXIS TO "X" AXIS = 34.724

(AT 34,724 MITH 'X' AXIS) PRINCIPAL SECOND HOMENTS OF AREA ABOUT CENTROID Dx = .00899 DY = .00011 SURFACE COORD 4ATE DATA MEANLINE DATA
ANGLE THICKNESS Poi ní Nun ner

.0004306131 .0130101986	.0351603610 .0361605600 .0507207754	.0632709737 .0756211747 .6863713780	.1134617989 .126882088 .1385522186 .1511824224
-			-1262217397 -1398019128 -1533921175 -1669723233
• •	• • •		.01512 .01632 .01752
. 0.03600-54.996 131823-94.646	7 03583-35-148 • 05575-55-605 E 37499-56-019	7 0 9452-56, 393 6 11431-56, 7 30 1 13434-57, 2 00	17503-57.527 17503-57.727 21640-57.896 23728-56.035
1 • \$0 224 2 • 01531	3 .02837 4 .04146 5 .55451	6 . 06757 7 . 08064 8 . 09377	10 11986 11 13290 12 14597

OI M	MEANLINE DATA	SURFACE COORDINATE	DATA	
CM GRIP	ANGLE	SX SE	d <b>k</b>	
14	5827-58.	3955 -·	2.	
15	27933-58.223 .	3412 - 2737	-,2	
16	33045-58.274 .	37682946	3	
11	32159-58.297 ·	2124 - 13		
81	34139-56.299	3391 - 3	M I	
61	- 36118-56.266	1020	?!	
ន	- 35595-55-26t - ·	4264	,	
22	- 177 - 95 - 171 - 177	? 4		
16	114 - CY - C	7745	-	
26		4 - 9760		
20	47930-57,949	75.2		
20	-43879-57.846	3495 - 4		
12	51819-57.729	.7535	S	
28	53751-57.598	5 6009		
53	55672-57.453 .	7264 - +5	ŗ	
30	57582-57.293	85175	ŝ	
31	59479-57.118 .	9768 - 5	9.	
\$2	-, 61364-56, 928 .	1018 - 6	9	
33	63234-56.722	2266 - •6	•	
) (i	64985-56.523	3442 - 6	•	
35	- 66722-56.331	4617 - 6	ָ י	
92	65448-56.146 ·			
37	7 3162-25-968	0405 - ed	•	
80 d	-,71864-55,795	81357	•	
gr co	** / 3556-55.635 *	9305	,	
7	- 1 7638 79 465 -	10110 101 10140 101		
10	**************************************	2840 - 27		
M	69229-55-066	3976 - 2		
3	81876-54.945	5141 8		
£5	83517-54.833 .	6305 - •8	;	
9.	85151-54.730 .	74688	:	
14	86779-54.637	8630		
E) (	65401-54-552			
5 (	- 90019-94-477 -	0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 -	, c	
2 2	· MACON LANGUAGE	2143	, ,	
51	1	0.	, ,	
1 M	95555-54-1194-	5737 - 4		
2	96312-53.970	.6692996993		
55	99949-53.633	61209	1.0	
56	1. 31576-53.683	9309-1.0	4	
25	1.03198-53.522	0495~1 0	٠ ب	
20	1. 14506-55.547	1079-1 •U	, ,	
50	1. 06407-53.159	7.020	,	
D.	1.17955-52.956	コードッカウラナ		
61	1.19571-52.743	n• 1-+126		
20	1.11134-5745	0000011 *C		
r d	4 44 004 F0 24 0	1776-1	•	
t u	4.45742-64.777	0875-1-1-1	•	
60	0 10 10 10 10 10 10 10 10 10 10 10 10 10	4480-1-1-1		
200	040 · 24 · 124 · 124 · 17 · 1	2479-1-10	•	
	2247-1-22740-58.854 -0386	X774-1-19		
69	5-1,22439-50,594 0366	.25963-1-21275	. 82229~1 .236B3	
<b>,</b>		***		

. TN TU	A T A O O A T A	SURFACE COORDINATE DATA	TE OATA
TOW BE R	X Y ANGLE THICKNESS	XS YS XR	ΧΡ
7.0	. 44995-1.24073-50.352 .03513		. 83643-1.25193
	•	.87623-1.24625 .	,85063-1,26763
72	•	•	,86490-1,28315
73	•	•	,87923-1,29848
7.	•	•	89362-1.31364
75	•	•	, 90 80 9-1 • 3 2864
76		•	92263-1.34348
7.	•	•	93726-1,35819
78	•	•	95196-1,37276
5.		•	96675-1.38721
) e	•	•	98163-1.40156
. *		•	99661-1.41580

67 (BLADE INLET ANGLE.) 154 (BLADE OUTLET ANGLE.) 155 (BLADE LEADING EDGE RADIUS AS A FRACTION OF CHORD.) 156 (BLADE HAXIMUM THICKNESS AS A FRACTION OF CHORD.) 157 (BLADE TRAILING EDGE HALF-THICKNESS AS A FRACTION OF CHORD.) 158 (LCCATION OF MAXIMUM THICKNESS AS A FRACTION OF MEAN LINE.) 195 (MERIDIONAL CHORD OF SECTION.)	parised result — All the Following refer to Ablade maving a merious electronal chord projection of uni 	ž.	13
# - 56 - 457 # - 50 - 456 # - 60 - 456 # - 60 - 456 # - 669 - 3	- ALL THE	= 1.7825	z-55.923
85141 85142 72590 1 7005 2 6060	PAALISED RESULTS	BLADE CHORD	STAGGER ANG. E =-55.923

¥## Ž.

z . 15593 SECTION AREA CAMBER ANGLE

LOCATION OF CENTROID RELATIVE TO LEADING EDGE

X3AR = .53760 Y3AR = -.83533

SECOND YOMENTS OF AREA ABOUT CENTROLD

ANGLE OF INCLINATION OF CONE) PRINCIPAL AXIS TO "X" AXIS = 33.553

PRINCIPAL SECOND NOMENTS OF AREA ABOUT CENTROLD

io To

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74		•	. 85183-1.32167
7.2	•	•	,86519-1-33793
, M	٠	•	87945-1.35400
7.	-	•	, 89379-1,36989
u.	•	•	. 90823-1.38561
7.6	•	•	. 92269-1:40117
77.	•	.95211-1.43441 .	. 93726-1.41659
	•	•	. 95192-1.43186
7	•	•	. 96668-1.44701
. 180	•	.98818-1.45656	,98153-1.46205
+1 (8)	•	٠	. 39648-1.47697

# STREAMSURFACE GEOMETRY ON STREAMLINE NUMBER 20

(3LADE INLET ANGLE.) (3LADE OUTLET ANGLE.) (3LADE LEADING EDGE RADIUS AS A FRACTION OF CHORD.) (3LADE HAXINUM FHICKNESS AS A FRACTION OF CHORD.) (3LADE HAXINUM FHICKNESS AS A FRACTION OF CHORD.) (1.OCATION OF HAXIMUM FHICKNESS AS A FRACTION OF KEAN LINE.) (4.OCATION OF HAXIMUM FHICKNESS AS A FRACTION OF KEAN LINE.)	NORMALISED RESULTS - ALL THE FOLLOWING REFER TO ABLADE HAVING A MERIDIONAL CHORD PROJECTION OF UNITY  BACK CANCEL CHORD = 1.8373							*X * AXIS = 22.377		AXIS) AXIS)	SURFACE COORDINATE DATA XS YP YP
(BLADE INLET ANGLE.) (BLADE OUTLET ANGLE.) (BLADE LEADING EDGE RADIUS AS (BLADE HAXIMUM THICKNESS AS (BLADE HAXIMUM THICKNESS AS (BLADE TAILING EDGE HAL-THIC (LOCATION OF HAXIMUM THICKNESS (MERIOIONAL CHORO OF SECTION.)	LLOWING REFER TO ABLA			LOCATION OF CENTROID RELATIVE TO LEADING EDGE		T CENTROID		ANGLE OF INCLINATION OF CONE) PRINCIPAL AXIS TO "X" AXIS = 22.377	PRINCI PAL (#COND HOMENTS OF AREA ABOUT CENTROIO	(AT 32,377 MITH "X" AXIS)	N L I N E O A T A Y ANGLE THICKNESS
=-55.463 =-51.933 =-51.933 =-01.127 =-0.127 =-6949 =-2.1145	S - ALL THE FO	==57.371 = -3.533	= .35877	ENTROID RELATI	NBAR = .54020 NBAR =87518	S OF AREA ACOU	= .00794 = .00321 =10533	INATION OF 101	OND MOMENTS OF	= . 61113 = . 40831	M M M
BETA1 BETA2 YZE40 1 TONE 2 COR0	NORMALISED RESULTS	STAGGER ANGLE CAMBER ANGLE	SECTION AREA	LOCATION OF C.	ABAR = Y3AR =	SECOND MOMENTS OF AREA ACOUT CENTROID	######################################	ANGLE OF THOU	PRINCI PAL TO	TP Y	POIN! NUMBER

01318 01318 013318 013868 01462 016415 016415 01632 01534 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01647 01

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5	5 9 645-57-123	5768289632 .533299205	60
46	3 92612-57.368 .044	823791359 .544619383	35
r,	3 9+576-57-327 . 345	33%1 - 93145 - 55594 - 956D	<b>e</b>
4 40	5 96138-57-309 - 345	1545 - ,94999 . 56728 - ,9737	<b>6</b> 0 -
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<b>3</b> 2	3-1.: : \$721-56.658 .046	6779-1-07447 - 64907-1-0999	32
56	3-1-1 5:16-55-547 .046	9951-1.09229 .56087-1.1178	M I
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3	7417-1-2-437-55-313 . 143	79234-1.23149 . 75643-1.2566	55
59	8514-1.26580-54.734 .243	0376-1,24835 ,76853-1,2732	92
Š.	2933-1-514-29-24-414 - 645	1655-1.26715 . 78223-1.2917	군 :
<b>5</b> ;	23765-54-111 - 041	-1.28580 .7960J-1.3396	
e (	29-40-10-51-656-55-629	4198-1.38443	V 5
6.9	59ID-1, 354Id-73,778 , 230	2487-1-92583 • 95310-1-9432	2

POINT	A E A N L I N E O A	4 T A	SURFACE COORDINATE DATA	NATE DATA
NUM BE R	X Y ANGLE THICKNESS	HICKNESS	SX YS	γ _γ
2	. 85241-1.35196-53.305	.03679	.86715-1,34:97	. 83765-1.36295
7.1	. 85555-1. 35966-53, 374	. 13499	.87964-1.35915	,85167-1,38017
72	. 87893-1, 39723-52, 862	. 33299	.89255-1.37727	. 86575-1.39719
73	. 89215-1. 4 1467-52.671	• 03073	.95440-1.39533	.87992-1.41400
7.5	. 90541-1. 42199-52.501	. 02837	.91656-1.41335	. 89415-1.43962
25	. 91865-1. 43921-52.353	. 02573	.92885-1.43135	. 93847-1.44707
76	. 93191-1. 45635-52. 226	. 12286	.94095-1.44935	. 92288~1,46335
77	. 94516-1, 47342-52,122	421974	.95295-1.46736	. 93737-1.47948
7.9	. 95841-1. 49343-52,343	. 01637	.96487-1.48539	. 95196-1.49546
79	. 97167-1.5 1739-51.981	.01274	.97669-1.50337	. 96665-1.51132
60	. 96432-1. 52433-51. 946	. 00884	.98640-1,52161	. 98144-1.52705
61	. 99817-1. 54125-51.933	• 0 0 4 6 5	1.00000-1.53982	. 39634-1.54269

# SIREAMSURFACE GEOMETRY ON STREAMLINE NUMBER 21

事 一日本

(BLADE INLET ANGLE.)
(BLADE OUTLET ANGLE.)
(BLADE LEADING EDGE RADIUS AS A FRACTION OF CHORD.)
(BLADE MAXIMUM THICKESS AS A FRACTION OF CHORD.)
(BLADE TRAILING EDGE MALF-THICKNESS AS A FRACTION OF CHORD.)
(LOCATION OF MAXIMUM THICKNESS AS A FRACTION OF NEAN LINE.)
(MERIDIONAL CHORD OF SECTION.) #-56.539 #-53.539 # # 00125 . 00125 . 00125 . 7038 2. 0273 BETA1 BETA2 VZERO 2080 YORE

MORMALISED RESILIS - ALL THE FOLLONING REFER TO ABLADE MAYING A MERIDIONAL CHORD PROJECTION OF UNITY page assocretes as secretes consecretes essecretes experience extrates as extrates as the transfer as the expertes

BLADE CHORD = 1.8993

STAGGER ANGLE =-58.277

CAMBER ANGLE = -2.667

SECTION AREA * . 06228

LOCATION OF CENTROID RELATIVE TO LEADING EDGE

MBAR = .54388 YBAR = -.91645 SECOND HOMENTS OF AREA ABOUT CENTROLD

IX = .00922 IY = .80339 IXY = -.00558 ANGLE OF INCLINATION OF (ONE) PRINCIPAL AXIS TO "X" AXIS = 31.213

PRINCIPAL SECOND MOMENTS OF AREA ABOUT CENTROLD

IPX = .01263 (AT 31.213 MITH 'X' AXIS)
| IPY = .00001 (AT 31.213 MITH 'Y' AXIS)

MUMBER X A M. L. I. N. E. D. A. T. A.

MUMBER X A ANGLE THICKNESS XS XF YS XF

DIM	LINED	RFACE	NATE DATA
134 BE R	Y ANGLE	X SY SX	
7	639 - 23155-60.854 .9	85462864	2.5
15	21561-60-949	9940 - 3132	
16	33974-61.911 .	1332 - 33	
17	36392-61.043 . [	27243580	
16	35689-61.052 .0	4045 - 3807	21607 3
13	41987-61.348 . 6	5364 - 4034	7
5	+3284-61.033 . C	6683 - 4261	
77.	45579-61.306 .0	5001 - 44	25477
27	- 196-1991	#1/#* - B105	
2 6	C24-60-916	1000 - A4940	
, r	266 • NO - TA+26	1017 - 15181	20. AREA
) k	56.00 CO - 14.00 CO - 15.00 CO -	4572 - 45615	34647
22	59244-69-585	5882 - 5838	328496
28	61493-60-471	7191 - 6061	34082 6
53	63731-60.342	84986282	353176
30	65957-60.201 .0	9803 - 6572	. 6
31	68170-60-345 . 8	111076721	9
35	7,368-59.675	2419 - 6938	
13.3 13.3	72550-59.693	3709 - 7154	40274 1
<b>4</b>	74492-59.522	4873 - 47346	41366
35	76421-59.353	45835 - (755)	#47004
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14	87778-58-619	529906562	492188
24	83642-58.532 .0	541458847	50341 9
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23	34456-58.232	3363-1.0321	59385-1.0
51	35340-56.210 .0	6120+1-45549	69545-1.0
25	19221-58.173 .[	65725-1 -0697	-
53	11099-58-122	99	62871-1.1
ψ.	11972-56-056	65565-1.1371 60320-4.4254	54U55-1+1
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25	17557-57.771	1556-1-1629	
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00	21240-57-504	73872-1.1997	69894-1.2
63	23866-57.347 . (	75025-1 -2180	71074-162
61	24681-57-174 .0	76175-1,2361	72257-1.2
29	26683-56.984 . [	7321-1 -2545	73445-1.2
63	29471-56.776	8462-127	74637-1.2
•	77716-1-31245-56-551 .	126-1-26-6	75554-1.
92	32003-56-397	9730-1.3377	77036-1.3
99	33954-56.329	1993-1.5	
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r B	114-11 33433-33*C03 * 133	0 C+ T - 7 + 1C	

POINT	THAND AND CAMA	SURFACE COORDINATE DATA	CNATE DATA
NUM BER	X Y ANGLE THICKNESS	xs YS	ΧΡ
7.3	.85422-1.41571-55.336 .33797	.86978-1.49483	.83867-1.42659
7.		.88207-1.42393	. 85254-1.44475
72	•	.89427-1.44296	. 86649-1.46269
73		.90640-1.46192	. 38652-1.48043
74	•	.91844-1-49385	. 89464-1.49797
75		.93039-1.49973	•
76	. 93271-1. 52555-53. 964 . 12362	.94225-1,51860	•
7.2	•	.95401-1.53747	•
78	•	.96567-1.55635	. 95204-1.56639
62	•	.97723-1.57525	. 96564-1.58304
. <b>4</b> 0	.98501-1.59688-53.566 .00909	.98867-1.59418	. 98135-1.59958
) <b>6</b> ;	•	1.00000-1.61317	. 39618-1.61599

# BLADE SURFACE GEOMETRY IN CARTESIAM COORDINATES AT SPECIFIED VALUES OF "Z"

# SECTION NUMBER 1 'Z' = 2.5000

SECTION PHOPERILES	SECTION AREA LOCATION OF RELATIVE TO	REA OF CENTROID TO STACK AXIS	XBAR YBAR		5.8568E-01 2.0291E-02 1.3603E-02			
	SECOND MONENTS #BDUT CENTROLD	MENTS OF AREA	****	1 H H D	2.5256E-02 2.4836E-01 -1.1407E-02			
	PRINCIPAL OF AREA A	PRINCIPAL SECOND MOMENTS OF AREA ABOUT CENTROID	IP X AI	11 41	2.4674E-02 (AT 2.4894E-01 (AT	-2.92 DEGREES TO -2.92 DEGREES TO	XX.	AXISS
	TORSIONAL CONSTANT	CONSTANT			1.0203E-02			
SECTION COORDINK FES	٠.							
2	я	75	€.		g.			
	-1.43679E+00	6.33176E-01	-5.45084E+03	6	6. 059 66E-01			
	-1.39618E+00 -1.35580F+00	6.06838E-01	-1,61494E+0	9 5	5.72801E-01			
	-1.31550E+00	5.±.508E-01	- 1. 34040F+9.0	9 6	5. 067 95E-01			
	-1.275 JOE+00	5.290006-01	-1.30 339E+D	2	4.73919E-01			
	-1.23440E+30	5.03292E-01	-1.26624E+03	00	4. 410 69E-01			
	17* TO 200E FO	40-100001-04 4:6207-04	-4-404E2E40	7 6	7 75 4 48 F = 0 4			
	-1.11138E+00	4.265878-01	-1.153915+0	90	3.42662E-81			
	-1.07190E+00	4.01163E-01	-1.11613E+0	5	3.89956E-01			
	-1.02998E+00	3.75928E-01	-1.07814E+00	9 6	2. 77321E-01			
	-9-47 B67E-01	3, 25971E-01	-1.00156E+00	9 9	2, 125 61E-01			
	-9.06850E-01	3.01452E-01	-9.62930E-01	9	1.80512E-01			
	-6.65904E-01	2.77379E-01	-9.24061E-01	-01	1.48712E-31			
	-6.25672E-01	2.53782E-01	-8.84941E-01	<del>,</del>	1.174755-01	-		
	-7.49577E-01	2.11665E-01	-6.11339E-01	1 4	6. 071 92E-02			
	-7.15064E-01	1.934106-01	-7.77.174E-01	10	3.53477E-02			
	-5.80867E-01	1.758435-01	-7.43062E-01	4	1.06250E-02			
	-5.43646-01	1.42725F-01	- / . USUUOE-U	4 -	-1. C03 /1E-UC			
	-5.80198E-01	1.27366E-01	-6.41377E-01	5	-5.61747E-02			
	-5.47284E-01	1.12727E-01	-6.07220E-01	10.	-7 . 95938E-02			
	-5.14690E-01	9.88267E-02	-5.734416-01	70	-1. 00138E-01			
	-4.82416E-01	8.56370E-U2	-5.39748E-01	<b>7</b>	-1.19833E-01			
	-4-188475-04	6.45%45FF	- 4. 72 646F-0 1		-1 - 156 A 17 F - 0 1			
	- 3-87464E-01	5-05329E-02	-4.39254E-01	4	-1.73997E-01			
	-3.56420E-01	4.02423E-02	-4.05980E-01	14	-1.90319E-01			
	-3.25668E-01	3.06210E-02	-3.72633E-01	0.	-2.05771E-01			
	-2.95197E-01	2.194.82E-32	-3.39626E-01	50	-2.20311E-01			
	-2.6503E-01	1.36692E-02	- 3. 05954F-0	H 7	-2. 556 /9E-U1			
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dx dX	40 0 0 9 E - 0 1 - 2 + 59 6 3 6 E - 0	1.73541F=01 A1670F=0	4.40454E-04 -7.9129E-0	07537E-01 -3.00198E-0	7.47684E-02 -3.08243E-0	4.21563E-02 -3.15311E-0	70 873E-03 -3. Z1 239E-0	C2000E-02 -3.20K75F-0	55 68 35 - 0 - 3 - 30 50 50 50 50 50 50 50 50 50 50 50 50 50	18276E-01 -3.36246E-0	49779E-01 -3.37330E-0	81067E-01 -3.37512E-0	12134E-01 -3.36857E-0	42066E-01 -3.34667E-0 71803F-01 -3.31772E-0	01256E-01 -3.27205E-0	384186-61 -3.216956-0	59256E-01 -3.15307E-0	67736E-01 -3.07651E-0	43468E-01 -2.87450E-0	70642E-01 -2.75783E-0	97 296E-01 -2.63133E-0	23.388E-01 -2.491.23E-0	736555-01 -2.14642E-0	97.743E-01 -1.96381E-0	21059E-01 -1.77002E-0	43546E-01 -1.56248E-0	50 325E=01 -1. 26 / 42E=0 16 955F=01 -9. 90 842F=0	53496E-01 -6.82216E-0	90 0046-01 -3.381106-0	26530E-01 6.71665E-0	65 2845-01 4.745 395-0 00 8956-01 9.167 096-0	37 301E-01 1.40210E-0	74937E-01 1.94236E-0	ULOIMETOU CAMMONULO	09175E+00 3.73775E-0	13247E+00 4.42531E-0	17433E+00 5.14448E+0	1.21750E+00 5.90684E-01 1.26215E+00 6.71369E-01							
YS	1.69691E-0	4.44.096-0	2. 03272E-D	2.53521E-9	2.94111E-0	3,29182E-0	3.61523E-1	3.0315CE -0	4. 25437F-0	4.31664E-0	4.335746-0	4. 31147E-0	4.22010E-3	02949E-0 73845F-0	3.389396-0	2.997 24E-0	2.541546-0	1.93778E-0	5.43468E-0	31115E-0	06581E-0	02848E-0	42979E-0	63283E-0	92119E-0	3 <b>3527E-</b> 9	0-1606CC	4.18235-0	63426E-0	90839E-0	19191E-0	82662E-0	21022E-0		51122E-0	02850E-0	57525E-0	6.16159E-01 6.79330E-01	VSFNT	05986E-0	0-398698	6.08122E-01	197535-0	12219E-0	13764E-0
SZ.	03586E-0	4 - 42 A 95F-0	1.128155-8	29120E-0	5.31839E-0	2.36337E-0	747355-0	0-305251	28.37.26.10	215385-0	590196-3	78333E-0	06477E-0	53539E-0	86683E-0	12810E-0	30629E-0	54128E-8	14130E-0	38 61 86-0	52747E-0	865 )2E-0	32 6.15F-0	55326E-0	77 390E-0	989646-0	55 55 9E-0	04 2 8 2 E - 0	39960E-0	760495-0	10001E-9 19965E-3	BB315E-0	0-309692	88 42 4F+0	05 0 9 1 E+0	09519E+0	14131E+0	1.24034E+00	KSEHI	1.45084E+0	1-451988+8	5.302E	1.4547964	1.455495+0	1.45636E+8
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(C) # (C) # (F) #	XBAR XIV AR IPX Y	XP -1.46520E+03 -1.42873E+03 -1.3556E+00 -1.3556E+00 -1.2823E+03 -1.20673E+03 -1.17178E+03
+00 6.172E-01 +00 6.17025E-01 +00 6.27293E-01 +00 6.23724E-01 +00 6.23724E-01 +00 6.23724E-01 +00 6.2337E-01 +00 6.2837E-01 +00 6.2837E-01 +00 6.2837E-01 +00 6.2837E-01 +00 6.38946E-01 +00 6.38946E-01 +00 6.38946E-01 +00 6.38546E-01 +00 6.38546E-01 +00 6.38546E-01 +00 6.38546E-01 +00 6.38546E-01 +00 6.38546E-01 +00 6.38546E-01 +00 6.3874E-01 +00 6.3874E-01 +00 6.3874E-01 +00 6.3874E-01 +00 6.3874E-01	LOCATION AREA LOCATION OF CENTROID RELATIVE TO STACK AXIS SECOND MOMENTS OF AREA ABOUT CENTROID PRINCIPAL SECOND MOMENTS OF AREA ABOUT CENTROID TORSIONAL CONSTANT	YS 7.47523E-01 7.17393E-01 6.8769E-01 6.2969E-01 6.0160E-01 5.4639E-01 5.4639E-01
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**	ECTION PROPERTIES	ECTION COORDINATES POINT NO 2 2 3 5 7 7 9

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POINT NO	XS	YS	d _X	d.
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13	93525+0	ò.	0434/461	1904061
#	53376+0	• 656 90E - 0	1.09759E+0	80531E-0
27	14 4 5 0 E+0	.39524E-D	1.06032E+0	. 537 98E-0
77	41825-0	756-0	1. 02292E+1	21505E-3
#	4241E-0	890 J9E-0	9.85360E-0	895 00E-0
51	4290E-0	527 0 3E-0	47 623E-0	577 51E-0
51	4347E-8	37830E-0	9.09692E-0	263 23E-0
<b>3</b>	44385-0	133 BBE-D	71549E-0	95358E-0
9	8155E-0	31583E-0	36531E-0	. 67479E-0
2	2115E-0	73383E-0	R. 01522E-0	40138E-0
₹	6 327E-0	19803E-0	7.66525E-0	13423E-0
ಸ	-6.70796E-01	2.29826E-01	-7.31543E-01	8. 73933E-02
Ħ	15531E-0	134708-3	6.96579E-0	. 20 2 36 E-0
23	13 5 35E-0	917 97E-0	6.61637E-0	. 728 93E-0
ž	58135-0	73805E-0	6.26722E-0	32703E-0
ß	11367E-0	56509E-0	5.916405-0	. 992 39E-1
8	71995-0	398 62E-0	5.56996E-0	24746E-0
23	3311E-0	23952E-0	5.22194E-0	41916E-0
<b>8</b> 2	973E-0	19729E-0	4.8744E-0	51570E-0
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£	3321E-0	0-300Z40	4. 18 122E-0	. 146 28E-9
ĸ	13 543E-0	73775E-0	3.83567E-0	. 330 39E-0
32	130345-0	49742E-0	3.49094E-0	. 507 06E-0
17	5791E-0	324572-0	3.14711E-3	6744E-0
ä	3547E-0	239365-0	2. 80 293E-0	83463E-0
K	115425-0	16291E-0	2. 45 954E-0	96650E-0
<b>3</b>	96545-0	1.8466F-0	2.11705E-0	12957E-0
4 €	17071F-8	344EES	1-77552E-0	26353E-0
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i d	74.3.39E-0	7.03511E-0	78 380E-0	24627E-0
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6	3634E-0	6-E56285-0	98 87 9E-D	06514E-0
3	101536-0	5.68312E-0	26 091E-0	99312E-0
3	16375E-0	5.19525E-0	56 86 3E-0	90 8 30 5-0
3	2255E-0	4. 552.07E-9	05153E-0	. 80 6 16E-t
29	17 7 8 2 E - D	7.79190E-0	129146-0	. 68376E-0
3	12949E-0	3.647436-0	40 114E-0	. 55669E-0
3	17733E-0	21535E-0	56701E-0	. 42184E-0
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69	.997526-0	• 49527E-9	37 296c-0	34597E-3
92	. 34 B66E-0	+55017E-0	73367E-0	. U3195E-U
7	.70416E-8	. 7:35 0 7E -3	09526E-0	11192E-0
72	0-306790°	.13228E-0	45 822E-0	, 60 3 81 E-0
73	.43171E-0	.36283E-0	52 327E-0	70774E-0
ż	. 83554E-0	• 66276E-0	01 31 32+0	. 59493E-0
72	.01881E+0	•97929E-0	05632E+E	07751E-0
76	. 058:3E+0	. 32154E-D	09401E+0	. 39297E-0
72	.09637E+0	•63792E-0	13230E+0	. 317 30E-8
78	•13999E+0	.11337E-0	1733E+0	, 48061E-0
62	.18338E+0	.55530E-1	21 11 TE+0	, 07255E-C
<b>6</b>	.22781E+0	.03173E-0	258231E+0	, 70251E-3
51	.27 441E+0	4719E-3	29.397E+0	37194E-0
POINT NO	XSEMI	<b>ASEMI</b>		
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91	.46724E+0	.45305E-0		
17	.46654E+0	* 46249E-0		
<b>9</b> 1	.46577E+0	.47104E-0		
<b>6</b> 7	.46432E+0	.47861E-0		
S	. 464 11E+0	.48511E-0		
ฆ	.463J4E+0	.49847E-3		
8	462:3E+0	0-349464.		
53	1.450985+0	.43757E-0		
24	45 991E+0	.49922E-0		
£	45 683E+0	0-385664*		
8	45776E+0	.49863E-D		
23	45669E+0	0-304964*		
82	.45565E+0	0-306264.		
æ	45465E	48816E		
2	.45369E+0	.48225E-0		
31	5279E+0	.47523E-0		

# SECTION NUMBER 3 '2' = 3.5189 errererere

X	SECTION PROPERTIES			द्ध			
KS YS  -1.476.2E-00 8.759.2E-01 -1.48.076E-01 8.6572E-01 -1.39.29E-00 8.759.2E-01 -1.48.076E-01 8.2572E-01 -1.39.29E-00 8.759.2E-01 -1.48.076E-01 7.4712E-01 -1.39.29E-00 7.702E-01 -1.39.06E-01 7.4712E-01 -1.39.29E-00 7.702E-01 -1.39.06E-01 7.4712E-01 -1.39.29E-00 7.702E-01 -1.39.06E-01 7.4712E-01 -1.39.29E-00 7.702E-01 -1.39.06E-01 7.4712E-01 -1.39.29E-00 6.5132E-01 -1.39.06E-01 7.4712E-01 -1.39.29E-00 6.5132E-01 -1.39.06E-01 7.4712E-01 -1.39.29E-01 6.5132E-01 -1.39.06E-01 7.4712E-01 -1.39.26E-01 6.5132E-01 -1.39.06E-01 7.4712E-01 -1.39.26E-01 6.5132E-01 -1.39.06E-01 7.4712E-01 -1.49.36E-01 6.5132E-01 -1.39.06E-01 7.4712E-01 -1.49.36E-01 6.5132E-01 -1.39.06E-01 7.4712E-01 -1.49.36E-01 6.5132E-01 -1.39.06E-01 7.2540E-01 -1.40.36E-01 6.59.4E-01 -1.306E-01 7.2540E-01 -1.40.36E-01 6.59.4E-01 -1.406.4E-01 7.206.6E-01 -1.40.36E-01 6.59.4E-01 -1.406.4E-01 7.206.6E-01 -1.40.36E-01 7.209.4E-01 7.206.6E-01 7.206.6E-01 -1.40.36E-01 7.209.6E-01 7.206.6E-01 7.206.6E-		SECOND NO ABOUT CEN PRINCIPAL OF AREA A	HENTS OF AREA FROID SECOND MOMENTS SOUT CENTROID		2.0468E-02 2.1601E-01 -6.0196E-02 1.0610E-02 (AT	-16.35 BEGREES TO	
YS		TORSIONA	CONSTANT		4.7219E-03	•	
## NO KS  ***********************************	COORDINATE	<u>v</u>					
1 -1.47862E+00 8.75928E-01 -1.48876E+01 2 -1.43840E+00 8.42611E-01 -1.45238E+01 3 -1.35829E+00 8.42611E-01 -1.45238E+01 4 -1.35829E+00 8.42611E-01 -1.45238E+01 4 -1.35829E+00 8.44719E-01 -1.45238E+01 4 -1.49939E+00 8.44719E-01 -1.423408E+01 4 -1.49939E+00 8.44719E-01 -1.423408E+01 4 -1.49939E+00 8.59948E-01 -1.4376E+01 4 -1.49948E+00 8.59948E-01 -1.4376E+01 4 -1.49948E+00 8.59948E-01 -1.4376E+01 4 -1.49948E+00 8.59948E-01 -1.4376E+01 4 -1.49949E+00 8.59948E-01 -1.4376E+01 4 -1.49948E+00 8.59948E-01 -1.4376E+01 4 -1.49948E+00 8.59948E-01 -1.4376E+01 4 -1.49948E+00 8.59948E-01 -1.4385E+01 4 -1.49948E+01 8.79948E-01 -1.4385E+01 4 -1.49948E+01 8.79948E-01 -1.4385E+01 4 -1.49948E-01 8.79948E-01 -1.4385E+01 4 -1.49948E-01 8.79948E-01 -1.4385E-01 4 -1.49948E-01 8.7773E-01 4 -1.49948E-01 4 -1.49948E-01 4 -1.49848E-01	POINT N		rs.	d _X	ğ.		
2 -1, 39 & 29 & 29 & 47 & 50 & 47 & 47 & 48 & 48 & 47 & 48 & 48 & 48	=1	-1-478625+00	8.75928E-01	-1.48876E+			
6 -1.35627E+01 7.77620E+01 -1.37966E+01	∾ ≠	-1. 436+0F+05	6,42611E-31 A. 69677F-01	-1.45238E+	, .		
5 -1.318 34E + 10 7 - 447 19E - 11 - 11 74 30 10 + 10 7 10 10 10 10 10 10 10 10 10 10 10 10 10	*	-1.35627E+00	7. 770 20E-01	-1.37 966E+	7.		
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4 1.199 15E 40 6.51125E - 01 - 1.23400E + 0 1 1.199 15E 40 6.51125E - 01 - 1.197 15E + 0 1 1.197 15E + 0 1 1.197 15E + 0 1 1.199 15E + 0 1 1.197 15E + 0 1 1.197 15E + 0 1 1.197 15E + 0 1 1.199 15E + 0 1 1.1	<b>.</b>	-1.27.852E+0.0 -4.248.745+0	7.12738E-31 6. 81192E-01	-1.30693E+	e d		
9 -1.15943E+00 6.19529E-01 -1.19179E+0 1 11 -1.100192E+00 5.599443E-01 -1.16102E+0 1 12 -1.00039E+00 5.599443E-01 -1.16102E+0 1 13 -1.00195E+00 5.59943E-01 -1.0004E+0 1 14 -1.00195E+00 5.5195E-01 -1.0004E+0 1 15 -1.00195E+0 5.5195E-01 -1.0004E+0 1 15 -1.00195E+0 5.5195E-01 -1.0004E+0 1 16 -1.00195E+0 5.5195E-01 -1.0004E+0 1 17 -1.00195E+0 5.5195E-0 1 -1.0004E+0 1 18 -1.00195E+0 5.5195E-0 1 -1.0004E+0 1 19 -1.00195E+0 5.5195E-0 1 -1.0004E+0 1 19 -1.00195E+0 5.5195E-0 1 -1.0004E+0 1 10 -1.00195E+0 5.5195E+0 1 -1.0004E+0 1 10 -1.00195E+0 5.5195E+0 1 -1.0004E+0 1	. •	-1.19919E+02	6.51125E-01	-1.23 406E+			
13 -1.1498E+CD 5.89946E=01 -1.2438E+00 1.2 -1.00039E+00 0.5 59946E=01 -1.00030E+00 0.5 59946E=01 -1.00030E=01 0.5 5956E=01 0.5 595	•	-1.15943E+00	6.19529£-01	-1.1975eE+			
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13 -1.01572.00 5.02600E-01 -1.0500E-01 14 -3.62235E-01 4.74807E-01 -1.05003E-01 15 -8.6363E-01 4.476807E-01 -9.75765E-01 16 -8.6363E-01 1.94807E-01 -9.39536E-01 17 34.6418E-01 3.94807E-01 -9.39536E-01 21 -5.6952E-01 3.95940E-01 -9.65866-01 22 -5.657336E-01 3.95940E-01 -9.65866-01 23 -7.3469E-01 3.526346E-01 -9.65866-01 24 -5.695297336E-01 3.526346E-01 -5.69656-01 25 -5.695336E-01 2.99477E-01 -5.69656-01 26 -5.47646E-01 2.99477E-01 -5.69656-01 27 -5.69526E-01 2.99677E-01 -5.69626E-01 28 -5.47646E-01 2.99677E-01 -6.48626E-01 29 -5.47646E-01 1.77636E-01 -5.75665E-01 29 -5.47646E-01 1.7736E-01 -5.75665E-01 20 -5.47646E-01 1.7736E-01 -5.75665E-01 20 -5.47676E-01 1.7736E-01 -5.75665E-01 20 -5.477676E-01 1.7736E-01 -5.75665E-01 20 -5.47676E-01 1.7736E-01 -5.75665E-01 20 -5.47766E-01 1.7736E-01 -5.75665E-01 20 -5.47776E-01 -5.75665E-01 -5.75665E-01 20 -5.47776E-01 -5.75665E-01 -5.75665E-01 20 -5.47776E-01 -5.75665E-01 -5.75665E-01	12	-1.046365+00	5.33936E-01	-1.08765E+	• •		
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						-21.85 DEGREES TO "X" AXIS) -21.85 DEGREES TO "Y" AXIS)				
			4.3507E-31	1.5621E-03 *,3085E-33	4.02256-02 2.11646-01 -8.19776-02	7.3590E-03 (AT	3,5964E-13	ş	ž	1, 90162E+03 9-6236E-01 9-2148E-01 6-6069E-01 7-61856E-01 7-61856E-01 7-61876E-01 7-61876E-01 7-61876E-01
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TREME	6.64966E-31 6.74966E-31 6.7496E-01 8.7266E-31 8.7266E-31 8.7266E-31 8.7266E-31 6.7367E-31 6.7567E-31 8.7567E-31 8.7767E-31 8.7766E-31 8.7766E-31 8.7766E-31 8.7766E-31 8.7766E-31 8.7766E-31 8.7766E-31 8.7766E-31 8.7766E-31 8.7766E-31	SECTION MUMBER & 12' K 4.0000 exception	₹ 9	LOCATION OF CEMPACIO RELATIVE TO STACK AXIS	Second Maren's of Area About Centrold	PAINCIPAL SECOND NONENTS OF AREA ABOUT CENTROLD	CONSTANT	3	£	A. C.
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サーマー 大田人

### ECTION NUMBER 5 "Z" # 4.5333

AXIS) AXIS)

			S DE GREES TO "X"																														
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4.31.34E-01	-6.9821E-0	5.9258E-02 2.1181E-01 -1.0537E-01	5.4513E-03 2.6562E-11	3.3032E-3		<b>d</b>	1 156C4E+0		+		3 4.33566E=0				1 6.92371E-01		0 6.14336E-01					m i	1 3. C444/E=01	N	N		: -:	4		÷ ,	1 1.99386E-0 4 -6.50582E-0		1 -5.53096E-0
u	XBAR #	1X 2Y 1X Y	E XeI	u		×	-1.53528E+3	-1.46218E+3	2 531E+0	-1.38856E+3	39 1916 • J	-1.27.894€+1	-1.242615+93	-1.20639E+33	-1.13422E+0	-1.09825E+0 )	-1,06232E+03	-9.93518E-0	-9.54595-0	-9, 17 990E-0	-8.44576E-1	-8-07750E-9	-7-13825F-3	-6.967105-0	-6.59463E-21	-6.22138E-3	-5.47067E-01	-5.09334E-0	6.71472E-0	4. MG 487E-0	- 3-95354E-0 - 3-57168E-0	3.202216-0	-2.83193E-0
<b>131</b>	OF CENTROLD TO STACK AXIS	PENTS OF AREA	PAINCIPAL SECOND MOMENTS OF AREA ABOUT CENTROID	COMSTANT		S.A.	1-165 25-6"	4.09629E+33	1.0+725E+0J	1,0%51E+03	9. X2028F-01	8.944 36E-31	8.57325E-31	5.2 J696E-31	7.43091E-31	7-1-1865-11	6.73877E-01	6.13060E-31	5.6.6202-31	5.43246E-11	6.85294E-01	4.5-752E-01	4,24846E-J1	3.658446-31	3.387536-11	3.11307E-01	2.56338E-01	2.327 87E-01	2.079.17E-11	1.63762E-01	1.674.875-01	1.161328-01	9.541875-32
SECTION AREA	LOCATION CRELATIVE 1	SECOND MOMENTS ABOUT CENTROID	PATHCIPAL OF AREA AG	TORSIONAL CONSTANT		Š	-1.528 9E+36	-1.4-6242+36	05+3555-4-1-	90+30:591-	10-340424-1-	39+36+42*1-	-1.20 +72E+33	-1.155185+66	-1.03077E+30	-1.3478E+2E	-1,003172+36	- 3, 32 2 4 3E - 0 1	-9.939995-01	- 5.55 1395 - 54 - 5.55 335 - 54	-7.77726E-41	-7.39121E-C1		-5.236415-11	-5.853135-31	-5.469855-31	-+. 75 +58E-31	-+-322325-01	-7.941916-32	-3.561:35-31	-3.181916-31	-2.438+8E+31	-2.074462-31
SECTION PROPERTIES					SECTION COORDINATES	ON INICA	<b>~</b> 6	<b>.</b> •n	91	un v	۰ ۵	. •	Φ.	B (	2 C	11	e u	<u>9</u>	<b>. .</b>	m g	: X	# 60 E	7 %	స	£	26 25	. <b>6</b> 0	\$	25	i i	24 17	) <b>3</b>	22

dA dX SA	556454E - 12 - 12, 40, 50, 50, 50, 50, 50, 50, 50, 50, 50, 5	2.51764E-01 1.32155E+0] -3.14463E-0 2.35445E-01 1.3552E+0] -2.91038E-0 2.19328E-01 1.35943E+0] -2.65340E-0 YSEMI 1.15634E+0] 1.15634E+0] 1.15767E+0] 1.15767E+0]
KS		30853E+0 37759E+0 XSEMI 53671E+0 53754E+0 53767E+0
ON TRIO	\$1444777738888888888888888888888888888888	7.9 6.0 6.0 6.0 7.4 8.4 8.4 8.4 8.4 8.4 8.4 8.4 8.4 8.4 8

		-31.10 GEGREES TO *X*
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άχ	9.63531E-U1 1.02537E+U1 1.06331E+U1 1.15327E+U1 1.15327E+U1 1.27980E+U1 1.27980E+U1 1.32131E+U1 1.40240E+U1 1.40240E+U1 1.447976E+U1 1.47976E+U1	
¥S	-4.2828E-01 -4.28288E-01 -4.54851E-01 -4.52831E-01 -4.54651E-01 -4.5465E-01 -4.6546E-01 -4.72308E-01 -4.72308E-01 -4.72308E-01 -4.76346E-01	YSENI 1. 30375E+00 1. 30575E+00 1. 30575E+00 1. 30527E+00 1. 30537E+00 1. 30537E+00 1. 30537E+00 1. 30537E+00 1. 30537E+00 1. 30537E+00 1. 30537E+00 1. 30537E+00 1. 30537E+00 1. 30527E+00 1. 31151E+00 1. 31257E+00 1. 31257E+00
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## ECTION NUMBER 7 "Z" = 5.5000

'X' AXIS)

SECTION PROPERTIES	SECTION AREA	REA	*	4.1420E-J1	
	LCCATION RELATIVE	OF CENTROID TO STACK AXIS	XBAR = YBAR =	9,4696E-13 -1,9512E-03	
	SECOND MOMENTS ABSUT CENTROLD	MEMIS OF AREA TROID	H H H	1.0978E-01 2.0981E-01 -1.4871E-01	
	PRINCIPAL OF AREA AB	MCIPAL SECOND MOMENTS AREA ABOUT CENTROID	IP X P dI	2.8963E-03 (AT -35.71 3.1669E-01 (AT -35.71	1 DEGREES TO
	TORSIONAL CONSTANT	CONSTANT	u	2.4255E-13	
SECTION COCROINATES					
POINT NO	Ş	S.A.	d X	Ē	
ų.	-1.52326E+00	1.443425+00	-1.53719E+0	3 1,9 436 22E+0 3	
<b>N</b> I	+1.48958E+00	1-4-01.39E+33	-1.501112+3		
n j	-1.41.23E+00	1.316735+00	-1.42962740		
, rv	-1.37 25 3E+0 B	1.27423E+03	-1.39446E+3		
Φ!	-1.33499E+00	1.23179E+03	-1.35981E+0	4.	
<b>&gt; «</b>	00+355592-1-	1,19935E+01 1,14716E+00	-1.291575+0	3 1.16263E+90	
· •	-1.22360E+0#	1-115246+09	-1.25773E+0	: 4	
다 <b>.</b>	-1.186592+00	1.06367E+00	-1.22387E+0	~ 6	
7	-1-141835-00	1. 022495.03 9. 816775-01	-1-109635+0	, ,	
17	-1.37395E+30	9.41247E-01	-1.12067E+0	80	
44	+1.03572E+00	9.012098-01	-1.08584E+3	~ 6	
3 2	-9.58386E-01	8-22176E-01	-1.01471E+0	3 7.64683E-01	
4	-9.13421E-01	7.831516-01	-9.78678E-0		
<b>49</b> 0	-8.61989E-01	7.45187E-01	-9.43100E-01	1 6.81968E-01	
	-8-842115-01	6.7.1147E-01	- 6.71332E-0		
រ	-7.65729E-01	6.33127E-01	-6.35202E-01	1 5.59382E-01	
3 2	-6-88747E-31	5.633535-81	-7.62526E-01	_	
នឹ	-6.52259E-01	5.24631E-01	-7.25987E-01	*	
3	-6.11775E-01	4.89353E-01	-6.89311E-01	•	
92 (	-5.73294E-01	4.54665E-01	-6.52494E-0	, ,	
22.52	-5-34B14E-07	3.86969E-01	-5.78424E-01	1	
52	-4.5785E-01	3.53987E-01	-5.41160E-0	. +	
C) .	-6-19378E-31	3.21653E-01	-5.03740E-0		
z C	-3.01 9.14E-31	2. Kan. 25 - 11	-4.001055-U1	1 1.040001111	
2 12	-3.039556-01	2,263465-01	-3.90546E-0	•	
<b>4</b> 1	-2.66547E-01	1.99392E-31	-3.53561E-0	6	
ß	-2.29139E-01	1.73822E-31	- 3.16485E-0	1 5.46130E-12	

dA dx	-2.79319E-01 -5.6528E-02 -2.4259E-01 -5.6528E-03 -2.04769E-02 -1.594769E-02 -1.594769E-02 -1.5958E-03 -2.5453E-03 -2.5453E-03 -2.5453E-03 -2.5453E-03 -2.54569E-03 -1.5958E-03	
SA		1.6 436.52E +0.0 1.6 436.52E +0.0 1.6 437.3E +0.0 1.6 438.15E +0.0 1.6 438.15E +0.0 1.6 438.15E +0.0
ឌ	T. EE TOOL EE EN HOLD EN EE EN LANDER EN EN LANDER EN BEKENDER FORDEN FO	ASENI -1.53719E+00 -1.53754E+20 -1.53878E+00 -1.53878E+00 -1.53878E+00 -1.5384E+00 -1.5384E+00
POINT NO	*************************************	7 2 2 3 40 19 4 16 10 10 10 10 10 10 10 10 10 10 10 10 10

	-01 -02 -04 -01 -01 -01 -03 (AT -40.55 DEGREES TO "X" AXIS) -03 (AT -40.55 DEGREES TO "X" AXIS)	YP 1.54036E+00 1.45036E+00 1.4527F+00 1.4527F+00 1.3514E+00 1.2539E+00 1.2771E+00 1.13139E+00
·	3.8436E-01 -1.2015E-02 -5.253E-04 1.3113E-01 1.7856E-01 -1.5144E-01 1.5556E-03 3.0814E-03	44444444444444444444444444444444444444
		XP -1.49846E+0] -1.4532E+0] -1.43641EE+0] -1.50641EE+0] -1.30641E+0] -1.3041E+0] -1.3041E+0] -1.20426E+0] -1.20426E+0]
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		LOCATION (	LOCATION OF CENTROID PELATIVE TO STACK AXIS	XB AR YB AR	= 1.8416E-03		
		SECOND HONEMS	FENTS OF AREA	222	* 1.5472E-01 * 1.5472E-01		
		OGINCIPAL OF AREA AS	PAINCIPAL SECOND HOMENTS OF AREA ABOUT CENTROID	× 43	# 9.3916E-34 (AT	F -44.55 DEGREES TO "Y" AXIS) F -44.55 DEGREES TO "Y" AXIS)	
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Αb	. 26972E+J	. 2224/E+D	. 17513E+U	. 127 74E+0	0 + 13 CO 0 0 CO	* 63 5 6 5 6 4 5 85 8 22 7 1 2	. 41636E-3	. 97613E-3	. 537 70E-0	. 10138E-0	. 667 37E-3	• 235 63E-J	6. CAC 225-01	957265-0	. 537 38E-0	. 120 78E-0	. 707576-3	. 236 115-0	. 89256E-3		70235E-4	. 315 05E-J	. 93184E-0	. 55259E-3	. 177 27 6-3	. 05234E-J	. 365 61E-0	7 . 13962E-0		13475F-3	357755-0	. 7. 7 95E-3	. 05540E-3	. 40019E-0	.74253E-0	- 096 AFE	796446-0	. 144 96E-0	. 46 8 85E-3	• 62991E-D	. 15773E-3	, 51211E-0	U-342660	. 151 05E-0		0-36000	7-433825-0	7.4666.0	7 + 7 + 1 to 2 to	36323E-0	. 67668E-3
ě,	1.06950E+	1.038722+9	1.00 782E+9	7.757865-3	5-11770C***	A. A	8.53252E-3	9.23491E-0	7-936385-0	7.63695E-0	7. 33482E-9	7. 03 24 3E - 9	-6.726665-31	6.44446	5-611405-9	5. 50 3335-0	5-19416E-0	4. 88 3895-3	4.57.255E-0	4,94666	3-633755-0	3.31988E-3	3.03510E-3	2.689452-0	2. 37 295E-0	2.05564E-0	1.73757E-0	1.418765-0	7.791765-0	4.582675-0	1.366585-3	.851185-0	.076285-0	306425-0	.15413E-0	#2 1/2010 #2 006 11	16 37 45-3	-59806E-3	. 84 792E-3	. 18 835E-J	529375-3	. 67 096E-0	C1 32 15 - U	197666E-0	21100100	0 1 1 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	- 20 40 46 FF	300000	62 68 35-3	996586	698£~3
4.8	£+3655£	5028E+9	14 BBE +0	15943E+3	1.4 3.5 5 6 1 1 4 1.4 3.5 5 6 7 8 7 8	. 10000cr • 0	610195-3	35834E-0	.96833E-1	. 550 F M - 3	. 23389E - 7	720166-3	7. 53903E-32	C = 340 Sept.	- 348.260	. 692 92E - 3	.236965-0	.934625-3	• <b>515 505 - 3</b>	704 464	373545	0 31776-0	633296-1	.267765-9	935446-3	54613E-3	15976c-3	. 353 65E - U	4489975-1	2. 5.17.34E-1	5.55126E-0	8.97475E-3	1.23792£-3	1.576635-3	1.916.15-3	2, 6,11,1 TF =1	2,957 655-9	3.330945-3	3.64260E-7	3.952552-1	4. 31966E -0	6-14-2-44-6 6-14-2-44-6 6-14-2-44-6 6-14-2-44-6 6-14-2-4-4-6 6-14-2-4-4-6 6-14-2-4-4-6 6-14-2-4-4-6 6-14-2-4-4-6 7-14-2-4-6 7-14-2-4-6 7-14-2-4-6 7-14-2-4-6 7-14-2-4-6 7-14-2-4-6 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14-2-4 7-14	- 17000 P. F.	5. 31947E-J	C 100 000 00 00 00 00 00 00 00 00 00 00 0	C-1246/646	のようプロンドローの	6-34-0	746616-1 26939E-1	7. 535 645 -3	7.929.406-7
ži Ši	1-33-725-3	1.001316+0	9,678 148-3	9. 56.7.12	0-100 GC-6	4. V2A77F=:	8. 31.322E-u	7.695446-9	7. Tr 1996-4	7.053425-5	6.72928E-5	5.43751E-2	-6-3000000-11 -6-7600000-11	5-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	5-116+35-0	W. 73271E+3	4.468698-3	*-30% 5 8 8 · 4	3, 81 344E-9	3. 47 14 OF -9	2. 84 34 3E-0	2,522785-0	2-325681-5	1.87 4 525-9	1.529776-3	1. 22 5 155-3	9.00 1.91E-0		7.53247543	は一分ができる。	25 3 9 9 6 - 3	25354E+6	375646-0	734565-3	. 32556E-3	737466	03 36 JE - 3	, 37 6 54E-0	. 72 359E-0	.0-9755-5	385746-0	B-386617	31306070	400 4 3E + 3	7 700 0 7 1	25 CC.	144 X Y Y F - 1	4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3565E-3	734175-6	052-15-0
OK BIL	#	2	1	<b>.</b>	<u> </u>	9.5	. 40 4 +4	61	×	77	ř.	¥? (	5 X	: <b>:</b>	K	£2	62	£	# <b>;</b>	; :	į,	ĸ	3	ŭ	<b>2</b>	Ġ;	;; ;	M (	y #	3	*	4.6	67	<b>9</b>	7 (	řů	25	53	ኤ	<b>3</b> 2	9	. ·	9 (	ž (	63	1 G	y +-	3 3	. S	3	<b>2</b>

### CTION BUNDER 11 "Z" = 7.5303

SECTION PROPERTIES	PERTIES	1,4	SECTION AREA	<b>₹</b> ₹		y	3.14.18E-01	
			LOCATION O	LOCATION OF CENTROID RELATIVE TO STACK AXIS	XBAR YBAR	1 4 H	6.1938E-04 -9.1229E-03	
			SECOND NON ABOUT CENT	SECOND MONENTS OF AREA About Centrolo	222	1 4 4 4	1,6673E-01 1,0130E-01 -1,2958E-01	
	,		PRINCIPAL OF AREA AB	PRINCIPAL SECOND MONENTS OF AREA ABOUT CENTROLO	IP X IP Y		2.8766E-91 (AT 3.7215E-34 (AT	37.91 DEGREES TO "Y" AXIS) 37.91 DEGREES TO "Y" AXIS)
			TORSTONAL	CONSTANT		u	8.53028-04	
SECTION COCHDINATES	ROIMATE	<u> </u>						
	POINT NO	0	23	3.4	<u>Q</u>		Αb	
	**	•	-1-27 3115+90	1-734265+03	-1.281746+0	0	1.76785E+30	
	<b>N</b> P	• '	-1.263 (7E+0.0	1.75344E+33	-1,254346+0	0 0	1.74585E+33	
	• •	•	-1.162652+00	1.67014E+30	-1.198435+0	ה ספ	1.65902E+00	
	u ·	•	-1.15226E+00	1.62722E+34	-1,17 650E+0	6	1.61446E+00	
	۵ ۴۰	•	-1.121746+00	1,55564E+63	-1.14247E+0 -1.11434E+0	n n	1.55930E+01	
		•	-1.05036E+0G	1.43469E+00	-1.08611E+0	9	1.47716E+00	
	Φ.	- '	-1.729*9E+00	1.44952ii+05	-1.057766+0	0 0	1. 430 37E+03	
	2 ::		-9.67419E-01	1. 357 97E +0.0	-1.808716+0	7 0	1.33563E+30	
	25	٠	-9. 35221E-01	1. 311 77E +0:3	-9.72005E-3	10	1.23780E+00	
	2	•	-9.04.01.0E-01.	1.26539E+03	-9.43169E-01	70 5	1,23976E+03	
	1 11	•	-5.42027E-01	1,172126+00	-8.851062-01	4	1.143268+00	
	#:	•	-8-20-6476-01	1.125445+00	-8.556756-01	#	1.09496E+03	
	3 3	. •	-7.49184E-01	1.01538E+00	-7-99304E-0	7 T	1. 00172E+10	
	5	•	-7-1951JE-01	9.92063E-31	-7.71384E-01	7	9. 56868E-31	
	≅;	• '	6-49775E-01	10-34984.6 0.4384.8	-7.43651E-01	# :	9. 121 42E-01	
	3 23	. •	-6-30116E-31	6.62844E-01	0-364929-9-	4 7	6.23129E-01	
	S	•	-6. 602 31E-01	8.210958-01	-6.59782E-0	70	7.78880E-01	
	£	•	-5.75234E-61	7.775 35E-01	-6.31605E-91	ط د ق و	7. 346 35E-01	
	0 %	•	-2-10-10-10-5-	f. 35153E-91 6. 610 12F-61	-6.74.025Fun	# * 5 6	6. 474.24F=31	
	3 %	•	-4- 60 S 6 0 E-01	6.51110E-01	-5.464276-0	4 4	6.040798-01	
-	2	•	-4.49924E-81	6. 89476E-31	-5.17 824E-0	4	5.60997E-01	
٠	\$	•	-4-19756E-01	5.68111E-31	-4-89118E-01	10	5. 10212E-31	
	2 :	•	-1.69568E-01	5.278286-91	-4.60 312E-0	ed e	4.75739E-01	
	: 1	. •	-3-257455-01	4. 457 78E -01	-4- 02 402E-0	4 4	3.91763E-01	
	12:	•	-2.98848E-01	b. 05674E-51	-3.733046-01	5	3. 50 3 10E-01	
	1	•	-2.44292E-01	1. 66664F-61	- X. 44 A5 15-0	-	3. 43191E-01	

dÅ	2010-	-24 4.53148F-0	-01 1-14629E-0	-01 7.64246E-0	-01 3.05218E-0	-31 9.30491E-3	-02 -3.64539E-3	-02 -7.35610E-0	0-2044MC+1- 26-	-32 -1.53521E-3	-32 -2.19738E-3	-32 -2.55758E-0	-01 -2.93038E-0	-01 -3,30076E-0		-0.1 -4.34484F-0	-31 -4. 75153E-9	-01 -5.12074E-J	-01 -5.47715E-3	-01 -5.63053E-0	-01 -6.527A6F-0	-01 -5.67170E-0	-31 -7-21182E-3	-01 -7.548 96E-0	-01 -7.86037E-0	-01 -6.20632E-U	-01 -8.92535E-0	-01 -9.27610E-0	-01 -9.62247E-3	-31 -1.03018E+0	-31 -1.36356E+3	-01 -1.39655E+1	-31 -1.12922E+0	-01 -1-1515155E+0	-1.22535E+3	+0.1 -1.25685E+3	+0 ] -1.28812E+3	TO TO STATOE OF	103 -1.35035E+3									
<u>0</u>	-2.87569E	2.39012	2.01127	1.72177	1-43167	1.14.099	5.4977	7.56 85 ¢	2.66.64.0	19617	12912	.06517	.21200	.51785	- 56 + 37	43732	74436	. 05170	.35936	. <b>55</b> 7.35	25.57.5	59364	. 93 322	21 324	52 376	18131	52.852	. 87 627	25,462	92326	27 367	. 62 487	97694	26,75	0333	03955	07532	77117	14729									
2	2.9:095E-31	1 * + 57E -	770995-0	398 368	028646-0	61361E-1	Z+92955E-0	0 - 7 - 6 0 - 6 - 7 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	7. 449 445 = 2	1.147295-3	1.514388-1	1. 350 21E-7	2.22866E-3	2.53554E-0	7. 17466F-7	3,63664E-9	4, 346 66E-3	4.43464E-3	F. 75069E-5	5.11694E+7	5-81678F-3	6.164225-0	ú-39561 5·9	6-852785-3	7.193555-3	7 - 9 3 5 3 5 5 - 9	8-27691E-J	8+64614E-3	113905-1	9.7.595E-0	1.011 198 +3	1.047565+3	1.354,65.+3	t	1. 19391E+3	1.23077E+3	1. 257 81E+)	2000	14252E+1	YSEMI	.78785E+3	*75837E+3	.788788+3	-75929E+6	1.78961E+03	745 AGE +1	791446+0	) 
ž.	-2.137995-01	2.5.5.8.24E=0	1. 21 16 16-5	9-14-9195-0	6-181736-7	J. 21 176E-0	0-255962		65454545	C-316191	45.82.05-0	. 7542BE-0	* 18 16 65 - 3	. 35867E-G	04.725.15	236595-0	591548-3	0-316560.	196385-0	90 1 50t - 0	15 31 15-3	4.3226E-0	. 73 3 21E-0	996346-0	292116-0	911145-0	23511E-3	.55724E-3	. 67.761E-0	51233E-0	82759E-0	1-36:6-1	45 15 2E - C	. 770007FF	03676€+6	46651200	. 4965.6E+D	54201021	.1552ZE+0	XSE41	1.281746+0	1. 282 , 25 +1	1.282358+0	1. 25 24 JE + 3	-1.2025556400 -1.2025556400	1.282635+0	1.26259E+9	
DOENT NO	22	2	£	**	7	2	<b>,</b>	, u	2	, <b>,</b>	6	6,	Š	2	2 2 2	1 3	2	2;	25	, V 0	6	19	20	<b>*</b>	<b>3</b> 4	3 3	67	\$ 9	63	: #	22	2	2 :	, <u>*</u>	Ė	2	23		<b>:</b>	POLM NO	**		<b>#</b>	e v	s d	> <b>~</b>	. <b>w</b>	

					25 CEGREES TO "X" AXIS) 25 DEGREES TO "Y" AXIS)										
		2.7642E-01	-1.717UE-03 -5.8601E-03	1.6126E-01 7.4860E-02 1.0965E-01	2.3592E-01 (AT 34.25 2.1749E-04 (AT 34.25	6.52.29E-04		æ	1.02498E+03	1.74190E+01 1.69893E+10	1.65522E+00	1.61080E+00 1.56564E+00	1.5196E+03	1.47351E+00 1.42663E+03	
	0000°9 × ,2,	*	XBAR F	XX XX	x b di	4		ę,	-1-17140E+0J	-1.12060E+0] -1.09510E+0	-1.06952E+03	-1.04.354E+00 -1.01.606E+00	-9.922306-01	-9.66236E-01 -9.60150E-01	
1. 79198E 00 1. 79291E 00 1. 79391E 00 1. 7939E 00 1. 7939E 00 1. 7936E 00 1. 7935E 00 1. 7935E 00 1. 7955E 00 1. 7952B 00 1. 7952B 00 1. 7952B 00 1. 7952B 00 1. 7952B 00 1. 7956E 00 1. 7966E 00 1. 7956E 00 1.	SECTION NUMBER 12 '2' x 6.0000 eeessessessessessessessessessessessesse	REA	LOCATION OF CENTROID RELATIVE TO STACK AXIS	SECOND MOMENTS OF AREA ABOUT CENTROLD	PRINCIPAL SECOND MOMENTS OF AMEA ABOUT CENTROIO	. COMSTANT		S.A.	1.83074E+00 1.79102E+00	1.75027E+60 1.73664E+60	1.65630E+39	1.623162403	1.53492E+00	1.46991E+33 1.44435E+33	
- 1.28 5.2 1 1 1 2 1 1 1 2 1 1 1 1 2 1 1 1 1 1 1	25.07	SECTION AREA	LOCATION RELATIVE	SECOND NO.	PRESCIPAL OF ANEA A	TORSTONAL		ž.	-1.15234E+00 -1.13541E+00	-1.10777E+DC -1.460:2E>4D	-1.05215E+00	-1-15-17-15-15-15-15-15-15-15-15-15-15-15-15-15-	-9.67 8.9E-01	-9-33515E-01 -9-1116E-01	
^ទ ាដជាជនជង្គង ឯកឧត្តស្តស្តស្តស្តស្តស្តស្តស្ត		CTION PROPERTIES					STION COCROEMATES	POINT NO	<b>लक्ष</b>	•• •	4.4	<b>0</b>	•		

YSEMI

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ST ST	64 36 0 CM 4 12 0 20 20 50		0/05/2-01 1+39196540	1846-01 1.283446+0	613E+01 1.235J5E+3	8764 4F=0 4 + 186 49F40		01002E=01 1+13/00E=0	11 5 E - 0 1 T - 0 5 5 7 4 E + 0	28718E-01 1.04283E+0	03212E-01 9.96934E-0	77599E-01 9.51061E-0	51879E-01 3.05244E-0	26 952E-01 8. 595 08E-0	80118E-01 8,13881E-0	74.0785-01 7.66363E-0	47933E-01 7.23034E-0	21583E-01 6.77869E-0	95 330E-01 6. 329 15E-0	68875E-01 5.86191E-0	42319E-01 5.43704E-0	15666E-01 4.99481E-0	88915E-01 4-55553E-0	62069E-01 4-11971E-0	35130E-01 3.68727E-0	89665E-01 3.28274E-0	84121E-01 2.88125E-0	58504E-01 2.46276E-0	22816E-01 2.08715E-0	57 058E-01 1-694 29E-0	81.250E-01 1.354.08E-0	99 59/C+U1	0.346661-0.1 0.327464610 6469661-0.1 0.327464610	75 27 4E-0 2 -2 X36 29F-0	14-925E-02 -6-12652E-0	54244E-02 -9.69736E-0	72655E-04 -1.36502E-0	57947E-02 -1.7369E-0	29381E-02 -2.11093E-0	90 993E-02 -2+ 45175E-0	10 201E-01 -2 00 20E-0	55 55 55 55 55 55 55 55 55 55 55 55 55	67627F-01 -4.00268F-0	14797E-01 -4-37908E-3	41976E-31 -4.75329E-3	69165E-01 -5.12529E-J	96357E-01 -5.49467E-0	23586E-01 -5.86188E-0	53 825E-01 -6. 226 30E-0	78369E-01 -6.56762E-0	85 57 9E-01 -6. 946 09E-0	32701E-01 -7.300 86E-3	63 356E-01 -7 - 65 265E-0	67 445E-01 -7 999 67E-0		23 * 0	-17 -49 104 15E-1
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#### ECTION RUNGER 13 "Z" # 6.50(

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TORSTONM, CONSTANT  **S. **S. **S. **C. **C. **C. **C. **C.		PRINCIPAL. OF AREA AL	SECOND NONZNTS BOUT CENTROID			DEGREES TO "X"
YS  *** \$\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$		TORSTONAL	CONSTANT		5.3063E-04	
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#### 5. STATOR GEOMETRY

The technique and computer program used to define stator airfoils were the same as used for the rotor. The only significant differences were the stacking axis location and the number and spacing of manufacturing planes. The stator stacking axis was located near the trailing edge in order to minimize acute wall intersection angles in the aft portion of the passage. However, the stator twist turned out to be so slight that this is not a critical choice. Because of the reduced span (relative to the rotor) and the more complex leading edge shape, 11 manufacturing sections were employed spaced 0.375 inch apart. The computer printout on the following pages fully defines the stator airfoils and is identical in content and format to that shown for the rotor. Superimposed plots of the stacked streamsurface sections are shown in Figure 27 and of the manufacturing sections in Figure 28. Every other manufacturing section has been eliminated from the plot to improve the clarity of the figure.

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MOTOENCE AND EXTRA DEVIATION DISTRIBUTION

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EXTRA DIVISION

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15600 6.125 0.603

STREAM SURFACE GEORETRY SPECIFICATION

COMPUTING STATION	ut	NUMBER OF DESCRIPING POINTS.	4 POINTS# 4	IF 12465 ( 1) a	10
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		21	_	31.4865	
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		<b>₽</b>	6.3893	21.1694	
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		16	7.6936	21.1131	
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7)= 1			0 <b>*</b>	
IF ANGS (			IF ANGS (	
POINTS= 2	AIR ANGLE		POINTS= 2 Air Angle	
NUMBER OF DESCRIBING POINTS=	RADII	5.65314 5.65699 5.956699 6.0508 6.0508 6.0122 6.4574 7.5481 7.5481 7.5481 7.5481 7.5481 8.3714 8.3713	NUMBER OF DESCRIBING E RADII	5,7569 5,8931 5,8931 6,0569 6,0569 6,3939 6,8939 7,1794 7,3899 7,3899 7,3699 8,01297 8,2502
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	START VAL	. 10 00 . 10 00 . 10 00 . 10 00 . 10 00
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	TE THICK /2* CHORD	.00189 .00215 .00226 .00229 .00226
	MAK THECK /CHORD	.04000 .04740 .05740 .05716 .05716
ECTION GEOMETRY SPECIFICATION	LE RADIUS /CHORD	.00189 .001215 .001226 .001229 .001228
	NO.ALD INFL. PTS	
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BETAS = 45.765 (BLADE INLET ANGLE.)  BETAS = -7.557 (BLADE INLET ANGLE.)  BETAS = -7.557 (BLADE HAXINUM THICKNESS AS A FRACTION OF CHORD.)  T	IPX = .020.3 (MI 21.154 WITH 'Y' AXIS) IPY = .00193 (AI 21.154 WITH 'Y' AXIS)
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**≥**‡

-01141 -01374 -012846 -02846 -05857 -03657 -03657 -11996 -11996 -14264 -15345

> .08533 .11 72 .12470

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SURFACE COORDINATE DATA

N E D A T A ANGLE THICKNESS

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POINT NUMPER

POINT	ui T	ANLI	٥	ATA	SURFACE		THATE DAT
NUM BE R		<b>&gt;</b>	_	HICKNESS	X	ts xP	
#	. 20733	.17628	3	M.	.19867	.18856	2159
<u>.</u>	. 22313	. 19715	ă.	131	-21424 	-29329	2322
9 !	26952	19761	3 1	S;	52622*	-21152	2
) ·	17462.	. 23783	X.	3	155420	*22239	8
5 5	27833	22239		126.24	627624	27.72	18672
50	. 29314	. 22936	30.	3 (	28879	24538	8
12	. 30195	••	Ŕ	. 33784	.29260	.25263	. 31130
25	. 31376	.24281	R	. 03855	10 10 10 10 10 10 10 10 10 10 10 10 10 1	.25%	. 32309
23	. 32557	•••	8	. 03922	.31629	.26652	. 33486
* 6	. 53738		N i	2962	.32816	-27316	. 34663
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27	37251	- ''	g K	64132	PERSE.	20000	30.00
23 23	38462	.27680	12	. 34170	37585	29771	0.4868
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8	. 45824		23	. 04233	• 3 9979	.30561	. 41673
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7 2	45130		Ňi	. 04267	. 42379	.31915	+000p+ •
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36	. 48935	. 31791	5	·	47319	33602	. 48753
37	19264 *	. 32219	9	. 34252	*4 8567	.34229	<b>566</b>
33	. 56479	. 32630	3	* C4231	• 4 9815	.34639	. 51144
62	. 51732	. 3 3 3 2 7	4	• 04204	.51063	.35330	5234
3	42626	. 55410	3	2/140.	.52312	35434	5353
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3	57843	74603	1	* 0 4 0 4 0 4 0 4 0 4 0 4 0 4 0 4 0 4 0	57765	36734	COT 10 .
, in	. 59036	. 35119	1	1.3936	.58557	37.27	59519
46	. 60256	. 35423	7	. 03675	.59603	37395	60717
14	.61461	. 35715	Ħ	.33610	.61046	.37570	. 61915
<b>1</b>	. 62793	. 35995	4	. 037 41	.62292	.37.820	.63113
т Э (	• 63925	. 36265	4	. 03668	.63538	.3679B	. 64313
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4 6	67155	* 500 ES	:	. 13950	4657.52	******	7400
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- <b>^</b>	0.00 mm	78047	671		88218	.39751	. 38199	.38126
10	いないのは、	78047	-4 . 39P		89403	.39670	. 89367	.38165
7.4	10000 ·	1 4 8 8 9 7	-2.199		.90587	.39574	. 90536	38189
· ·	4 4 4 4 B	1 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	6/8-7-		.91769	39453	. 91707	.38198
. · ·	92044	38765	-3.569		.92953	.39337	. 92879	.38194
7.7	4 35 314	1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	74.7		.94129	.39195	. 94052	.38175
2.2	05257	4 4 5 G G	-4-989		95306	.39:38	. 95228	.38141
. 4	95.443	48683	107.5		.96482	.38866	. 96405	.38893
2.6	07621	75282	-6.42G		93926	.38679	. 97583	.38830
n c	98796	1 4 8 9 4 5 F	-7-142		.98823	.38477	. 98763	.37952
) <b>c</b>	00000		-7.857	70703	1.00000	.38260	99945	.37859

(BLAGE IMLET ANGLE.)	(BLADE OUTLET ANGLE)	(BLADE LEADING EDGE RADIUS AS A FRACTION OF CHORD)	IBLADE MAXINUM THICKNESS AS A FRACTION OF CHORD.)	IBLADE TRAILING EDGE HALF-THICKNESS AS A FRACTION OF CHUMD.)	ILOCATION OF MAXIMUM THICKNESS AS A FRACTION OF HEAN LINE-)	INERIDIONAL CHORD OF SECTION.)
	= -7.844					
ETA1	BETA2	rzeko		SNO		5080

NGRABLISED RESULTS - ALL THE FOLLOWING REFER TO ABLADE MAYING A MERIDIONAL CHORD PROJECTION OF UNITY SECONDACIONAL CHORD PROJECTION OF UNITY

BLADE CHORO = 1.0659

STAGGE & ANGLE = 20.284

CAMBER ANGLE = 52.650

SECTION AREA c . 03165

LOCALICM OF CENTROLD RELATIVE TO LEADING EDGE

X3AR = .46739 Y3AR = .27673 SECOND MOMENTS OF AREA ABOUT CENTRAID

IX = .00326 IY = .00176 IXY = .09363 ANGLE OF INCLINATION OF (ONE) PRINCIPAL AXIS TO "X" AXIS = 20.561

PRINCIPAL SECOND MOMENTS OF AREA ABOUT CENTROID

EPX = .05033 (AT 20.561 HITH 'Y' AXIS)

IPY = .03194 (AT 20.561 HITH 'Y' AXIS)

POI NT WUMBER	. '≍ ≅	A	N E O	NEANLINE DATA V ANGLETHICKNESS	SURFACI	SURFACE COORDINATE XS YS XP	NATE BATA XP	dž. Š
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Ņ	• 01736	. 11509		/+app.	076100	-	30010	
سو ،	13253	32977		400674	102962	*6220*	. 03564	• 0 2660
, ,	16701	401		101000	61419	909+0.	. 05161	<b>*06</b> *0*
• 4	06.147	40406		01312	05878	6284	. 067.55	.05308
N v	4000	4444		101524	.07343	.07722	44686	.06574
۰ +	2017	0 4 7 5 7		04736	.98811	.09121	. 09930	.07803
. •		02740	70.507	27070	1,0283	-10464	. 11515	• 0 8995
٥ د	16161			27.75	.11763	-11609	. 13068	. 10151
r (	1000	12486		. 02311	1 3242	\$3397	. 14663	.11273
1:	1000	* * * * * *		10420	.14727	24349	. 15228	.12361
4 (	1000	40000		2000	1 6217	45565	.17792	.13416
77	* 14 003	****			4 77 4 2	16746	19351	14639
21	119321	. 12233		****			1	•

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:	.29754	.16661		298	.19211	.17891	. 20906	.15431
15	. 21595	.17697		. 131.19	.29714	-19092	. 22457	.16392
91	. 23112	. 19791		.03281	*5 22 21	.23376	. 24003	.17323
17	. 24633	. 19673		. 03415	.23732	21120	. 25546	•18226
10	- 25818	. 29493		. 03513	20642	.21962	. 26734	446905
61	96692 •	-21115		409E4	*26075	*992Z*	126 12 .	414500
D C	7.192.	60912		*5970	262120	25,436	60162	27.75
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12	36434	26174		. 04158	.15538	26050	37330	24298
58	. 37614	. 26729		. 04202	.36733	.28535	16491	.24823
52	. 38793	. 27267		64240	.37924	+29201	. 39662	.25334
0.00	. 39973	. 27789		. 04273	.39120	\$4.26°	. 40626	.25830
34	. 41152	. 25295	ĸ	. 54299	.40317	37202.	. 41987	.26314
32	. 42332	. 23784		. 04523	.41516	.30784	. 43148	.26784
33	. 43511	. 23257	ಸ	. 64335	• 4 27 16	.31273	. 44 307	.27249
*	****	.29731	ន់	140to.	* 3962	-	. 45507	.27700
35	. 45957	. 37.186	8	. 34444	*45203	N	• 46706	.26147
36	. 67187	. 17628		. 04343	\$6405	.3267 p	* 47904	.28581
27	. 46402	. 31353		. 04433	.47703	,32131,	. 49102	.29003
8 H	• +9625	. 35463		• 0.6316	• 6951	Ζ,	. 50299	.29413
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3	55962	1252X		3	26642	: 5	57482	11639
63	58185	13937		04048	\$ 7690	.35899	58679	.31975
9	. 59437	34239		. 03969	.58937	.36178	. 5967.8	. 32301
24	. 68633	. 54530		. 03927	.63184	.364.2	.61076	. 12618
*	.61853	. 3+611		. 03863	.61433	.36694	. 62276	.32927
63	. 63976	. 35380		. 037.69	·6 2675	.36932	. 63476	• 33228
20	66178	. 35314		22.450.0	.6 37 96	.37136	• 64556	. 5 34 92
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20	. 75789	16530		. 53256	.70535	3813	. 71043	34922
2.5	. 71691	. 36699		.03169	.7 1650	.38266	. 72124	. 15132
23	. 72993	. 36657		. 03340	.72781	,38383	. 73205	.35332
64	.74095	- 37605		63620.	.7 395 3	.30487	. 74.286	. 15523
2	. 15197	37242		* 02895	•75026	.16579	. 75167	.35704
55	. 76298	192 in	٠	. 02363	.76247	*38658	.76449	. 35675
25	. 77403	12.260		20.220	•7.7269	229	* 77532	. 16035
3:	21687.	28478		*0420	64567.	700	478615	90107
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NUMBER	Σ	1 7 7 1	ANGLE T	X F A N L I N E D A L A X Y ANGLE THICKNESS	S UKF AC	SUKFAGE COUKDINA TE	XP UNIA	<b>4</b> ★
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70	.85726		. 091		.86725	.38755	. 86728	
71	. 87931		632		04628*	.38688	. 87921	
72	. 89135		-1.355		•09153	.38605	. 89116	
73	. 99339		-2.179		.93365	.38537	. 99313	
74	. 91543		-2.802		.91575	.38393	. 91511	
22	. 92747		-3.525		.92784	.38267	. 92710	
26	93951		842.4-		<b>6626</b>	1. 188.	. 112	
22	. 95155		-4.969		*95196	<b>.37</b> 9	. 115	
78	. 96359		-5.693		.96399	! <b>!</b>	319	
79	. 97563	. 37249	-6.413	. 00678	40070.		525	.3691
30	. 98767		-7.128		.98801		33	
•	16000		2 81.1.		CORC . *	٠,	2.4	

والإنجاج والإعراض والإوراف فالمراق والمسافقة والمساورة والمتحد والمتحدود والإستان والمساورة والمتحدود والمتحدود

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VTINO

(BLAGE INLET ANGLE.) (BLAGE OUTLET ANGLE.) (BLAGE OUTLET ANGLE.) (BLAGE MAXIMU THICKNESS AS A FRACTION OF CHORO.) (BLAGE TRAILING EDGE HALF-THICKNESS AS A FRACTION OF CHORO.) (LOCATION OF MAXIMUM THICKNESS AS A FRACTION OF HEAN LINE.) (HERIUJONAL CHORO OF SECTION.)	HOPMALISED RESULTS - ALL THE FULLOHING REFER TO ABLADE HAVING A HERIOTONAL CHORD PROJECTION OF ALLOHOUS STATEMENT OF ALLOHOUS STATEM			X° AXIS = 19.23. AXIS)	SURFACE CODED IN A TE DATA KS YS XP YP
(81405 INLET ANGLE.) (81405 CUTLET ANGLE.) (8140E RAXINUM THICK (8140E RAXINUM THICK (8140E TRAILING EDGE KLOCATION OF MAKINUM (MERIUIONAL CHORO OF	LONING REFER TO ASLAD	GANDER ANGLE = 51,317 SECTION AREA = ,03172 LOCATION OF CENTASID RELATIVE TO LEADING EDGE	-67087 -26518 AREA ABGUT CENTACIO -69523 -93170	IXY = .00358  ANGLE OF INCLINATION OF GOME) PRINCIPAL AXIS TO "X" AXIS = 19.23.  PRINCIPAL SECOND MOMENTS OF AREA ABOUT CENTROID  IDX = .00#31 (AT 19.230 MITH "X" AXIS)  IPY = .00#31 (AT 19.230 MITH "Y" AXIS)	EANLINE DATA V AMGLE THICKNESS
	- ALL THE FO	= 51,317 = ,03172 andro relati	# .67087 # .26518 OF AREA ABGU # .89923	# .00358 HATION OF COM HONENTS OF # .00833	# H
BET41 BETA2 YZE90 T TONE CORC	HOP WE ISED RESULTS  ***********************************	GAMBER ANGLE SECTION AREA LOCATION OF CEN	XSA2 # YSAR # YSAR # SECOND HONDROFTS OF	XY ANGLE OF INCLIN	POINT NUMBER

4	되 경 ·	1 1 1 4			SURFACE	S COURDINATE	THATE DATA	2
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1	.18523	,	23.59)	•	44.77.31	15716	19295	13361
£ .	12661 *		32. 885	•	.1911	.16710	23728	1,4212
91	. 2133	:	32.159	•	•23498	.17678	. 22156	
<b>.</b> .	. 22736	•	30 % · 150 %	•	.2 1687	.19619	. 23585	
e (*	レンティン・	•	30.47	•	123063	26.65	. 24768	
Ñ	100 to 10	. 1935.3	22.22		100000 100000	27.75	. C. V.	17760
72	* 274%	•	2	•	26525	200	3 2	4 8384
2	. 28584	·	28.57	•	.27691	.22259	29470	18978
2	さなべながっ	*	27.36.	•	.25859	.22934	3,164	+19561
2 ;	. 10,023		27.34.5	•	.13023	.23591	. 31818	.2 3130
C %	****			•	.31201	67242*	. 12985	-20665
S <b>2</b>	744.5	•		•	92525	6442	94449	*21226
*2	154 2				10000000000000000000000000000000000000	16+62	15472	. 22265
5-2	. 46772	•			.\$5913	266999	37633	.22765
\$	19648	•		•	. X 7:97	+27145	. 39796	
4 :	11165	•		•	.38282	*27672	C *66£ *	.23721
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POT ME	tu.	ARLI	2	A T A	SURFACE	COCROI	NATE DATA	4
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	. 85936	33.353		61932	• 6 5932	.36320	. 85939	.34387
	K7212	35350		. 91832	.67228	.36250	. 87 203	64448*
72	99790	35330		. 11663	.88506	.36164	. 88469	34495
, M	10/5E	35293		. 91536	.89790	.36961	. 89737	.34526
7.2	94039	35241		. 7.1481	.91073	35940	. 91006	.34541
4	100 M	35172		. 91264	.92354	.35803	. 92277	.34541
	93534	3000B		. 61127	•93632	.35649	. 93550	.34524
7.2	764.857	34.989		68600	.94913	35478	. 94825	34492
. 40	95163	34867		. 10653	.96185	.35290	. 96101	***
7.0	97419	34733		. 007.13	92428	.35386	. 97380	.34380
) /C		34582		. 66573	.98730	.34865	. 98660	.34299
5 +4 2 <b>4</b> 0	12666	いいなかない。	-7.910	. 00433	1.00000	.34628	- 39942	.34202

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MORALISED RESULTS - ALL THE FOLLOWERS REFER TO RELAGE MARING A MERICIONAL CHORD PROJECTION OF UNITY

LOCATION OF CENTROID RELATIVE TO LEADING EDGE * 15.336 97759 . . 1 1.0531 146767 = STAGGER ANGLE SECTION AND CAMBER ANGLE PLASE CHERS

TARR - -47261

SECOND HOMEN'S OF AREA ABOUT CENTROLD

12 - - 98421 27250 - - 7X

ANGLE OF INCLINATION OF IONE: PRINCIPAL RAIS TO "X" AXIS # 18.463

CAT 18-461 HITH "X" AXIS) PRINCIPAL SECOND HONGHIS OF AMEA ABOUT CENTROLD

. . 65252

SUMFACE CODROINATE DATA REARCENECORESS A MAGLE THEORRESS POINT NUMBER

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R.C. 9.7	3.4.		. 61228	.95219	.05111	• 05996	. 4416
	45.4	4. K.	4.4.4	.86542	1627	07.195	.0517
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28.86	. 33663	3	) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (			4000	2 7 7
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17.7.7.   17.5.5   11.01   1.27.69   1.1697   1.1666   118463   1.167.7   1.17.7   1.17.3   1.0.7.3   1.0.7.7   1.0.7.3   1.0.7.3   1.0.7.7   1.0.7.3   1.0.7.3   1.0.7.7   1.0.7.3   1.0.7.3   1.0.7.7   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.0.7.3   1.				tak	CKMES	eg X	ħ		-
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1, 14, 17, 18, 14, 17, 18, 14, 18, 19, 19, 19, 19, 19, 19, 19, 19, 19, 19	*	1772	*4	E	327	.16973	414656	끆	.12346
22726 16756 1875 1817	â	437	ű	ù	2	16201*	.15693	Ξ	.13142
2.222. 6.153. 7.15. 6.151. 7.15. 6.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.15. 7.1	<b>3</b> 2 (	.29623	-	ñ	333	.1 9614	.16517	2	*13919
25239 11077 754 515 10 1041 1	ha 1	992.2	2		2	.20943	56427	2	.14678
15.259   14077   29.544   29.51   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.239   25.	6 d el v	****		2	2 5	20022	/ CX21.	3 6	.15515
Fig. 1995   Fig. 2   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997	7.	25.734	*	~ W		26374	119645	2 %	16549
23756   2157   22 150   2157   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169   2169	**	26.395	-	25.344	63.35	.25523	23334	2	17145
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13.046.5   12.155   12.07.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.04.5   12.0	r: N	. 25712	H	27.779	13	+27629	.21651	ર	.1 5297
1710.77   27110. ZC. 5757   1710.77   27110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110   23.9110	35.	. 29859	~	27.169	S	58682"	.22239	ξ	.18853
13342   22266   25.932   14.12   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.646   13.6	22	. 31.527	21	8.55	びや	かけれてか。	.22336	ñ	.19395
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.67972 . 32513 9.119 . 33691 . 67587 . 34291 . 68757 . 3 .69183 . 32792 8.613 . 03511 . 66918 . 34437 . 69443 . 3 .70399 . 32645 6.982 . 03320 . 72641 . 34797 . 72011 . 3 .72316 . 33149 6.982 . 03220 . 72641 . 34497 . 72011 . 3 .74212 . 33547 6.465 . 03117 . 75410 . 34499 . 77310 . 3 .7422 . 33473 5.201 . 6296 . 76629 . 35137 . 75975 . 3 .7639 . 35691 4.571 . 02795 . 76599 . 35137 . 76950 . 3 .7639 . 35691 4.571 . 02793 . 76756 . 35137 . 76939 . 3 .7643 . 33928 2.491 . 02725 . 6243 . 35137 . 76939 . 3 .8143 . 33928 2.491 . 02725 . 6243 . 35137 . 802841 . 3 .8462 . 35010 1.162 . 02294 . 32723 . 35123 . 62643 . 3	, R.	66764		, -	·	666456	34432	3	, 57
-69141 .32702 6.613 .01511 .66414 .34437 .66443 .3 71339 .2277 6.165 .03417 .7149 .34671 .71629 .3 71236 .31599 6.982 .03221 .72611 .34797 .71011 .3 75225 .33473 5.611 .03012 .7540 .34691 .77101 .3 75225 .33473 5.611 .03012 .75671 .34797 .72010 .3 75435 .33597 5.611 .03012 .75671 .34790 .77575 .3 77639 .33691 4.571 .02796 .77529 .35137 .7593 .3 87647 .33780 3.926 .02563 .77756 .35137 .76939 .3 81468 .33726 2.811 .22755 .62795 .35137 .89339 .3 81468 .33726 2.811 .22725 .86139 .85137 .861239 .3 81468 .33726 2.2153 .86133 .86143 .3	ž.	.67972	-			67587	.34291	3	.30736
71574 32477 6 145 0 13417 77049 37471 77629 33 71571 71571 71572 33 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 71571 7157	23	.69183	•	•	0	.6.6914	VE+45.	69	.30967
.71577 . 33945 7.542 .03320 .71379 .34691 .71915 .3 .72316 .13199 6.982 .03221 .72241 .34797 .73001 .3 .74212 .33473 5.311 .03012 .75070 .34690 .75716 .3 .75439 .33691 6.971 .02964 .76299 .35133 .76562 .3 .77639 .33691 6.971 .02793 .77529 .35133 .76562 .3 .77639 .33691 8.971 .02793 .76756 .35137 .76910 .3 .81458 .33928 2.491 .22593 .61435 .35137 .81239 .3 .81458 .33977 1.766 .22594 .32713 .35123 .62643 .3 .84628 .35910 1.162 .02294 .32713 .35123 .62643 .3	ę,	. 70389	-	•	4.3	.7 0149	+57	2	.31188
.72316 .X3199 6.982 .03223 .72613 .34497 .73001 .3 .7621a .31341 6.465 .03117 .7340 .7340 .74185 .3 .7622a .3147 6.465 .03112 .75640 .34459 .75630 .3 .76431 .31587 6.201 .02914 .75629 .3513 .76562 .3 .7643 .33597 6.201 .02914 .77629 .3513 .76562 .3 .7639 .35690 4.571 .02793 .77656 .3 .76539 .35690 4.571 .2263 .401096 .35137 .78939 .3 .8112 .3132 .2263 .32425 .3263 .32137 .35139 .36243 .3 .82848 .33377 1.768 .02294 .32423 .35123 .02843 .3 .86128 .54010 1.142 .02153 .8113 .35123 .82643 .3	64	.71537	_	^	•	.71379	<b>69</b>	Ľ	~
************************************	63	. 72336	-	•	~	.7 2613	•79	7	~
*75222 33473 5.811 ,03012 .75071 .34459 .75775 .3 *76431 .33590 4.571 .0263 .75529 .35133 .77550 .3 *77639 33590 4.571 .02633 .77526 .35147 .77550 .3 *7158 .35726 3.21 .02633 .76756 .35147 .76939 .3 *8168 .35726 3.21 .02553 .6096 .35147 .76939 .3 *8168 .35726 2.21 .02553 .61435 .35147 .61239 .3 *8168 .35726 2.225 .61435 .35549 .85540 .3	<b>61</b>	.7492.	# # 3345	•	U	0.492 %	600	Ž	~
.764%; .33587 5.200 .02966 .76299 .35:33 .76562 .3 .776%9 .33690 4.57; .02793 .77750 .3 .776%9 .33690 4.57; .02793 .77750 .3 .476% .336% 3.227 .22593 .00096 .35147 .77590 .3 .81488 .33924 2.49; .22525 .01096 .35139 .01540 .3 .8284% .3397 1.758 .02294 .0273 .35123 .02643 .3 .846.28 .36010 1.142 .02153	23	. 75227	. 33473	ų,	. 93012	.75073	342	ĸ	~
.77639 .33690 4.971 .02753 .77550 .35162 .77750 .3 .77647 .33780 3.926 .02683 .76756 .35117 .78939 .3 .47168 .35127 .78939 .3 .816488 .33928 2.491 .22553 .861435 .35137 .85939 .3 .82848 .33977 1.768 .02294 .82773 .35123 .82840 .3 .82848 .35977 1.768 .02294 .82773 .35123 .82843 .3 .86128 .59010 1.142 .02153	3	. 76431	. 33587	ķ	330	.76299	35:3	2	. 32141
**************************************	*5	. 77639	. 33693	j	61.30	17525	5.56	C	.32298
.49168 .33928 2.217 .02553 .60096 .35137 .60239 .3 .61488 .23928 2.491 .02425 .61435 .35139 .05540 .3 .82648 .3337 1.768 .02294 .02773 .35123 .62643 .3 .84128 .34010 1.142 .02153 .84196 .35389 .8.146 .3	65	. 746+7	. 33786	-	. 02683	.76756	511	2	.32443
.81438 .83928 2.491 .92425 .61435 .55139 .02540 .3277 .82843 .32843 .3285 .82843 .3285 .82843 .3285 .82843 .3285 .82843 .328	\$ :	. 49154	. ¥3862	m	. 32553	.63096	513	. 69239	. 32568
. #284%	<b>.</b>	4	13.924	64.2	*	.61435	213	8	27
ANDRE GENTLO E ROTARE GANGOS CARANTOS NELSON CHOSES BUNGOS	e (	9	. 15137	9.4	2:	.82773	212	8	29
	Ď	, i	21045	*	7	****	2	9.1.0	3

POINT	III	A N N	ω ω	ATA	SURFAC	E COORDI	ENA TE DATA	•
NUM BE R	×	>	ANGLE T	Y ANGLE THICKNESS	S.	XS YS XP	Α×	ΥΡ
in the	. 85446		. 313	* 32025	.85443	35.38	. 85454	.33513
7.1	. 86768		-, 413	. P.1887	.86775	.34958	. 86761	.33080
72	. 63089		-1.151	. 01748	.88106	.34880	. 38071	.33132
73	66468*		-1.887	. 11618	.89435	.34774	. 89382	.33168
74	. 90729		-2.625	. 11465	•9 0762	.34651	. 90695	.33187
75	64826*		-3,364	. 01322	.92088	.34510	.92010	.33193
76	. 93369		-4.105	.01177	.93411	.34351	. 93327	.33177
77	68936		-4.846	• 61031	.94733	.34174	94946.	.33146
7.8	. 96,003		-5.589	. 00885	.96053	.33980	99656	.33099
64	. 97333	. 33462	-6, 3.32	. 00738	.97370	.33769	. 97289	.33035
50	. 98650		-7 , 175	* 00593	.98686	.33539	.98613	.32954
*	. 9997.9		-7. R13	- 00442	4.0000	77233	0.4000	3285F

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is mail white.

# 41.185 (BLADE DULLET ANGLE.) # 47.553 (BLADE DULLET ANGLE.) # 47.553 (BLADE DULLET ANGLE.) # 47.553			* 2.1995 (Meriolonal Chord of Section.)	NGG MALISED RESULTS - ALL THE FOLLOWING REFER TO ABLADE MAYING A MERICIONAL CHORD PROJECTION OF UNITY	አርተር ። አ	* 17.660	s & \$. 93\$	* ,13267	LOCATICH OF CENTROID RELATIVE TO LEADING EDGE	X340 x 047439 Y36 x 026557	SECOND HOMEN'S OF AREA AROUT CENTROIS
05 TA1 05 TA1	0.371 T	; • ~	CORCO	NOG 48LISED RESULT	BLADE CHORD	STAGGER ANGLE . 17.665	CANBER ANGLE	SECTION AREA	LOCATION OF C	163	1994C+ GH0325

DATA

INCLINATION OF CONT.) PRINCIPAL AXIS TO "X" AXIS = 17.754

.3312

RREA ABOUT CENTROLD

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PRINCIPAL SECOND HOMENTS

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(AT 17.754 WITH 'X' AXIS)

. 3759.3

4 4 7 X Z

OOI NT FUNGER	# #	7 7 X	NE D	A T A MICRORESS	SURFACE	E COORDINATE 75 XP	KATE DAT	<b>▼</b>	
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1	. 17 392	12668		. 62731	46355	01021	. 17829	.11519	
2 A	* 10000 ·	3		X0 1	1 8900	15580	2017	4 -	
17	20334			315	-20176	.16+30	2179	-	
**	12122 *			326	.21297	.17158	. 22946	.14337	
1.9	. 23259	4		337	.22421	.17871	. 24097	.14939	
<b>5</b> 3	96133			×	.23547	.18558	. 25246	.15527	
12	. 25534	-		25	.24675	19250	. 26393	┥,	
25	. 26672			99	.25605	-19915	. 27 536	.16666	
53	. 27413	er: 1		3.577	Ν,	*20564	. 25650	,,	
*	7562			1,000	5 / 00 Z *	261170	12067	4 .	
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0.6	22276			1	44400	20001	112227	٠.	
. 62	Contrar .			; ;	.32636	23558	25.5	. ~	
5.3	14634	2		Ŋ	.33782	.24105	3548	N	
50	. 15772			3	_	.24635	. 36613	N	
75	. 36939			043	.36081	.25147	. 37738	N	
32	. 38 347			3	.27233	.25642	. 33663	.21579	
33	. 19164	Ň		3	.36387	,26118	19661	N	
45	. 47:368	ž		3	\$9590	*56594	. 41145	N	
35	. 61552			1	*6.079	.27 151	. 42309	N	
36	* 45735			S	6661 4.	*27488	. 43472	.23227	
37	. 43919			ŝ	*6 32 04	.27936	46634	-23612	
e i	. 45113			5	. 4 4413	.2837	4579	W I	
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9	. 54573			.04413	.54861	.30917	5506	ıN	
	. 55757	Ň		. 04368	.55266	117	. 56248	N	
**	. 55941	Ñ		. :4322	.55479	3	. 57411	.27210	
**	. 58124			. 04273	.5767	18	. 58575	.27491	
<b>₽</b>	. 59374			. 04211	·58945	6	* 59664	N	
er (	62969	m i		94740	/1289*	N (	6103	Ŋι	
, i	01410	•			694709	į	2220	v	
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i i	6.55.55			1986	65308	3 (4)	6594	! N	
20	. 66873			03754	.65581	3 37	6716	N	
57	.68125	-		O	.67854	m	. 68396	N	
<b>89</b>	. 69375			.03567	.69127	336	. 69623	. 29832	
<b>5</b>	. 73625	ä		. 03468	.70403	350	. 70850	8400 M*	
ç	. 71975			'n	.71673	2	7207		
61	.73:25	2		2	.7 2945	369	7330	<b>m</b> 1	
. i.	. 74.575			5	.74217	377	7453	. 3 1636	
£ .	. 75625			BU OND .	•	9	7576	•	
,	4,007.			0			7693	2 C T T T	
2 3	20101			3 8	- *	100	7056	11015	
2,4	25.00			Š	86708	8	7		
3	£222			: 2	.82181	393	8226	. 31533	
<b>.</b> 6	43546		1.193	. 02263	. 8 3563	13302	63619	31640	
·	1			}		}	}	!!!	

POINT	¥	A M L I	N E O	ATA	SURFAC	E COORDI	NATE DATA	Ø
NUMBER	×	X Y ANGLE THICKNESS	ANGLE T	HICKNESS	XS	KS YS XP	Α×	۲P
2	. 84352		.478	. 62129	.84943	.33851	. 84961	.31730
7.5	. 86 317		246	• 91610	.86321	.33781	. 86313	.31805
72	. 87682		976	. 61833	.87698	.33694	. 87667	.31864
73	4.69347		-1.715	.01682	.89073	.33587	. 69022	.31906
7.4	. 90413		-2.463	. 01532	693445	.33462	. 90 38 3	.31932
25	. 91776		-3.213	. 11381	.91817	.33319	. 91739	.31943
76	. 93143		-3.971	.91228	•93186	.33156	. 93101	.31931
7.7	. 94538		-4.736	. 01074	.94553	.32975	<b>+9446</b>	.31904
78	.95874		-5.508	. 60923	.95918	.32775	. 95829	.31863
79	. 97239		-6.284	• 63764	.97281	.32556	. 97 197	.31797
63	. 98634		-7.166	. 006.08	.98641	.32318	. 98567	.31715
81	93666	. 31.838	-7.853	• 0.0451	1.00000	.32061	. 39938	.31614

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(CLACE INLET ANGLE.) (CLACE CUTLET ANGLE.) (CLACE CUTLET ANGLE.) (CLACE MAXIMUM FORCESS AS A FRACTION OF CHORD.) (CLACE MAXIMUM MICKNESS AS A FRACTION OF CHORD.) (CLACE TRAILING EDGE MALF-THICKNESS AS A FRACTION OF CHORD.) (LOCATION OF MAXIMUM THICKNESS AS A FRACTION OF MEAN LINE.) (MERICHOMAL CHORD OF SECTION.)	HOP FALISED RESULTS - ALL THE FOLLONING REFER TO ABLADE HAVING A MERIDIONAL CHORD PROJECTION OF UNITY  OR ADE CHORS - A 1.7459						ex = fals = 17.097		AXISI	SUKFACE COORDINATE DATA KS YP XP XP
	THE FOLLOWING REFER TO ABLA		SECTION AREA - 135292 Location of Cemirold relative to Leading Edge	ም ነ ተ የ የ የ የ የ የ የ የ የ የ የ የ የ የ የ የ የ የ የ	CARLA ABOUT CENTRGIO	529 54 54	ANGLE OF INCLINATION OF CONTI PRINCIPAL AXIS TO "X" AXIS = 17.097	PRINCIPAL SECOND ACHENIS OF AREA ABOUT CENTROLO	12 (AT 17.097 MITH 'A'	SANLINE OATA Y ANGLE TAICHNESS
82741	DAYALISED RESULTS - ALL IM	STAGGER ANGLE = 17.566 CANJER ANGLE = +8.639	SECTION AREA - 132892 LOCATION OF CENTROLD AS	ANDER CONTRA	4754 . SINGHON CHOUSS	PACED N AND THE PACE	ANGLE OF INCLINATION O	PRINCE PAL SECOND ROMEN	repos a mai	Pollof A A A A Service A A A Service A A A A A A A A A A A A A A A A A A A

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POINT	# E &	7 1 1 1	9 3	ATA	SURFACE	E COORDINATE	NATE DATA	•	
NOW GEE R	st	<b>-</b>	-	HICKNESS	য়	ኤ	œ G	d >	
9	. 15686	. 12539	-	. 72723	.15962	319	3	.1.388	
	17452		31.567	. 02867	17232	4	1570	.11605	
9.	1261	1 1596	32.907	36.39	-	.14535	8	.12307	
F 7	. 23494	化二二二二二二二二二二二二二二二二二二二二二二二二二二二二二二二二二二二二二	30.432	314	.1 9683	45734	8	.12992	
<b>6</b>	26.512	. 14993	29.923	- 33261	-2 3779	-16436	3	₩.	
54	. 227 :1	12951	219-62	337	2.1872	2	χ.	-	
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13	)1642 ·	10001	70.	- 5555 WAS	26456	474014	90/67	4 5800	
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	797E	19578	26.666	03867	27373	3	3	•	
2	29.54.9	1.1128	26. 182	39.5	•	93	2	-	
52	30457	1,1663	18 m	100 mg m	N	.21683	32		
27	. 31566	23584	24.679	7	.33701		-		
2	32674	169: 2	24.259			253	. 33532	-	
62	. 33752	- 21103	23.627	34242	-7	32	3463	•	
33	. 34639	. 21661	22,983	500	~	\$	. 35731	.19678	
77	. 15994	. 22123	22.326	, 14362	.35170	24.5	. 36827	.20105	
32	37116	. 22571	21.656	ï	.36292	29	. 37 92 3	•20520	
13	· 38.25.4	. 2 3003	26.02	w	.37416	5.4	. 39012	w	
ž	. 19177	. 23440	20,263	. 34501	.3 6596	ž	• 40156	u	
33	. 405/40	. 23462	19.565	. 24537	.3978.	66.0	• 41299	W	
36	. 41732	192+2	18.889	• 34567	£ 3963	5*5	4544	w	
37	. 42865	. 2.457	18 - 2 31	16541	.42147	563	. 43583	.22477	
36	. 44.328	25033	17.595	. 64613	.4.3331	23	****	. 2 28 36	
13	. 45493	•	16.979	22956.	91544	.27635	. 45 865	.23105	
Ş	. 46353	いというと	16 - 345	. 34628	** 5703	8	. 47 006	.23523	
**	. 47516	. 25479	15.416	* 34627	. 46885	33	. 49146	. 23853	
2	. 46678	~	15.265	. 14629	6.6834	30	** 49267	•	
, .	45865	м.	26.7.39	609		ġ.	12505		
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9	• 52146	- 27.304	13.759	V6V40.	42914	26.6	226		
9	6.28.56	496.22	27.73	. 06535	Λ,		10000	4 .	
	25456	16112	12.577	10791	1998	2 (	つかかかい	<b>v</b> (	
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7	61476	. ~	10.375	.06156	-61602	3	6235		
	48356	. 2.3626	***	. 04977	·w	163	6361		
22	. 64555	. 2 3846	•	. 63994	w	101	6488	"	
<b>36</b>	. 65445	-		. 03966	w	8	6614	**	
2	. 67 \$ 35	.31252		. 23826	.66854	213	. 67 415	.20365	
<b>₩</b>	.68424	. 37637	7. 935	.03717	.63168	.3227	6868		
<b>6</b> 0.	. 69754	4 10 10 1	•	91999	19469	3	9669		
e :	*CB1/	. 53773	•	. 53511	46.20.4	762	7.7.2.1		
od (	1224	27671	221.9	20360		192	3		
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7	アンサイト	51715	5. 185	* 6327.5	•	2	ě	20062	
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POINT	¥	A C C	2 W	4 7 4	SURFACI	E COGRDI	NATE DATA	A
NUM BER	×	>	ANGLE T	X Y ANGLE THICKNESS	XS	xs vs xP	A ×	ΥP
4	9044		. 533	. 22216	.84478	.32778	66448 •	.30562
7.7	. 85896		189	• 62064	.85899	.32736	. 65892	.30642
72	. 67393		921	. 31911	.67318	.32616	. 87288	.30705
7.3	. 88710		-1.663	. 01755	.88736	.32536	. 98685	.30752
74	. 90118		-2.414	.01597	.90151	.32377	+8006	.30781
75	. 91525		-3.174	. 01438	.91565	.32226	. 91485	<b>3</b> 33792
76	. 92932		-3.943	. 01277	•92976	.32060	. 92888	.30785
2.2	94339		-4.723	. 01115	.94385	.31872	. 94293	.30769
7.8	. 95747		-5.536	• 00952	.95792	.31664	. 95701	.30716
62	46176		-6.299	. 30768	•97197	.31436	. 97111	.30653
60	. 98561		-7-198	• 38624	00986*	.31189	. 98523	.33570
40	. 99968	<b>→69 : 2 •</b>	-7.908	. 98458	1.00000	.30921	. 99937	.30467

# 19.2% (%LADE INLET ANGLE.)  # -7.4% (%LADE OUTLET ANGLE.)  # -8.4% (%LADE LEADING EDGE RADIUS AS A FRACTION OF CHORO.)  # -8.4% (%LADE RATING FOR PACKESS AS A FRACTION OF CHORO.)  # -8.4% (%LADE RATING EDGE HALF-TMICKNESS AS A FRACTION OF CHORO.)  # -5.3% (LCCATION C* MAXINUM FRICKNESS AS A FRACTION OF CHORO.)  # 2.3% (MERIOIDMAL CHORD OF SECTION.)	MUNICALISED DESILIS - ALL THE FOLLOHING RETER 10 ABLADE MAVING A MERIDIOMAL CHORD PROJECTION OF UNITY AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA	E = 15.536 = 47.251	Section area - 13344 Location of Centroto Relative to Leading Edge	(3) br. 1. 47645 19 br. 23.25	second noments of area boast centrold	* • • • • • • • • • • • • • • • • • • •	ANGLE OF INCLINATION OF (OHE) PRINCIPAL AXIS TO "x" AXIS = 16.485	principal secong moments of area about centrolo	r a cardis (at 16.450 with "Y" ares) r a caras (at 16.450 with "Y" ares	MEAMLINE DATA SURFACE COOLOIMATE DATA R T AMGLEIMICKHESS KS VS XP
06 TA1 06 TA1 72 E R O 1 1 1 ON E 2 00 R O	MORYALISED BESIALT BEADE CHORD	Stagge augles	SECTION AREA LOCATION OF C	401	SECOND 10MENT	<b>6</b> 48	ANGLE OF THEL	PRENCIPAL SEC	H & B	POINT NUMBER

-0.173 -0.0795 -0.0795 -0.0795 -0.0795 -0.0797 -0.0797 -0.0797 -0.0797 -0.0797

0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000

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2	. 16.74	. 11612	=	~	.1575	412776	. 17193	649010	
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9	16972	13223	Ä	13029	•1.6202	14427	13745	11019	
17	+ 23222	. 1 1452	Š	3	.19439	.15224	. 21.314	.12401	
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2	. 22.366	. 15566	Ė	. 63195	.21543	.16591	. 23169	.13502	
	- 234 19	. 1.5654	e);	. 53532	.22503	.17193	. 24274	. 14115	
2	. 24.54.5	***	N.	3.76.36	.23665	.17822	. 25 356	.14637	
23	25262	15.26.7	8	. 53796	*54730	.10437	. 26436	.1514.8	
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M.	. 4479.3	. 25707	**	. 44724	66 19 %	27098	. 49386	.23427	
3	. 49954	66652.	ű	•	.49362	.28278	. 50506	N	
<b>4</b>	. 51376	. 26281	Į	. 246 82	.5 1524	.26556	. 51627	.24005	
<b>3</b>	. 52217	. 26552	7	. 44653	.51586	.23520	. 52748	N	
	. 53359	. 25.615	Z	. 54623	.5 2848	.29 172	. 53869	.24558	
*	. 54 533	2 . 869	H	. 24594	60015.	.29313	. 54991	.24825	
<b>6</b>	. 55641	.27319	-	. 04554	•55169	29562	. 56114	. 25088	
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S	6359	25451		. 24.45	,	30856	61928		
25	. 64.923	23163.	•		•	.31:26	. 65230	.27017	
25	. 66245	12262.	•	•	£9059*	.31161	. 66531	N	
2	.67571	. 23488	~	. 63865	.67349	.31322	. 67433	.27493	
£.	. 65396	. 29593	~	. 63762	.6 2659	64379	. 69134	.27710	
9	* 76222	29766	Φ.	. 25.56	10000	.I1561	. 73436	.27932	
<b>,</b>		16942"	•	. 63542		.31658	. 71739	. 20136	
29	. 72973	. 4 1035	•	92 100	.72703	.31740	- 73042	.28330	
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*	. 75523	2/2: 5		. 0.3183	.75397	*21858	. 75650	.28686	
<b>3</b>	. 764:3	3777	<b>~</b>	. 0.50.50	.76743	31932	. 76955	.28947	
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*	£ 2424 *	Tage .	No 255	· 65+03	1000	* > 2 2 2 4 4	•		

POI M	# #	1 7 2 4	O W	ATR	SURFAC	E COORDI	ENATE DAT	•
NUK ARK	*	سو	ANGLE T	Y ANGLE THICKNESS	X	Ž.	XS YS XP	46
7.5	* 64374	. 3 ,666	.633	• 62309	.64861		98039	.29511
7.7	. 85519	. 3 1673	182	. 02151	.85520		. 85517	.29598
72	. 66953	. 3 . 662	613	. € 1994	.86978		67698 *	.29667
73	. 65438	. \$ 1632	-1,553	• F1826	.88433	.31545	. 38 38 4	.29719
74	. 89853	. 37583	-2, 311	• £1661	.69687		. 89820	. 29753
25	. 91238	. 33515	-3.082	. 01494	.91338		. 91258	.29769
76	. 92743	. 39426	-3.966	11325	.92788		. 92699	.29767
Z	. 94188	.3.320	-4.564	. 01155	.94235		. 94141	.29744
78	. 95633	. 3 1 192	-5.474	. 00963	.9568		. 95586	.29702
19	.97078	. 31043	-6.295	. 00811	.97122		. 97034	.29640
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E 37.918 (BLADE INLET ANGLE,) E -5.163 (BLADE QUILLT ANGLE,)	* .3)226 (86.ADE LEADING EDSE RADIUS AS A FRACTION OF CHORD.) A .34743 (81.ADE MAXIMUM THICKNESS AS A FRACTION OF CHORD.)		8 . STOOD (LOCATION OF FREILLOR THIOKNESS AS A FRACTION OF MEAN LINE) A 2.2547 CHERICIONAL CHOSO OF SECTION.	FOLLO	अंक्रीता में स	LE = 15.617	n 46.157	% t .)3459	LOCATION OF CENTROID RELATIVE TO LEADING EDGE	1348 × 67523 1848 × 62930	SECOND MOMENTS OF AREA ABOUT CENTROID
BE TAS BE TAS	YZERO T	TONE	6803 2003	WERNALISED RESI	BE ADE CHARG	STAGGFR RNOLE	CAMBER ANGLE	SECTION AREA	LOCATION OF		3404 CH0225

ANGLE OF INCLINATION OF COME! PRINCIPAL AXIS TO "X" AXIS

PATHOT PAL SECOND HOMENTS OF AREA ABOUT CENTROID

(AT 15,434 HITH "X" AXIS) (AT 15,434 HITH "Y" AXIS)

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# E #

P01 M 124 PTR

COOR CYATE DATA YS XP YP	. 15999	.19263	72476	74797	. 22816 .1	. 23637 .1	. 24654 .1	. 25869	. 26882 .1	. 27.893	. 20902	29908	24045	12047	33915	34912	35907	. 36903	. 37966	. 39071 .1	. 40155 .1	.41238 .1	. 42321 .2	70 40464	000000	5. 69564.	. 10001	24 7.73	2. 01004.	5. 5. 19. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	52065	. 53149 .2	. 54234 . 2	. 55595 .2	. 56956	. 20310	. 53070 •	62395	. 63754	*****	**************************************	. 56472 . 6	.56472 .6	. 56472 . 67832 . 269192 . 6	67472 67832 69192 69192 6	67 251461 67 251461 67 251617 67 251617 67 251617		65672 65113 65113 65113 651672 651832 651832 651832 651832 651833 651833 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65183 65180 65180 65180 65180 65180 65180 65180 65180 65180 65180 65180 65180 65180 65180 65180 65180	67832 67872 67832 67832 67832 67832 67832 67832 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833 67833	67 872 8 67 832 8 67 832 8 67 832 8 67 832 8 67 832 8 67 832 8 67 832 8 67 832 8 67 8 67 8 67 8 67 8 67 8 67 8 67 8 6	5.8.2.8.5.4.5.4.8.5.8.8
SUR ACE CO																																																			67342 66746 66746 76576 77256 77256 77376 87377 89338 89338 89338 89338 89338
A T A TAICKNESS	•	•	•		, ,	3			•	•	•	•	•	• (				٠	•	7	٠	•	•		,	•	•	•	•			•	•	٠	•	:	•			•	•		•	* *	4 4 4	0000	****	* * * * * * *	******	* * * * * * * * * *	*******
LINE O AMGLE																																																			2010 5.993 2010 5.993 2029 5.403 2029 5.403 2050 6.495 2050 6.403 2050 5.903 2050 5.303 2050 2.303
# F	16791	17515	• •	24991	•	•	٠	•	•	٠	•	•	•	•	1 177	3-384	•	٠	57.232	•	•	•	•	٠	•		•	•	•	• •	•	•	•	•	٠	•	• :	•	•	•	•	•		•	• •	• • •	• • • •		• • • • • • •		700970 71786 71786 71786 71786 71789 71799 71799 71799 71799 71799
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POINT	tii T	ANLI	() ()	ATA	SURFACE	E COORDI	SURFACE COORDINATE DATA	4
NUM 3C &	×	<b>&gt;</b>	ANGLE T	X Y ANGLE THICKNESS	X	χ.	× م	۵
	. 834£4	. 28954	672.	. 02485	.83398	.31136	. 83430	.27711
7.1	84919	- 28964	. 348	.02313	.84918	.3 1121	. 84923	.27808
7.5	85424	28956	675	. 02138	.86436	.30.25	. 86411	.27887
73	. 87328	. 23928	-1.422	.01963	.87953	.29308	.87904	.27949
4.6	85468	. 28881	-2.193	. 7178)	29768	.29770	. 89399	.27992
10	90933	2.58413	-2.973	. 61597	6406	.29611	96806	.28016
7.	92443	. 29724	-3.789	.01413	.92489	62462	. 92396	.2832
22	93948	. 29614	-4.623	.01226	693997	.29225	. 93898	.28003
78	95455	. 28481	-5.471	. 11039	.95502	.28998	. 95403	.27964
62	. 96 957	. 28325	-6.342	. 0.0852	40076°	.28747	• 9691 D	.2790
. 6	98462	. 23146	-7.232	• 00663	<b>•985</b> 04	.28473	. 98420	.27819
<b>8</b>	19696	. 27943	-8+143	69400 •	1.00000	.28175	* 88834	.2771

(BLADE INLET ANGLE.)

# 37 . +12

= -8.231 (BLADE OUTLET ANGLE.)	E .0.227 (BLADE LEADING EDGE RADIUS AS A FRACTION OF CHORD.)	= .34851 (BLADE MAXIMUM THICKNESS AS A FRACTION OF CHORD.)			= 2.2479 (MERIDIONAL CHORD OF SECTION.)	NORMALISED RESULTS - ALL THE FOLLOWING REFER TO ABLADE MAVING A MERIOTOMAL CHORD PROJECTION OF UNITY Des sessossesses sessessessessessessessessessesse	0 = 1.0363	\$TAGGER ANGLE = 15.255	1.E = 45.643	EA = , 93522	LOCATION OF CENTROID RELATIVE TO LEADINS EDGE	X3AR = .47697 Y9A.R = .21531	SECONU MOMENTS OF AREA ABOUT CENTROIO	IX E .00116 IV E .01160 IX E .0015C
BETA2	YZERO	-	SHOA	N	C040	NORMALISED RES	BLADE CHORD	STAGGER AN	CAMBER ANGLE	SECTION AREA	LOCATION O		SECONU MON	

ANGLE OF INCLINATION OF CONES PRINCIPAL AXIS TO "X" AXIS = 15.341

PRINCIPAL SECOND HOMENTS OF AREA ABOUT CENTROID

(AT 15.041 WITH "X" AXIS) (AT 15.041 WITH "Y" AXIS)

* .01312 * .33231

AA

.01198 .01198 .02192 .03168 .04127 .05369 .05394 .05904

. 00669 . 006669 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 0106666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 0106666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 0106666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 0106666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 0106666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 0106666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 0106666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 0106666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 0106666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 0106666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 0106666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 0106666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 0106666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 0106666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666 . 010666

. 92692 . 92692 . 92692 . 93692 . 95148 . 95148 .14402

.08653 .09519 .10357

14285

SURFACE COORDINATE DATA
XS YS XP YP

H L I N E D A T A Y MGLE THICKNESS

POINT NUMBER

.152.2	.11755	33, 365	. 02842 . 02999	.15483 .16685	.11981	.16921	.09529
200	. 12163	Ŕ		.17888	353	1945	1.37.88
986	. 12643	8	• 03299	•19094	£23	2367	•11396
1 9	13377	N N	. 13525	•2 1934 •2 1934	3 3 3 3	. 22677	.12342
3	. 14415	27.3	_	.22097	•	. 23674	.12801
61	1.918	8	. 03737	.22361	.16586	. 24669	.13251
101	11474		0 40 45 5 40 45	21676	47664	10007	413032
773	.15365	8	_	,25917	.18186	. 27640	14544
763	. 15825	່ຂໍ	. 04119	-2690 s	.18695	. 28 627	.14955
746	. 17274	2	•••	.27865	.19191	. 29611	.15357
7 60	19178	3 .	49240	278872	213574	30294	15/43
7.22	15552		_	.30651	.20632	32553	.16503
647	11955	ಸ	•	7701 20	-21 146	.33529	.16864
671	. 1346	7	_	.32839	.21476	. 34503	.17216
959	.19724	8	• 04635	.33836	.21892	. 35476	.17557
6:1	27090	ល់ ទ	_	.34835	.2223¢	36446	.17887
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963	. 21900	16.	_	-40368	•24260	. 41792	19541
1168	. 22223	3	. 34963	•41476	*54634	. 42863	.19841
9525	. 22533	ä,	-	+425 <b>4</b> +	.24933	• 43926	.23133
1000	2332		•	4 60 44	1500ct	1.00 A	25.692
529	. 23397	7	•	45913	.25834	. 47130	.20963
6.38	. 23665	띪	•	.47318	.26138	. 48198	.21222
969	. 23923		•	44 8125	.26358	• 49266	.21478
12.5	2,14.2	7	•	26264	검법	50000	21020
298	2+648	17	•	.51445	9	. 52474	.22215
3+5	. 24874	H	•	.52551	8	. 53544	.22451
153	+ 25157	H	•	.53979	12	. 54928	.22751
1265	25428	3;	•	տա	27812	. 56310	.23.45
8671	25937	4 "		5,58269	, Y	59073	23610
3377	. 26175	· U·	•	ູເກ	4	. 60454	.23881
1683	. 26493	•	•	o	14	.61835	.24144
10 to	+1992	•	•	.62561	Ň	• 63216	.24399
234	. 25816	-	•	•63992	ġ.	. 64597	.24646
57.3	900.22	,	•	•65423	.29127	. 65977	-24685
0 6	27.70		*	Dν	Ó	56570	252114
916	27502	3 4	2 40 5	7 2020	ģų	70172	25555
1324	.27642		.0380	.7 1143	12	.71504	.25747
5723	.27773	•	. 5367	.72571	3	. 72666	.25939
1135	.27885	4	. 1354	•73999	10	.74272	.26120
5-1	.27987	- 1	. 334		9	. 75657	.26291
0	+25084 +25084	30	. 03242	+1697+	29792	.77161	• 26465
+ 7 1	+0107	-	Š	7766 14	3	000/	C 7 00 7 *
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POINT	¥: W	ANLI	х Е	4 7 4	SURFACE	COORDI	NATE DAT	⋖
NUM BER	×	>	ANGLE T	X Y ANGLE TAICKNESS	sx X	ξ.	xs vs xp	<u>۸</u>
7.0	. 33174	. 25382	.729	. 32567	.83158	.29585	. 63190	.27019
7.2	. 847.11	. 29312	. 125	.02368	.84703	.29506	.84701	.27118
72	.86227	. 28303	732	. 62297	.86241	.29436	. 85214	.27200
M	. 87754	. 28275	-1.451	. 02522	.87779	.29285	. 87728	.27264
74	. 89281	. 28226	-2.224	. 01834	.89316	.29142	. 89245	.27309
75	. 90 8 17	. 23156	-3.019	. 41645	.93853	.28977	<b>*90106</b>	.27335
76	. 92333	. 23064	-3.836	. 91453	.92382	.28789	. 92285	.27340
77	. 93861	.27951	-4.674	• £1259	•93911	.28578	. 93809	.27324
7.8	. 95337	. 27815	-5,533	.01063	.95438	.28344	. 95335	.27285
79	. 95913	. 27655	-6.413	. 60867	•96965	.28186	. 96865	.27224
63	. 98443	.27471	-7.312	• 00669	•98485	.27833	. 98397	.27139
61	. 99965	. 27263	-8.231	. 63471	1.00000	.27496	• 39933	.27030

06141 06142 12640 1 1045 2	8 - 13 - 146 8 - 13 - 13 - 13 - 13 - 13 - 13 - 13 - 1	(BLADE INLET ANGLE.) (BLADE CUTLET ANGLE.) (BLADE LEADING EBGE RADIUS AS A FRACTION OF CHORD.) (BLADE MAXIMUM THICKNESS AS A FRACTION OF CHORD.) (BLADE TRAILING EBGE HALF-THICKNESS AS A FRACTION OF CHORD.) (LCCATION OF MAXIMUM THICKNESS AS A FRACTION OF MEAN LINE.)
CORD	* 2.2527	(MERIDIONAL CHORO OF SECTION.)

HOPMALISED RESULTS - ALL THE FOLLOWING REFER TO ABLADE HAVING A HERIOTONAL CHORD PROJECTION OF UNITY SECURES CONTROL CHORD PROJECTION OF UNITY

8LADE CHORD = 1.0350

STAGGER ANGLE = 14.989

CAMBER ANGLE = 45.176

SECTION AREA = .43591

LOCATION OF CENTRO IO RELATIVE TO LEADING EDGE

XBAR = .47954

YBAR = .21177

SECOND HOMBATS OF AREA ABOUT CENTROIN

EX * .00116 IY * .00191 EXY * .00050 ANGLE OF INCLINATION OF (ONE) PRINCIPAL AXIS TO "X" AXIS = 14.753 PRINCIPAL SECOND MOMENTS OF AREA ABOUT CENTROID

IPX = .00092 (AT 14.753 MITH 'Y' AXIS)
IPY = .0254 (AT 14.753 MITH 'Y' AXIS)

NEANLINE OATA Y ANGLE THICKNESS

Point Number

SURFACE COORDINATE DATA
XS YS XP YP

00180	*0.642	.01455	.02251	• 0 30 29	.03790	.04534	.05263	.05975	.36671	.07351	.08017	. B 8668
. 10376	. 11658	. 02935	0.04211	<b>*8450 *</b>	• 16755	. 16024	. 0929a	. 13554	. 11815	. 13074	. 14330	. 15584
.00188	.01184	.02162	.03123	191 900	46640.	•05915	.06738	.67674	.06533	.09375	.10200	.11709
7500C*	.31257	.02422	065£0*	•04759	.05931	•07105	.9 6281	09460	.10642	.11625	.13012	.14201
. 00472	• 00674	. 03673	. 01571	. 11256	. 01459	.01649	. 91837	• 02020	. 52201	.02378	. 02550	62719
37.346	36.517	15.987	35.453	34.916	34.381	33.841	33. 303	32.756	32.216	31.663	31.123	30.577
3- 99900	. 33953	. 31.839	. 12687	. 93548	. 3+392	. 15219	. 16630	+36824	. 17602	19966	. 09249	39638
. 90236	. 31457	. 92679	13930	. 15122	. 06343	. 07564	. 08785	. 10007	. 11228	12453	. 13671	16892
**	N	m		w	•0	~	•	•	12	11	<b>2</b>	13

.16114	•	37	623	.15392	183	'n	•
17335	. 11253	3.5	44080	.16586	.12575	2	40 9925
10770	+		4 6	C # B B B B	4	? [	4 +
267.4	•		63665	1 9936	6.65	2:	11589
21719	•	2	35	.20892	521	. 22544	*
. 22688	-	12	. 03687	.21853	577	. 23526	*
. 23658	•	Ŕ	. 03793	.22810	H	. 24506	.12923
. 24629	*	Ŕ	. 63896	.23772	9	. 25464	-13349
. 25598	•	N.	56613	.24730	17370	50465	.13767
. 26565		i.		*25732	.1785r	• 27 434	┥`
. 27538		i i	5	679924	.155/5	10497.	٠,
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4444		į	57573	32519	24132	26198	16767
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16734	•	9 5	; ;	400000 400000	21975	36112	17419
16376		5	3	\$5523	22326	. 37172	
37 65 3		1	24.5	.36674	.22731	. 38232	
36533		7	640	.37773	.23119	. 39291	_
39617	*	17	676	.38866	.23490	. 40348	**
40.634		16	35	.39963	.23846	. 41406	
42752	~	ģ	Ğ,	. 41063	.24187	. 42463	.19329
65839	•		* 0.55; 0.4 0.155; 0.4	• 2157	.24512	. 43523	~ ,
20019	•	7	7 4	CC2C++	2010	1,554	
46373			1	45459	25435	. 46691	2.423
67347		5	150	24694	.25676	.47748	170
48225	. 23432	7	153	*4764	.25434	. 46636	N
. 49332	. 23676	7	5	042840	.26130	. 49864	.21176
. 50 379	æ	ä	150	.49836	•26416	. 53922	1.0
95475	. 2+147	17.	S	.53931	.26640	. 51981	.21653
, 52533	. 2 - 370	#	350	•52025	.26855	+53041	w
53956	24655	11.	.50	.53471	.27123	C+++.	14
55378	W 1	3;		27675	27.376	. 25636	N
11000	v	÷ (		10000	31017	• 25 630	u :
505cs	v	ď	- C4022	5,0000	28 47	. 50034	00000
64.167	1000			46.0707	26226	64427	. "
65-69	. 20123		9	.62155	26399	62824	10
63912	. 26323		573	.6 3603	-28556	. 64221	.24589
65334	~		240	•65051	.28697	.65617	w
66755	N	ۀ		£6499 <b>*</b>	,28822	. 67014	.24561
62189	. 26857	٥		•61946	.26932	. 68412	.24783
696.1	. 27311	'n.		•69392	-29.26	. 69810	N I
71023	25112	5.47		.7 0836	-29105	. 71209	N,
72445	. 27.281	. و	37.8	.7 2264,	29168	. 72608	25394
1,333	965/2	*	9	62727	*23CT2	80047	V 1
75230	-27499	2.00		.75172	7.262.	. 75409	.25752
76533	. 27590	M F	. 33343	•76736	*2926* *********************************	. 76929	.25929
	9 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	•		770 /	767670	6 6 6 6 7 9	3.
	֡				0.000	7007	7.00

MIDd	1. T:		S W	A <b>+</b> A	SURFACE	E COORDI	NATE DAT	⋖	
NGH BE R	×	<b>&gt;</b>	ANGLE T	Y ANGLE THICKNESS	ΧS	Ş.	KS YS XP	۸b	
22	. 83431	. 27619	.756	. 02643	.62984	.29141	. 63019	.26498	
71	. 84544	. 27.636	. 952	• 02458	.84543	.29 )59	. 84545	.26601	
72	. 86386	. 27822	677	. 0227	66098*	.28957	. 86 072	.26687	
73	. 87528	.27794	-1.431	. 02079	.87654	.28833	. 87602	.26754	
74	. 8917 3	.27745	-2.211	.01885	.89207	.28686	. 69134	.26803	
75	. 9u713	.27674	-3. 115	, 01688	.90757	.28517	. 90668	.26831	
76	. 92255	. 27562	-3.843	. 61493	.92305	.28325	. 92205	.26839	
. 22	. 93797	. 27467	4.695	• 01289	.93851	.28139	. 93744	.26824	
<b>7</b> e	. 95339	. 27328	-5.571	. fi 1fi 86	.95392	.27869	. 95286	.26788	
64	. 96881	• 27 166	69**9-	.00883	.96931	.27634	. 96832	.26727	
63	. 95424	. 26378	-7.388	• 00678	.98467	.27314	. 98383	.26642	
91	• 99955	. 26766	-8.33,	.00472	1.09003	•26939	. 99932	.26532	

	(BLADE INLET ANGLE.)
HEIRZ = 6.439	(BLADE CUTLET ANGLE.)
¥2€80 = .03229	
40HE * .03229	
2 × 5307	
C080 × 2.2593	(MERIDIONAL CHORD OF SECTION.)

STAGGER ANGLE = 16,795

SECTION AREA = .03665

# 45.271

CAMBER ANGLE

LOCATION OF CENTROID RELATIVE TO LEADING EDGE

1348 = .47999 1342 = .27943 SECOND HOMBLES OF AREA ABOUT CENTROLD

05000° × AXI 46300° × AXI ANGLE OF INCLINATION OF 18M2) PRINCIPAL RAIS TO "X" AXIS = 14.57.1

PRINCIPAL SECONG MOMENTS OF AREA ABOUT CENTROID

IPX = .05032 (AT 14.570 MITH "Y" AXIS)
IPY = .03207 (AF 14.570 MITH "Y" AXIS)

1 .93237 3.31930 36.632 .094.5 .03095 2 .61651 .31930 36.264 .00676 .01249 3 .92663 .91781 35.734 .01361 .02495 4 .33876 .32653 36.284 .01362 .33564 5 .9532 .3452 36.987 .01483 .01565 6 .9656 .06134 37.992 .01673 .017054 8 .8956 .06134 37.992 .01673 .01657 14 .1155 .9172 31.917 .0241 .1741 12 .1155 .9172 31.917 .02641 .1741 12 .1256 .93220 31.953 .02641 .12563	XS YS XP	d. ×	YP
3.1750 36.632 .004/5 91781 35.734 .0061 91781 35.734 .0061 91892 34.635 .01281 91832 36.93 .01281 9533 32.645 .01657 9573 32.645 .02647 9573 31.990 .92231 99220 31.357 .02647			
93 930 36.264 00674 91781 35.734 00981 91781 35.734 00981 91925 35.635 001281 91922 35.935 001281 91938 32.945 00267 9173 31.990 02067 91520 31.397 02241		. 30 37 8	30189
91761 35.734 .00001 972645 35.165 .01002 973492 34.636 .01201 95132 34.93 .01477 95130 32.645 .01867 96739 32.645 .01867 9773 31.990 .02047 99220 31.357 .02411		. 01650	• 3 0626
13645 35.165 .01002 13492 36.636 .01283 14.22 36.707 .01477 15.13 38.539 .01857 15.930 32.991 .01867 16.73 32.445 .02047 17.73 31.950 .02247 19.220 31.357 .02413		. 32923	.01424
. 13492 30.636 .01283 . 13422 30.287 . 15434 30.539 .0167 . 15438 32.592 .01857 . 16739 32.445 .02047 . 1920 31.397 .02243 . 1920 31.357 .02413 . 18651 30.816 .02586		. 04188	.02203
. 34.322 34.387 .C1477 .05.34 33.539 .01673 .15938 32.992 .01865 .46739 32.445 .02047 .97473 31.993 .02231 .93220 31.357 .02413 .38951 38.815 .02586		. 63453	.02965
. 05134 33.539 . 01673 . 15930 32.645 . 01857 . 05793 32.645 . 02047 . 1773 31.957 . 02413 . 19220 31.357 . 02413	. 35689 .04933	. 06716	.03713
. 15930 32.991 .01857 .85789 32.445 .02047 .87473 31.900 .02231 .95220 31.357 .02413 .38951 30.816 .02586		. 37977	.04+38
. 46789 32.645 . 02047 . 97473 31.990 . 02231 . 99520 31.957 . 02413 . 38951 30.816 . 02586		. 39235	.05153
. 87473 31,900 .02231 .09220 31,357 .02413 .38951 30,816 .02586		19461	.05846
.18520 31.357 .02413		. 11744	• 0 6526
. 18951 30.816 . 02546		. 12995	.07191
		. 14244	.07841
. 24567 M. 276 . 02758		. 1549.	. 3 6476

POI M	نا <b>ک</b>	112	_	A 7 A	SURFACE	E COORDINATE	NATE DATA	•	
KUN PE &				MICKNESS	ĸŞ	ž.		4	
,	. 162 8	1.368	ž	. 52926	.15262	.11536	. 16733	.09098	
E.	17.221	111253	R	93069	16467	.12431	. 17975	• 0 97 05	
4	. 15+34	. 11726		. 0.3243	.17655	.13149	. 19213	.10360	
<b>A.</b>	. 19647	. 12382		. (3401	.18645	.13660	. 20451	.13881	
61	. 23621	. 12891		.03519	*19792	6***	. 21430	.11334	
61	. 21574	. 1 7393		. 13635	+20741	15 138	• 2240 E	.11778	
72	. 229 38	-		. 6.37 16.7	.2 1692	1 5 5 5 7	. 23364	.12214	
22	. 235 . 2	*		. # 3855	\$ 25645	-16 95	. 2+358	.15641	
22	. 24465	**		. 03967	.2363	.16622	. 25330	.13063	
2.2	. 25+29	**		• 34¢ 62	.2+557	.17139	. 26 303	.13473	
2.	. 26392	**		• 66193	.25516	.17643	. 27269	.13871	
<b>\$</b>	. 27 756	ing.		*5252*	*56477	.10136	. 28235	.14263	
<b>92</b>	. 28 319	₩		*****	•27443	.18618	. 29199	•14646	
22	1 9262 .	-			.26495	16.61.	. 31161	•15020	
82	992CE *	-		. (4512	.29372	19561	. 31121	.15384	
2.3	. 3121)	**		16549	.3354	119998	* 32078	.15739	
35	132173	-		. 24665	.31313	*2342¢	. 33034	•16384	
7.	. 33137	•		, 14735	.32286	.29638	. 13968	.16419	
32	. 36230	*		. 04601	.3 3261	.21243	. 34939	.16745	
77	170.70	*		48.63	.3 42 39	.21635	. 35689	.17069	
*	. 36,25	w		. 24927	.35328	*52202e	36963	17399	
S.	. 17217	~		. *4965	. 36417	.22456	16675	12/17	
<b>3</b> 2	. 13278	N		. 35.7 80	10545°	.22641	. 39049	18045	
22	. 1935)	74		· 550000	** 6598	.23210	. 40102	.18352	
2	. 40.621	N		. 55127	68968	-23563	. 41153	67981	
e e	. 45493	N)		. 35163	1926	*53931	45205	.16936	
ç.	. 42554	Ν,		. 55193	.41873	27.7	43254	912610	
7	. 43636	N 1		81251	99629*	554920	1001	16461.	
Ŋ	. 44737			95.26	06044	97642*	40.50	367610	
<b>5</b>	サントのよう	29522	13. 317	64N60 ·	37164	01152	1404	610020	
*	*****				700	E 15 C 34	7047	20000	
2	724	v :		00000	70723	00000	1601	• C C C C C C C C C C C C C C C C C C C	
9 1	77.00	٧,		20261	7 7 7 7 7	26446	5066	200.6	
	201.4	· 1		F. 20.1	1126.00	611024	1 2000	24220	
9 0	07116	4 4		4.36.4	445.74	26.63.0	62728	21459	
	. 276	4 .		66.60	50076	26.824	54.4	21762	
A	1000	9 .		10100	F 15 15 1	27.70	3554.8	2225	
1 7	ECE 12	9 6			45.79.5	27.319	56.056	.2234B	
2 1	679			90000	5.517	27542	. 56365	.22631	
, d	59324	25328		. 04938	.58976	.27750	. 59772	.22907	
\$\$	60 637	•		. 24624	.6 3435	1812	. 61173	.23175	
4	. 62243	25776		. 047 32	.61894	.28116	. 62586	.23435	
\$3	. 1357-	**		. 346 32	•6 3354	.28276	. 63993	.23688	
23	. 651.17	-		. 24525	.64813	.28419	. 65403	.23932	
63	. 685.	74		. : 46 11	.66273	97582	. 56867	.24167	
	. 67375	. 26525		* 34291	.67732	.28657	. 68215	.24394	
<b>6</b> 1	. 59-56	. 20681		. 04164	•63790	-28732	. 69623	.2.611	
29	. 70.664	4.25425		. 040 31	.73546	.28531	. 71031	.24818	
63	. 7227 3	. 25.955		. 03693	.7 2105	.26894	. 72443	.25016	
*	. 73766	.27272		6.577.69	.7 3562	.289.1	. 73853	.25204	
64	. 752.73	. 2 . 176		.03599	.75017	.28972	. 75261	.25301	
99	. 76691	. 27276		. # 34.32	.76592	78887	. 76790	*25561	
67	. 78263	* 27355		• 03260	.7 8166	- P 8 38 3	. 76319	.257.27	
•	.79734	. 27619		29660	.7 97 39	.28959	. 79649	61952*	
Ş	. 41.346	. 27465		. : 2903	.61311	•£8915	. 81381	•26116	

POI ME	T	11 12 4	Z ()	ATA	SURFACE	C00401	NATE DATA	4
NUM PER R	×	<b>&gt;</b>	ANGLE T	Y ANGLE THICKNESS	XS YS XP	Z.	Α×	۸
7.9	. \$2897	. 27493	. 689			.28850	. 82914	.26136
7.1	64449	. 27502	325			*28764	. 84448	.26241
72	. 86311	, 27492	763	. ^2333	.86916	.28657	. 85985	,26327
73	. 87552	. 27461	-1.525			.28527	. 87524	. 26395
7.	. 59134	.27469	-2.313			.28374	• 69 065	•26444
75	* 96856	. 27336	-3.113			.28199	93608	.26472
76	. 92217	. 27249	-3.952			.28330	. 92155	.26480
77	. 93759	. 27121	-4.6.6			.27777	. 93704	• 26465
70	. 95 31 3	. 25979	5.683			.27530	. 95256	.26427
79	. 96862	. 26812	-6.581			.27257	. 96811	.26366
83	* 3965 *	. 26623	-7.503			.26960	. 98369	.26281
61	59666	.25483	-8-439			.26637	. 19931	26169

THE RESERVE OF THE PARTY OF THE

BETA1 BETA2	= 36.785 = -8.562	(BLADE INLET ANGLE.) (BLADE OUTLET ANGLE.)
YZERO	• • 03259	(BLADD LEADING EDGE RADIUS AS A FRACTION OF CHORDS.
YONE	- 19229	(BLADE TRAILING EDGE HALF-THIS'S AS A FRACTION OF CHORD.)
7	5036	(LOCATION OF MAXIL SM "HICKNESS A FRACTION OF MEAN LINE.)
CORG	= 2,2974	(MERIDIONAL CHORD OF SECTION.)

NORMALISED RESULTS - ALL THE FOLLOWING REFER TO ABLADE HAVING A MERIDICAL CHORD PROJECTION OF UNITY and reserves the transfer the transfer the transfer the transfer transfer the transfer trans

SECOND HOMBNIS OF AREA ABOUT CENTI-IO

IX = .00016 IY = .03196 IX = .30351 ANGLE OF INCLINATION OF (ONE) PRINCIPAL AXIS TO "X" AXIS = 14.472

PRINCIPAL SECOND HOMENTS OF AREA ABOUT CENTROLD

IPX * .30013 (AT 14.472 MITH 'X' AXIS)

IPY E .00211 (AT 14.472 MITH 'Y' AXIS)

X X Y ANGLE THICKNESS  03237 0-71000 36-765 .00473  91443 -01589 35-245 .00682  92847 -02646 35-080 .01093  05:55 -93453 36-945 .01695  07:45 -05073 33-391 .01695  01:45 -05073 33-391 .01695  10:45 -05073 33-391 .01695  10:45 -05073 33-391 .01695  11:1066 -07378 31-78 .01695  11:1066 -07378 31-78 .01695  11:1066 -07378 31-78 .02645

OINT	₩ #	ARLI	0	A T A	SURFACE	E COORDINATE	NATE DATA		
13. E.R.	×	-	_	HICKNESS	4	Ę.	<u>م</u>	e.	
;	.15879	7	29.561	٠,	.15147	.11521	1661	.08937	
15	. 17083	-	29.033	Ģ	.16321	.12276	. 17844	.0.9533	
<b>16</b>	18286	7	28.509	• 03299	1174.39	413316	. 19673	•10116	
17	.19489	7	266.12	o	.18678	.13737	. 20300	.10686	
13	. 20 45 4	7	*12.57	•	•19626	.14306	2128	.11134	
£ 7:	. 21419	7	27.14	• 03697	.20576	.14864	2226	.11574	
9	. 22384	7	101.03	.03613	.21527	15412	2324	.12006	
12	6122	•	19.5.1		19422	12950	2421	.12430	
25	* 14 31 4	•	0		25.45.0	174010	? ?	*1.045	
5.6	1707	•	20.00		******	76,010	9 5	13231	
3 00	******	•	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-	402024	16471		1.0049	
20	05717	:		9 0	010070	16.75	2070	414030	
3.0	204 10	•	20.00	06.100	77600	1 1 1 1	00002	0777	
	No.	•	2		2004	4070		45450	
3 6	29 A&A			04686	30486	4000	10.1	4 55.62	
` <u> </u>	1201X		21.581	. 047.51	74167	2000	420	15845	
17	8000X		3	. 04636	32131	20693	33.864	.16178	
125	13%63		36%	, .	33108	21099	34.61	16501	
13	16927		19.783	69640	24087	21491	3576	16815	
10	15999		19.999		.35175	.21910	36.82	.17152	
45	. 37.97.3	•	18.437		*36264	.22312	. 37.676	17477	
36	. 38141	~	17.797	. 05151	.37354	*22698	3892	.17793	
37	, 39213		17.17	ب	38445	.23067	3996	.18098	
36	+ 40284		16.579	-	.39536	.23421	. 41032	.18394	
39	. 61355		16.902	.05282	.4 0627	•23760	• 42083	.18682	
£.0	. 42427		15.449	.05315	•41719	*54084	. 43134	.18961	
<b>61</b>	. 43498		14.913	. 95341	.4.2810	.24393	. +4185	.19233	
21	44569		16.413	.05361	** 3905	-24689	4523	.19497	
r,	* 45643		23.932	<b>P</b> (	26677	27:42	4628	.19755	
*	21/94	•	13.473	- ·	******	24252	47.55	•20003•	
A .	00114	•	15-0-51		9/1/4/	00447	700	* Z U Z 55	
	1000	•	16.033	20000	00704	04/67	2765	164070	
1	60007	•	11. 10.		70.00	10000	7	00000	
0 0	52368	PERK.	11.565	05329	78.1.2.5.	26420	52662	.21199	
50	. 53537		11.236	, ,	96575	26633	54.01	.21503	
25	54542	~	10.703	0	.54450	.26950	5543	.21801	
25	. 55336	ě	10.257	O	.55923	.27190	. 56.845	.22093	
53	. 57323	?	9.638	. 05112	.57387	.27415	. 58258	.22378	
3.0	. 59262	•	9. 351	. 050 34	58852	•27623	2965	.22655	
٠ د د	ED.109.		200	24640	φı	•27.515	17 ES	42622*	
91	66170	,	61.0	* 0 4 0 4	.01/65	056120	747	*23156	
	0.629	•		20140	D 4	64107	00000	24407	
	077C0 •	• •	6.00	04694	עים	262420	46.73	46.0000	
: 5	£7894		6.672	01660	6.7545	23520	68162	26455	
62.	69332		6.99	. 64272	6440	28623	6955	24374	
29	. 70771		5.459	. 04135		.28701	7096	.24565	
63	. 72213		6.943	. 03993	.7 2038	.28763	7238	.24785	
\$	. 73643	Ņ	6.423	44860.		.28808	. 73796	.24975	
65	. 75087	٠.	3.691	.03691	.7 4962	.28637	. 75212	.25155	
99	. 75642	+	3.392	• 03519	.76540	.28850	. 76743	.25337	
29	. 78197		2,687	400	.7 8118	-26644	. 78275	• 25506	
69	19791		2.046	315	• 7 9695	228218	19506	.25661	
6	01510.		1.373	20	12191	21197	. 61342	.25501	

POINT	11 31	AHANAR	N H	ATA	SURFAC	SURFACE COORDINATE	NATE DATA	⋖
NUMBER	×	>	ANGLE 1	ANGLE THICKNESS	SX.	ኤ	A P	Ϋ́
•	+ 52961	. 27314	.686		.82645	.28734	. 82878	.25924
71	. 94416	. 27323	032		.84417	.28615	. 84415	.26031
72	. 85971	. 27312	777		.85987	.28505	. 85955	.2612∄
73	. 87526	. 27 28 1	-1.546		.87555	.28371	. 87496	.26190
4.	.89381	. 27228	-2.341		.89121	.28215	69043	.26241
72	. 90630	. 27153	-3, 160		*9068*	.28035	. 90587	.26271
76	. 92199	.27.156	-4.303		•92245	.27832	. 92136	.2628⊍
7.7	. 93745	. 25936	-4.873		.93802	.27634	. 93688	.26267
7.8	. 95 3 3 3	.25791	-5.763		.95357	.27351	. 95244	.26230
52	. 96.855	. 26622	-6.673	.00913	80696	.27.174	. 96802	.26170
51	. 98413	. 25427	7.607		• 98456	.26770	. 98364	.26:84
81	. 99965	. 26296	-8.562		1.00003	.26440	. 9993	.25972

(9LADE INLET ANGLE.)	(BLADE OUTLET ANGLE.)	(BLADE LEADING EDGE RADIUS AS A FRACTION OF CHORD.)	(BLADE MAXIMUM THICKNESS AS A FRACTION OF CHORD.)	(BLADE TRAILING EDGE HALF-THICKNESS AS A FRACTION OF CHORD.)	(LOCATION OF MAXIMUM THICKNESS AS A FRACTION OF MEAN LINE.)	(MERIDIONAL CHORD OF SECTION.)	NORMALISED RESULTS - ALL THE FOLLONING REFER TO ABLADE HAVING A MERIDIONAL CHORD PROJECTION OF UNITY					LOCATION OF CENTROID RELATIVE TO LEADING EDGE
* 35.926	H +8.710	* .03229	r .05343	£ .93229	× .5335	<b>z</b> 2.3356	- ALL THE FO	= 1.9333	£ 14.644	* 45.635	. 03836	MIROTO RELATI
BETAL	BE 142	YZERO	-	YOME	-1	CORD	NORMALISED RESULTS	BLADE CHORD	STAGGER ANGLE = 14.644	CANBER ANGLE	SECTION AREA	LOCATION OF CE

ANGLE OF INCLINATION OF ONE) PRINCIPAL AXIS TO "X" AXIS = 14.451

PRINCIPAL SECOND MOMENTS OF AREA ABOUT CENTROID

IPX = .00013 (AT 14.451 MITH "Y" AXIS)

IPY = .00216 (AT 14.451 MITH "Y" AXIS)

POINT MEANLINE DATA SURFACE COORDINATE DATA

NUMBER X Y ANGLE THICKNESS XS YS XP

.03237 0.31000 35.926 .00473 .00094 .00189 .10379 -.03189 .01628 .01628 .01628 .01628 .01628 .01682 .01682 .01682 .01682 .01682 .01682 .01682 .01682 .01689 .01682 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689 .01689

CENTROID

MONENTS OF AREA ABOUT

SECOND

.48.38 .23769

XBAR # YBAR # .00232

POTM	*	1 1	32 G	¥	SURFACE	COORDI	NATE DATA	•	
NUMBER		: } : <b>&gt;</b> -	VGLE 1	×	SX	rs xp		<u>a</u>	
4	15725	-	ģ	0.30	.14984	-	1646	66780.	
15	16917	13778		. 93186	.16147	.12172	. 17688	.09363	
3	. 18109	-	8	633	.17311	61	, 18906	• 8 9955	
17	. 19333	**	D	К	.18478	-	. 20122	.10515	
18	. 27274	. 12578	2	936	19433	14192	. 2114	.10965	
<b>1</b>	. 21247	₩,	Ė	0376	16502	• •	* 22104	11400	
53	12222	٠,	8 8	0000	645120	A 11	25052	11039	
42	. 23194		ġ	1	v		04040		
22	90142	٠,	Ö k	1 6	+12024	•	20000	• •	
52	141.62	,	ġ;	. 04663	767470	^ .	. 20045	10000 T	
• u	27074	4 4		3	25477		24000	•	
3 %	28362	16132	73.	9	27149		. 28975		
2.6	20036	•		9	.28123	18876	29948		
25	30379		Ŋ	250	.29100	ž	. 30918	.14997	
2	30983	-	8		30079	976	- 31667	*	
e M	. 11956	-	่ส			.20228	. 32653	*	
H	32930	1.5341	8	0	-	59	. 33817	•	
32	33903		8	-	· P7	961	. 34778	•	
er.	. 34877	13364	5	0	.34016	3	. 35737	•	
34	35953	-	2	0	~	168	. 36797	~	
35	. 37333	-	3	•-	1	228	. 37 655	.17333	
36	* 36237	N	7	అ	.37301	267	. 36912	.17646	
22	. 39183	N	7	0	.38397	304	• 39969	.17954	
36	. 43263	W	7	. 05375	7676£°	3	• 41026	.18250	
39	. 41337	. 21141	15.983	. 35415	•4 0591	374	. 42082	.18538	
£3	. 42413	. 21443	ħ	. 15448	•41668	<u>ه</u> .	. 43138	.18817	
41	. 43493	. 21735	Ä	* 05475	.42786	438	• 44194	.19089	
4.2	• 44556	. 22417	#	¢	44 3883	.24678	. 45250	•19355	
<b>6.3</b>	. 45643	.22288	13.	0	*44983	.24963	• 46306	.19613	
ţ	. +672?	. 22550		. 05519	.46077	.25234	. 47362	•19867	
<b>\$</b>	. 47796	.22804	13.	. 15521	•47173	.25493	. 48419	.23115	
<b>\$</b>	. 45873	.23049	ä	. 05516	.4 827 0	.25740	• 49476	.2358	
¥.7	64664*	. 23287	ä	+05595	• 49365	.25976	. 50534		
4.6	• 51326	. 23517	ij	• 05487	.50463	•26232	. 51592	w.	
6.7	. 52133	.23741	11.591	. 05463	.51554	.26417	\$ 52652		
23	23242	N	=	9 (	.5501b	15002	00340	• (	
15	10001	. 24310	3	<b>3</b> 1	20.00	34607	70100	v (	
25	. 56423	. 24577	<b>;</b>	0	*****	2	00000	•	
23	. 57659	N 6	÷ (	9	27/47		. 2020	062224	
t u	67774	01242		3 6	C 100 C*		- 73/CU	• •	
22	- 0.00 ·	25511	•	2 6	400348		62544	, .,	
2 2	775.7	25764		9 C	A 107 B		6395	"	
	45056	25937		. 04757	164742		65366	1 57	
e g	F6493	26121			69299		. 66777		
` <b>.</b>	67932	26.293		, .	67675		1	•	
, <b>,</b> ,	69371	26451	9	1	v		. 69601		
62	70813	26596	Ś	9423		•	5	~	
63	. 72249	. 26728		040	•	•	ţ	"	
9	. 73688	25847	;	539	~	ഩ	7384	w	
. F.	75127	26951		037		- en	23	14	
99	• 76679	. 27649		• 03603		.28846	2	"	
29	. 76232	. 27129	ດໍ	Ħ	~	•	. 78311	14	
68	. 79784	.27192	4.9	323	.79728	•	\$	.25578	
69	. 81335	. 27237	÷	303	.B1301	60	37	.25718	

POI NT NUM 9ER	lil T ×	A Y. L I	N E O Angle t	MEANLINE DATA Y. ANGLE THICKNESS	SURFACE XS	E COORDI YS	SURFACE COORDINATE DATA	A YP
7.9	. 82839		.613	. 02842	.82874		42904	.25843
71	. 84441		121	. 02641	77778		864438	000000
72	. 85933	. 27257	876	. 02436	.86012	28474	85975	26139
73	. 87546		-1.655	. 32227	.87578		87513	-26109
74	. 89398		-2.459	. 92016	.89141		89055	26169
25	• 90651		-3.286	.01801	.90702		90599	.26193
76	. 92233		-4.135	• 01584	.92263		92145	256198
7.7	. 93755		-5.308	• 01365	.93814		93695	.26184
7.8	. 95317		-5.932	. 01144	.95366		. 95248	26147
79	. 96863		-6.818	. 0921	.96914		96805	.26186
83	.98412		-7.754	. 00698	98459		98365	25999
51	<b>79666</b>		-8.713	- 00473	1.00000		39928	2 SARK

ť

(BLADE INLET ANGLE.)	(BLADE OUTLET ANGLE.)	(BLADE LEADING EDGE RADIUS AS A FRACTION OF CHORD.)	(BLADE MAXIMUM THICKNESS AS A FRACTION OF CHORD.)	(BLADE TRAILING EDGE HALF-THICKNESS AS A FRACTION OF CHORD.)	(LCCATION OF MAXIMUM THICKNESS AS A FRACTION OF MEAN LINE.)	(MERIDIONAL CHORD OF SECTION.)	lyalised Resuls — All the Folloning refer to ablade having a meridional chord projection of (
= 37,394	66 <b>9</b> °9- =	± .91229	= .05477	622 û 0 ° ×	± •5333	= 2,3866	S - ALL THE FOLL
8E TA1	BETA2	YZERO	-	YONE	2	CORO	MALISED RESULT

UNITY NO.

= 1.0334 = 14.671 STAGGER ANGLE BLADE CHORD

CAMBEP ANGLE = 46.213

SECTION AREA = . 13929

LOCATION OF CENTROID RELATIVE TO LEADING EDGE

XBAR = .46331 YBAR = .20817

SECOND HOMENTS OF AREA ABOUT CENTROLD

IX = .90316 IX = .90297 IXY = .00353

ANGLE OF INCLINATION OF (ONE) PRINCIPAL AXIS TO "X" AXIS = 14.509

PRINCIPAL SECOND HOMENTS OF AREA ABOUT CENTROLD

(AT 14.519 HITH 'X" AXIS) (AT 14.509 HITH 'Y" AXIS) IPX = .99933 IPY = .80221

POINT	A E	7	۵ س	<b>4 + 4</b>	SURFACE	COORDI	NATE DAT	DATA
NUNBER	×	<b>&gt;</b>	ANGLE T	X Y ANGLE THICKNESS	Ř	S XX	X B	4
-		- 21688		. 50473	.00093	.00188	. 29383	00188
۰.		.37667	36.635	• 00689	.01208	.01163	. 31623	• 0 26 10
<b>•</b>		. 31752		*0600 *	•02326	•02118	. 32857	.01386
3		12597		.01116	244200	•63152	* 34092	.02141
. To		. 33421		.01326	.04570	.03966	. 05325	.02876
. uc		- 14226		. 11533	•05696	.04661	. 36554	• 0 3591
		. 05013		. 017 37	.06825	.05738	. 07781	.04288
. =0		. 15781		. 01937	.07956	66290	. 39006	19670.
• •		36532		. 129.34	06060*	.07434	. 10227	.05629
		. 07265		. 02327	.13226	.08256	. 11447	.36274
=======================================		. 37952		. 02517	.11365	.09360	. 12664	+0690+
12		. 35684		. 02703	•12506	84860.	. 13878	.07519
13	. 14377	. 39370		. 02884	.13650	.10619	. 15090	.0 6120

1								
POINT NUMERA	₩ *	1 1 1 1	N E D	A T A HICKNESS	SURFACE	E COORDINA YS X	TE OAT P	٨ ٨
						:		
3	15549	-	29.630	Č	479	.11375	7	(3)
15	. 16726	٠.	26.923	32	594	.12114	. 17508	.09283
91	. 17913	-	28.433	ž	709	.12839	. 18713	0
17	. 19031	₩.	27.962	3	954	.13550	. 19917	.10400
e0 (1	. 20 17 3	. 12495	27.568	. 57.00	.19214	.14135	. 23 926	• 4 0 6 5 5
2.5	60173	4 .	641.7	1 20	0 T T	16276	22027	~ •
21	23336	٠,	2 2 2	, 5	12	15831	93939	12174
22	. 24725	ű	25.845	041	311	.16375	24939	
23	. 25913		25.377	3	408	.16918	. 25937	.43312
2,5	-26912	**	24.893	120	507	.17430	. 26933	**
52	. 26931	ų,	24.394	642	695	17940	. 27926	Ħ
92	. 27979	w	23.879	g	704	.18438	. 28917	.14204
24	. 26968	.16753	23.247	• 04729	2803	42691	29905	₩,
D (2	10667 •		166.22	9 (	2	165610	. 51691	•
, .	V 2.545	•	25.75	7	֡֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֡֓֓֓֓֓֡֓֓֡	1,0001.	47816	м ,
3 3	12022		230.12	. 55074	100	777.00	42625	15000
1 C P	33911		20.4.30	9.5	X 401	7117	34.0	•
וייין פשו	34933	Ť	19.605	522	3431	21561	35784	•
**	.35987		19.133	. u529ù	3512	.21389	. 36.853	•
35	* 37374	u.	18.434	. 35355	3522	.22430	. 37921	•
36	. 38161	.23215	17.783	. 05414	733	.22793	.38988	.17637
37	. 39248	.2:557	17-154	. 05467	446	.23169	+5005+	•17945
33	. 40335	-2.886	16.549	. 15514	355	.23529	. 41121	• 18244
6.0	22919	. 21233	15.969	. 05554	, je 2	23873	. 42186	₩,
3 4	45507	10117	12.414	ָ ֡ ֡ עַ עַ	710	202420	45.75	-
10	14694	20073	14.004	0105.	407	7.64.76	01044	19203
'n	. 45771	22361	13,934	.05651	900	25193	. 46453	•
ţ	. 46858	N	13.454	35	*46203	.25377	. 47516	-
<b>4</b> 5	. 47945	. 22881	13. 3 32	• 95663	4730	.25638	3	w
94	. 49932	.23128	12.637	• 65654	484	+25887	. 49651	N
29	. 50119	.23369	12.271	. 05641	952	.26125	. 50719	.20613
en (	. 51236	. 23692	11.933	55	362	-26352	. 51787	u,
7	. 5223	2.000	11.023	200	710	20000	1 4974	A £
51	55163	24.398	10.87	0.0450	45.7	1007°	55679	.21697
1 60	56598	.24667	10-402	. 05435	610	.27339	. 57866	N
53	. 58033	N	9.972	. 05361	756	*27565	. 58497	N
Ú.	. 59467	. 25171	9.533	• 65279	903	.27774	<b>• 59904</b>	.22568
iv i	-649)2	-25406	9.176	. 05187	640	-27967	. 61311	S I
ž.	. 62337	62942	6.617	929	195	-28144	. 62718	<i>N</i> 6
	71150.	T#056	7.136	,	740	3	*21+9*	N 6
0.00	. 66641	. 25225	7.141	. 04737	534	25	. 56436	23875
9	. 68376	. 26399	6.525	3	6781	866	. 68342	•
61	. 69511	. 25559	6.103	3	6 927	378	. 69748	W
29	.7º9+6	. 25705	5.566	3	073	385	. 71155	*24554
. Q	. 72381	. 26838	5.017	7	7219	8	. 72563	W (
<b>1</b>	.73615	. 26957	4,456	3	365	3	. 73971	N
٠ د د	. 75253	27062	3.504	. 03853	7512	6	. 75381	<b>(7)</b> (
94	78147	27277	202	27950	900	26075	76699	v
. <del>.</del>	1000	27298	1.012	; ;	2 6 6 0	ð	70010	40
. <b>.</b>	61426	27.340	1.209	16200	81396	28698	61461	25792
;	i i		•	3	)	3	) } !	:

POINT	ui E	ANLI	N	ATA	SURFACE	E COORDI	NATE DATA	⋖
NUMBER	×	<b>&gt;</b>	ANGLE T	Y ANGLE THICKNESS	XX	XS YS XP		۲Þ
73	. 92973	. 27363	* 484	• 02895	.82961	.28810	. 82985	.25915
71	.84518	. 27366	264	. 02689	.84524	.28711	.84511	.26021
72	• 86162	.27348	-1.334	. 92483	.86085	.28588	• 86343	•26139
73	. 97637	. 27319	-1.827	. 32266	.87643	.28443	. 87571	.26177
7.4	. 83151	. 27250	-2.643	• 02050	. 6 91 99	.28274	. 89164	.26226
75	. 93696	.27167	-3.475	.01831	.90751	.28381	• 90643	• 26254
75	. 92241	. 27 362	-4.331	. 01603	.92301	.27864	. 92180	• 26263
77	. 93785	. 25933	-5.296	. 11385	.93848	.27623	. 93722	.26244
78	. 95333	. 25789	-5.132	. 61159	.95391	.27356	. 95268	*26204
73	• 9687 ^a	. 25633	-7.016	. 10931	.96931	.27365	. 96817	.26141
83	. 98419	. 25400	-7.949	502ur.	-98467	.26748	• 98373	.26052
81	. 99963	. 25171	-8.899	• 09473	1.00001	.26405	. 39927	.25938

Fire the Care Care Alexander

# 37.995 (3LADE INLET ANGLE.)  # -9.156 (BLADE CUTLET ANGLE.)  # -9.157 (BLADE LEADING EDGE RADIUS AS A FRACTION OF CHORD.)  # .9528 (BLADE MAXIMUM THICKNESS AS A FRACTION OF CHORD.)  # .97220 (BLADE TRAILING EDGE HALF-THICKNESS AS A FRACTION OF CHORD.)  # .5039 (LOCATION OF MAXIMUM INICKNESS AS A FRACTION OF HEAN LINE.)  # 2.4459 (MERIOIONAL CHORD OF SECTION.)	NORMALISEO RESULTS - ALL THE FOLLOWING REFER TO ABLADE MAVING A MERICIONAL CHORD PROJECTION OF UNITY ************************************	LE = 14.795 E = 47.151	SECTION AREA = .04022 LOCATION OF CENTROID RELATIVE TO LEADING EDGE	X3AP = %47994 Y3AR = %21321	SECOND 40MBNTS OF AREA ABOUT CENTROID  IX = .90117  IV = .30212  IXY = .00355	ANGLE OF INCLINATION OF (ONE) PRINCIPAL AXIS TO "X" AXIS = 14.659 Principal second homents of area about centroid	IPX = .03013 (AT 14.659 WITH 'Y' AXIS) IPY = .37226 (AT 14.659 WITH 'Y' AXIS)
96TA1 85TA2 YZERO T YONE Z CORD	HORMALISED RESUL	STAGGER ANGLE CAMBER ANGLE	SECTION AREA LOCATION OF	22	SECOND 40MB	ANGLE OF IM PRINCIPAL SE	AA

- 0 1186 - 0 5020 - 0 1163 - 0 1163 - 0 2699 - 0 2618 - 0 4989 - 0 5648 - 0 5648 - 0 6915 - 0 7528

. 03361 . 016608 . 05272 . 05272 . 05272 . 05466 . 05470 . 08470 . 11322 . 13322 . 13322 . 14322 . 14322 . 14322

.001186 .001172 .003177 .003177 .00478 .005774 .006533 .0096633

.01091 .01169 .01169 .01169 .01169 .013394 .016723 .016936 .111036 .1111336 .131393

37.261 35.261 35.261 35.32 35.128 35.128 31.275 31.275 31.275 31.275 31.275

19236 1939 1939 19326 19566 19606 19699 11326 11326 11326 11326

ď, DATA

SURFACE COORDINATE
XS YS XP

N E D A T A ANGLE THICKNESS

N L I .

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x

POINT KUM 3E A

POINT MARKETO	¥ ₩	AHLI	2 W 10 W 1	TUTCHECE	SURFACE	E COORDINATE	MATE DATA	4 A	
Y SE ROLL	•	-	3191	CCOMPT	ĝ.	2	L C	Ļ	
1	. 15349	•	Ŕ	8	.14582	3	. 16117	•0 47 05	
15	. 16512	7	R	ñ	.15714	3	. 17310	.09276	
91	.17674	7	8	Ä	.16848	얆	. 18501	• 0 9835	
17	. 18837	-	8	×	.17983	2	. 19691	.10383	
18	. 19346	7	Ŕ	Ŗ	.18979	2	. 20722	• 10852	
67	. 23856	7	Ŕ	R	•19963	2	. 21751	.11312	
20	. 216/3	7	8	3	*2 0952	ĸ	. 22778	.11764	
27	. 22874	•	8	3	•21946	8	. 23882	.12208	
25	. 23683	•	ĸ	3	.22943	3	. 24824	.12643	
23	. 24593	•	K)	3	-23642	*	. 25843	•13169	
ž	. 25972	•	Ŝ	Ž.	54652.	7	. 26360	.13486	
52	. 26911	•	ż	3	• 2 5948	2	• 27 875	•13895	
<b>5</b> 6	. 27 923	7	Ŕ,	3	•26954	줐	, 28886	.14293	
27	. 28933	•	ĸ	3	.27964	앜	. 29896	.14683	
28	. 29939	7	Ŕ	3	.28976	3	.30902	.15062	
62	. 30948	~	ห่	2	•29990	2	. 31906	.15431	
30	. 31956	•	ಸ	2	.31037	忒	. 32908	.15790	
31	. 32967	•	ಸ	2	*32027	8	. 13906	.16139	
32	. 33976	7	ន	3	.33050	¥	. 34902	.16477	
33	34 935	•	<del>\$</del>	2	.34075	М	. 35896	.16804	
3	. 36057	•	6	Ĭ.	.35196	5	. 36978	.17153	
35	. 37159	•	2	ž	.36319	8	. 38963	.17483	
36	. 38231	•	Ä	ĸ	.37442	Š.	. 39141	.17806	
37	. 39393		Ä	8	.38565	7	• 40222	.18119	
36	. 43496	•	9	8	.39689	2	. 41302	.18422	
39	. 41598		5	26	•43814	9	. 42382	.16716	
<b>6</b> 3	. 62743	•	\$	2	.41938	ŭ	. 43461	.19061	
4	+ 43832		3	6	•43652	Ż.	. 44541	•19260	
25	. 44974	•	*	2	.44186	3	. 45 621	.19551	
5 4 3	• 45036	•	7	2	• 45310	7	. 46701	.19817	
<b>3</b> (	67 106	•	j	3	.46433	7	. 47782	.29077	
, t	. 48210	•	1	3	•47556	È	+48864	*2325*	
61	. 19512	•	Y,	ă	9/494	Ŋ,	94664.	.23563	
<b>;</b> :	* 1406	•	ý :	7	55.75 ± 6	9 9	92914.	15837	
9 0	626.	•	i:	7 0	125C4*	2.7	. 52112	470120	
Û	107C	•	:	. 4	24473	! :	54660	21626	
, v	55475		9	1	64648	1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	21071	
25	56899		9	11.	56395	. 2	57404	22230	
53	. 58324		9	×	57845	2	56804	. "	
7	. 59751		6	16	£ 9299	=	. 60203	.22812	
55	. 61177	•	Ġ	2	•63754	×	. 61601	4	
56	.62534	?	ė	2	.62210	4	. 62998	.23366	-
25	. 64031		•	8	•63566	2	. 64395	w	
20	18159	•		5	•65122	2	. 65792	•23690	
6	. 66664	•	٠,	3	•68579	ַ עַ	67.189		
<u> </u>	.65313	•	۰	3	•6 58 35	2	. 66585	.24379	
79	. 69737		١٥	3	26469	2	29669	N 1	
29	. 71154	•		3 :	7.1947	Ø :	. 71350	N 1	
3 :	06421	*	۸.	γ:	50427	e s	11121.	150520	
	11641	•	•	3	10001	? !	0/14/0	v	
6	****	•	, ,	51	115679	Ž.	. 12212	v	
643	0,60,1	•	•	3 !	7/90/	2:	000//	25775	
. 4	414.00			} ;	70088	1	2000	25074	
9 4	A4574	27661	1.177	. A3463	81544	6 2000	* 000 C	26050	
ì	) 1 2 3	•	4	;		1	) } •	****	

Point Number	X X	A A L I	N E O	HEANLINE OATA Y ANGLE THICKNESS	S URF ACI	E COORUI YS	SURFACE COORDINATE DATA XS YS XP Y	Α Υ
Ş	91 12 8	27559	723		.83097	.29128		.26191
2;	07.400	-0.00			64948	29322		.26294
25	004000	27675	1.277		.86198	28892		.26378
2,	0.100 •	27594	27.74		44778	.28739		.26443
7 .	07 / 00 ·	46777	2.874		69287	.28563		.26488
<b>+</b> 0	CC2C0 •	07/170	-2.723		.90828	28352		.26512
2 4	93769	27.75	7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.		.92365	.28138		.26515
0 6	0 7 C 2 C 2	27404	45.656		.93899	.27888		.26495
- 6	95.55	WE5/6	-6.365		.95430	.27614	١.	.26451
0 0		04840	-7.28g		196957	.273%		.26384
n e	000000	25554	-8.211		68483	26930		<b>*</b> 2 62 92
	99962	75407	49.156	. 33472	1.00000	.26640	• 39925	.26174

The state of the s

# # # # # # # # # # # # # # # # # # #			(BLADE INLET ANGLE.) (BLADE LEADING EDGE RADIUS AS A FRACTION OF CHORD.) (BLADE MAXIMUM INICKNESS AS A FRACTION OF CHORD.) (BLADE TRAILING EDGE HALF-THICKNESS AS A FRACTION OF CHORD.) (LCCATION OF MAXIMUM INICKNESS AS A FRACTION OF WEAN LINE.) (MREIDIOMAL CHORD OF SECTION.)	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	02141 06142 YZERO T 7 CORU
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WORTHLISED RESILTS - ALL THE FOLLDNING REFER TO ABLADE MAYING A WERIDIONAL CHORD PROJECTION OF UNITY RESERVED SECTION OF UNITY

LOCATION OF CENTROID RELATIVE TO LEADING EDGE = 15.045 * 46,535 - .04112 1.3352 STAGGER ANGLE CAMBER ANGLE SECTION AREA MAGE CHORD

X348 c .47913 Y748 c .21612

SECOND HOMENTS OF AREA ABOUT CENTROLD

\$1\00\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 400\ = 444 ANGLE OF INCLINATION OF CONEY PPINCIPAL AXIS TO "X" AXIS = 14,906

CAT 14.976 MITH 'X' AXIS) PRINCIPAL SECUND MONENTS OF AREA ABOUT CENTROLD * . 909/5 44

Pol st	*	1114	3 E	REALLINE GATA	SURFACE	E COORD INA TE	NATE DATA	
HUN BEA	¥ ,	<b>&gt;</b>	ANGLE 1	HICKNESS	ž	ñ		g.
**	2 60 2 3 5	-	39.112	5.36.7.	78:00-	.09183	. 10335	03163
<b>~</b>	. 31.332	0.3919	34.312	. : 56.93	.)11.66	.01193	. 21.599	.00645
m	. 92523		17.524	. 53921	.0 2248	+02177	. 52809	.01446
•	. #3575		36.753	. 01141	•0 3334	•03137	. 04616	• 0 2223
٠	. 94621		15.933	. 01359	.04422	4 C 400	. 05220	.02974
٠	• 35964		15.247	.31572	.05514	78640	6421	.03703
	. 97 % %		325.4	. 01743	•0999•	.05879	. 07619	.04410
•	. 36263		33.816	. 11993	.97707	-36749	. 06814	405096
æ	4.3961.		22.132	. 02193	.18807	.07534	. 10006	• 05762
<b>6</b>	. 17553		12.471	. 12392	.2 9911	+0.6428	. 11195	.06419
11	. 11693		32.5%	. 12587	.11017	68269	. 12361	.07041
75	. 12846		22.52	. 92778	.12126	.10131	. 13566	.07655
77	. 13932		19.61	. 12965	.1 32 36	.19835	. 14747	.08254

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r H	<b>ju</b> t	•				!		:
3	. 16.5 24	11201	15. 141	1 2 0	~	1155	•	(A)
	15.224	1454		72.1	1946	45.7	•	0.00
	17431	11501	256.83	0 m	.16581	45.332	•	1660
	14575	. 1.21.32	23, 392	0356	.17699	.13742	•	952
	. 1961.	17697	25-173	1381	.18717	1.6373	٠	100
	\$ 25 E4 5	1.3240	27.752	7396	.19724	.1.932	•	140
	. 21683	. 1.177	20.139	0193	.23739	.15611	•	195
	\$1122.	. 1930	28.953	. 342 35	.21757	.16197	•	1241
	. 23786	224-1-	37, 375	98.00	.22773	.16752	•	202
	24782	. 15133	. Ser.	NO 175.	.23862	458 47	٠	331
	. 25816	158.1	25.377	. 24614	858+ %°	41.71.	•	.13745
	. 25453	. 16314	254 - 42	+ 0+731	.25855	.13461	•	.14168
	27 WAS	.157786	2.311	13 8 8 C .	.25888	18994	٠	*
	. 28929	. 17249	23.752	. 34953	.27922	419914	•	14983
	19993	. 176.76	23.175	. 55.52	656920	.23 20	•	7
	13557	13134	22.541	. 65145	66662*	.23511	•	*
	12921	11558	21.966	. 05239	14811	7.1937	•	.16128
	33356	15968	21. 337	465325	.32087	.214.8	•	1.16486
	28.733	13.66	20.687	256.75	.13135	.21.694	•	16837
	1612	1475	73. 117	1 March 1970	38398	22.324	•	17175
	44.248	B	16.73	65555	15127	22271	• •	
	17.16.6	41.0	A0 A	164.28	A 56.66 A	21108	•	
	16.45	****		2666	1764	21617	•	- A A 2 G G
	306.35		17.272	55736	18754	23996	•	•
	60.400	25.55.6	26.652	. 05785	79851	26.372	• •	
	9.84	21424	15. 358	15625	14014	24728	•	
	12987	. 27246	15.693	25858	42186	.25.68	•	
	14007	. 22551	26. 456	- 6550	. 3328	.25393	•	
	11251	. N.1845	54.649	. 35903	17444.	.25732	•	•
	. 46 328	. 23128	13, 972	. 0591	. + 5614	<b>9</b> 6652°	٠	N
	. 47 648	23462		. 15917	**5756	.26279	•	N
	. 14569	. 23.23		. 65913	** 7898	.25547	•	.2 u788
	. 1963	. 23424		10650	9. 06 A.	.26832	•	N
	多なのでは、	. 24174		2.6450 ·	.53179	*27.46	•	.21301
	500 B	3442	12.050	. 55656	.5 1319	+27279	•	
	24046	25442		. 25625	.52657	-2750X	•	21862
		244.52		11160	CF 22 C+	27773	•	N
	. 55-640	22,22		- E-2-4-3	STEPS ST	625820	٠	N 1
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		750.4		04747	TENS.	2054 W	• •	3
	1000		7.084	14602	14	207136	• •	25.
	71.46	27.56		204.60	71225	29781	• 1	) N
	7286	27721		. 26231	72673	29639	•	255
	76276	27420	VB 3 . 9	. 341.27		.29877	•	257
	. 75692	. 27423		. C3957	15554	.29698	•	259
	.7724	. 25016	3. 148		77.105	.29898		13
	\$2484	. 26396	2.427	. 03576	. 7 4649	.29877	•	.26303
	24261	29165	1.687	0.0000	.8 5192	.29633	•	545
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POINT	tui Æ	ANLI	(I)	ATA	SURFAC	E COORDI	NATE DAT	×
NUM BE R	*	<b>&gt;</b>	ANGLE 1	Y ANGLE THICKNESS	SX.	۲S	XS YS XF	<b>Y</b>
7.3	. 83276		. 153		.33272	.29677	. 83279	.2671
71	. 84792		647		.84808	.29554	. 84777	.2681
72	. 86339		-1.461		.86342	.29428	. 85277	• 855 <b>8</b> 9
73	. 97826		-2.293		.87873	.29268	.87780	.2695
7.4	. 89343		-3.142		• 8 94 B B	<b>.29</b> 384	• 89286	•2699
75	. 90 863		200 - 4-		• 9 0 9 2 5	.28875	. 93795	.2701
92	. 92377	. 27825	-4.890	. 31641	192447	.28642	. 92317	.2730
2.2	46386		-5.788		•93365	.28385	. 93822	.2698
78	. 95410		-6.791		62456	.28102	. 95342	.2693
79	. 96927		-7.628		£6696*	<b>.27734</b>	. 96865	.2685
90	<b>ካካካ86 •</b>		-8.570		26486	.27461	. 98391	.2676
4	40000		40.524		4.00000	27412	. 99922	X 9 5 6 4

		* .)1226 (BLADE TRAILING EGGE HALF-THICKNESS AS A FRACTION OF CHORD.) * .5330 (LOCATION OF MCXIMUM THICKNESS AS A FRACTION OF MEAN LINE.)		<b>S</b>		ZE = 15,239	959.64 = 37	18 n 34336	LOCATION OF CENTROID RELATIVE TO LEADIN; EDGE	134R = 047854 1942 = 021697	second woments of area about centrold	IX = .03119 IX = .03222 IXY = .90358	ANGLE OF LHCLINATION OF (CHE) PRINCIPAL AXIS TO "X" AXIS = 15.167	FRINCIPAL SECOND MOMENTS OF AREA ABOUT CENTROLD
BETA2 BETA2	TZERO T	7046	C0 40	HOR HALISED REST	the water Charles	STAGGER ANGLE	CAMBER ANGLE	SECTION AREA	LOCATION OF		SECOND 46M	~~~	ANGLE OF LI	FRINCE PALL

M. 595 M.

. 10387 . 025855 . 026855 . 054805 . 05496 . 05392 . 07563

SURFACE COORDINATE DATA

N E D A T A ANGLE THICKNESS

7 T

T.

POT M NUMBER

(AT 15,357 WITH 'X" AXIS) (AT 15,367 WITH 'Y" AXIS)

5 . 500 J3

181 M	u Z	* ***	- L		CIBEAC	100001	MATE DATA		
CH SER			ANGLE T	MGLE THICKNESS	XS X	YS XP		ď.	
1	. 45.924	4.7 180	13.643	. 114.03	7607	44736	4 11 4 11	_	
× ×	16169	1000	9	. 0 4 4 7 4		69167	47.000	0000	
16	17337	11637	29. 362	. C3546	15638	13183	18177	•	
ju •4	. 18445	. 12271	25. 893	. 63717	47547	.13899	19344		
16	. 19493	.12845	29.465	. 03671	.1 8571	34241	. 20416	•	
15	14502	. 1 3467	28.328	. 64919	.19597	.15182	. 21486	.11633	
53	69512	1 3960	52.569	.04164	.23626	.15605	. 22553	.12114	
100	24685	* 14787	25.7	*****	16912°	11041	2,5517	,,,,	
r M	25733	15651	20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00	. FLA.50	16077*	110/11	25775	~ ~	
36	. 25761	15059	25.563	. 04695	26767	18176	16292	13962	
25	. 26.829	.16555	25.345	. 04815	-25609	.18736	27.848	•	
26	27875	-17038	56.469	66933	.26855	.19262	. 28898	14795	
27	.28924	.17509	23.915	. 0504.3	.27903	.13813	• 29946	*,	
28	2,662*	. 17967	23, 323	• 05145	*5882*	.20330	. 30991	•	
٠ د	. 31920	. 19423	22, 713	. 25244	.3 30 0 B	•20831	. 32032	.15994	
n	. 32068	. 15865	22.084	. 05337	.31065	.21317	. 33071	.16372	
7 (	. 33116	19263	21.437	• 05425	.32125	.21786	34137	.16738	
7:	* 210	19961	20 - 7 7 3	+ 05507	.3 3167	2422*	. 35143	•	
7.5	22265	100.7	100.00		. 34253 461.00	6.7922*	. 36170	•	
, u	1000	604.74		0.0000	02100	25152	. 37.27.3	_ `	
22	4 6 7 6 F	700.7	10.03	12/60	00000	47.5700	19595	,,,	
17	EEZON .	- 0.166.	7.7.0	. 05/40 . 658.51	11//11	6/602*	00404	~ •	
100	45.854	2.070	16.561		10000	24.76	41200	• •	
2	41994	. 22251	16.062		41174	25110	42815	1 9412	
7	. 43125	. 22581	15.493	. 95962	.42329	.25453	+43921		
£.1	. 44255	. 22658	14.954	. 65987	.43483	.25780	. 45 026	•	
2,	. 45386	. 23185	14.447	• 76024	.44637	•26.95	. 46135		
43	• 46516	. 23471	13.972	• 069 14	•45790	.26389	. 47242	.20553	
<b>:</b>	47647	. 23747	13.530	. 06916	. 46943	.26672	. 48350	.20823	
7	11194	510+2	13.123	63396.	46084	*25941	. 49459	(4)	
, a	647470	2.627	7.7	0666	94754	27,198	70000		
	57168	1 (	12.302	10000	15125 51556	27670	. 52704	46	
9	56256		11.817	50550	1000	27.90.3	54904	22119	
2	. 547.37	•	11.486	* 05855	.54124	-28171	. 55290		
5.	- 55115		11.132	~	.55557	.28424	. 56675	.22743	
25	. 57524	•	10.757	. 25716	•56990	.28664	. 58057	.23346	
25.	* 58932	•	16. 159	• 05632	.58426	.28686	. 59438	.23348	
n T	6.75	•	0.943	υ.	59865	20000	. 60818	C) (	
	61167	• (	42 - 6	3 6	602700	767670	• 0417	ve	
57	64565		8.547	. 05206	6,4179	29633	64952	24485	
58	. 65974	*		~	.65519	.29779	. 66329	. 0	
65	.67382	*	7.525	1.0	69029	.29908	. 67705	.25006	
63	. 68793		6.953	e	•68503	.30019	. 69081	.25252	
19	. 72130	*	6.372	5.5	2 <b>4</b> 669•	.30113	.70457	.25487	
(V)	71617	*	5.772	66440 •	.71381	.30168	.71833	.25712	
20	61001	•	5.148	5433	•7 2621	.30245	.73210	*25924	
<b>.</b>	*74*1	•	200	5617	•7426J	.53283	74587	.26124	
٠ •	15032		•	(h)	.75598	.30301	• 75966	.26311	
2.2	78.08	16502.	3.195	. 0.36.39	.77237	42024	77443	256496	
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a	. 81854		•	10	;	20456	72470 •	2 2	
3	•				101	1	00000	Ď	

<b>4</b>	.27064	.27161	.27238	•27294	.27330	•27344	.27337	.27306	.27252	.27174	.27071	• 26943
NATE DATA XP	. 83371	. 84860	. 86351	. 87845	. 89342	• 91842	• 92346	. 93853	. 95364	. 96879	. 98397	. 99920
SURFACE COORDINATE	•3002	.29940	.29798	.29631	.29440	*2925	.28984	.28719	.28429	.28114	.27774	.27408
SURFACI	.83372	.84300	.86425	74E18.	99468*	.90382	<b>76726</b>	.94003	.95508	60026	.98506	1.00000
N & D A T A AMGLE THICKNESS	. 02995	. 02780	• 02561	. 02339	. 02114	.01885	.01654	. 11421	.01186	67600•	. 90711	. 80472
N & D A	118	835	-1.659	-2.517	-3, 379	-4.256	-5.145	-6.348	-6.963	-7.890	-6.828	-9.776
MEANLI							. 29160					
ω ×	. 83372	. 84.883	. 86388	. 87896	• 89434	. 90912	• 92420	. 93928	• 95436	+4696 •	. 98452	. 99960
POINT NUMBER	7.0	71	72	73	74	75	76	17	78	79	80	81

### ### ##############################	### ### ### ##########################
IX = 0.00125 IY = 0.00224 IXY = 0.0150	
EMATE	IPAL AXIS TO "X" AXIS = 15.262

**≱**‡

-.00179 .00690 .00590 .00536 .03118 .03573 .04603 .05994 .05994 .05994 .05994

. 10391 . 015993 . 015993 . 015993 . 015170 . 015170 . 015170 . 016170 . 016170 . 016170 . 016170 . 016170 . 016170 . 016170 . 016170 . 016170 . 016170

01179 01232 01232 012256 012256 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 015268 01526

.01082 .01139 .01139 .01266 .01256 .01256 .01256 .01266 .11919 .11919

3, 1500 40, 814 2, 1961 39, 929 2, 1652 38, 196 3, 1671 37, 352 16520 36, 528 16520 36, 528 17682 38, 167 2, 1682 38, 167 2, 1682 38, 167 2, 1682 38, 167 2, 1682 38, 168 2, 1682 38, 167 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 168 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 38, 1682 2, 1682 2, 1682 2, 1682 2, 1682 2, 1682 2, 1682 2, 1682 2, 1682

. 16236 3.1360 . 11365 . 11961 . 02696 . 02195 . 03666 . 02195 . 16756 . 11671 . 15895 . 14521 . 18496 . 16346 . 10496 . 1682 . 11536 . 1682 . 11536 . 19436 . 13797 . 19436

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SURFACE COORDINATE DATA
XS YS XP

N L I N E O A T A Y ANGLE THICKNESS

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W

POINT HUMBER

(AT 15.262 WITH "Y" AXIS)

= .309)3 = .39243

¥ &

PRINCIPAL SECOND HOMENTS OF AREA ABOUT CENTROLD

DATA YP	.09133	7	7		: :	: ";	-	7	7	7	•	17	*	7	•	7	•		-	7		4.	, ,	. 2			•	, ,	, cy	~	, i	•		,		•		, a	~			• •			C)		
	. 15755	. 16977	. 19236	20324	7740	. 23569	. 24646	. 25719	. 2679	27.85	2000	31045	. 32097	. 3315.	. 34199	45754	37408	. 38525	3964	• 43758	4187	16674 ·	45223	4634	4745	. 46575	4969	51935	5305	. 54183	5556	58312	5968	• 61059	6243	. 55450	. 56537	67905	6927	. 73641	.72009	74746	7611	. 77562	. 79050	. 61994	
E COORDINATE YS XP	.11915																																														
SURFACE	.14098 .15196	•16296	.17397	+1.0434 +1.0434	2.0516	·	N	•23663	•24714	~ ~	27803	10	m	•31103	9	*33555	79458	, IO	.37826	.38991	з.	775140	• 4 3653	*44818	*45965	•47146	4.8309	. 5 3534	.51791	•52949	•54372	.57723	· rv	vo 1	•61512 62044	1277	.65811	•	o	•73114 -	•71548	296274	75848	~	.78937	•61954 •61956	
A T A HICKNESS	.03229 .03411	335	037	500	24.7	3	345	346	947	9 K		13	553	354	25	500	2,5	358	2	059	520	֓֞֜֜֜֜֜֜֜֓֓֓֓֓֓֓֓֓֜֜֜֓֓֓֓֓֓֓֓֓֡֓֜֜֓֓֓֓֡֓֜֓֡֓֡֓֡֓֡֓֡֓֡֓֡֓֡֡֡֡	3 3	9	C 60	69	9	9	3	623	629	550	8	052		500		640	348	9	5	33	13	138	8	. 03226	
N E D Angle T	35.853 33.288	2	23	0 t	27.884	27.391	26. 552	26.357	25.816	25.258	24.404	23.4.82	22.854	22 • 209	22.545	200.00	19.413	18.693	17, 995	17.331	16.695	10.01	16.979	14.472	13, 998	13.558	13, 153	12.668	12.148	11.685	11.571	10.868	10.479	13, 165	6.629			7.613		٠	•				•	1.454	
ANLI	.1 519	1183	242	336	,	124	537	584	93	637 777	17.05	36	1.577	126	1964		36	13	163	199	2532	802	331	361	390	87.	ž,	7 6	2522	546	2575	2 K	2657	2663	7.07	3 6	773	26.	818	927	775	0 4	27.	•	593	.23314	
tit T ×	.14927	. 17187	. 18317	19379	21513	. 22565	. 23627	. 24593	. 25752	2561+	25045	. 300.00 . 300.00	. 31363	. 32125	. 53107	104747 10474	36452	. 37593	. 38734	. 39875	. 41.110	42120	. 44435	. 45579	. 46723	. 47851	1064	51283	. 52424	. 53565	. 54955	57.75	. 59159	60573	. 61971	64773	. 66174	.67575	• 68976	. 73377	. 71775	7657	75932	. 77 + 53	. 78979	. 81976	
POINT HUMBER	16 15	16	17	<b>•</b> 0 (1		51	22	23	ž	£ 5	2.0	. S.	F2	23	7 F	2 2	) 	35	36	22	9 0	P [	3	24	£3	3		<b>,</b>	<b>.</b>	5		55	23	\$ i	č i	2 20	50	23	63	61	29	? .d	<b>6</b>	99	29	<b>\$ 5</b>	

POINT		ANLI	O U	MEANLINE DATA	SURFAC	E COORDI	SURFACE COORDINATE DATA	4
NUM SER	×	<b>&gt;</b>	ANGLE T	HICKNESS	SX	ξ.	X O	۲.
7.0	. 83474	.23020	186		.83479		. 83469	.27513
71	.84973	<b>.29004</b>	-1.027		86648*		84648	.27606
72	. 86472	.28966	-1.887		.86514		. 86429	.27678
7.5	. 87979	.28905 -2.747	-2.747	• 62353	•8 B 9 2 6	.30081	. 87914	.27730
7,2	. 89469	. 28822	-3.626		•8 9536		. 89401	.27761
75	. 90967	. 28715	-4.517		.91042		. 90893	.27778
76	. 92466	. 28585	-5.419		44526*		.92387	.27757
77	• 93964	. 28431	-6.332		*94043		, 93886	.27721
76	. 95463	. 28252	-7.256		.95538		, 95388	.27661
20.	, 96952	, 28049	-8.189		.97029		<b>•</b> 96894	.27578
69	. 9846·B	. 27821	-9.131		•98517		. 98403	•27469
<b>€</b>	49939	. 27567.	-10.081		1.0000		. 29917	27735

81.40E CHORD = 1.4353 STAGGER ANGLE = 15.674

CAMBER ANGLE = 52,393

SECTION AREA = . 14338

LOCATION OF CENTROID RELATIVE TO LEADING EDGE

X3AR = .47675 Y3AR = .22466 SECOND MUMENTS OF AREA ABOUT CENTROID

IX = .00721 IY = .09227 IXY = .00352 ANGLE OF INCLINATION OF (ONE) PRINCIPAL AXIS TO 'X' AXIS = 15.492

PRINCIPAL SECOND HOMENTS OF AREA ABOUT CENTROLO

IDY = .00273 (AT 15.492 MITH 'Y' AXIS)
DPY = .06244 (AT 15.492 MITH 'Y' AXIS)

POI M	Σ *	ARLI	N E O	HEANLINE OATA V ANGETHICKNESS	SURFAC	SURFACE COORDINATE	NATE DATA	4 ×
	<b>:</b>	•			l	?	į	:
4	. 00237	9.11300	41.939	. 10473	.3 6076	.09176	. 30395	0 3176
N	. 11359		42. 338	.00713	.01125	.01261	. 01593	.0.723
•	. 32481		49.188	84600.	.02176	•02315	. 12787	.01589
	. 93693		39.182	.01161	.03231	.3333	. 03976	• 0 2424
Ŋ	. 34726		38 - 292	. 31409	•0 4289	•04335	. 05162	. 33229
φ	. 15548		37.423	. 01633	*15352	.05303	. 06344	• 0 40 0 6
~	. 1697.		36,569	. 11653	.36418	*106244	. 07522	.04756
•	. 38393		35.742	• 02069	.07488	.37159	. 08697	.05480
σ	. 09215		34.942	. 02289	•06562	.38350	. 09868	.06181
9	. 13337		34-169	. 02487	e£96a•	1680.	. 11036	.06863
11	. 11+59		33.428	• 126.89	61011	*19762	. 12200	.07518
12	. 12582		32.723	. 92887	.11801	.13585	. 13362	.08156
13	. 137 34		32.347	. £3683	.12887	.11388	. 14521	. 08777

ATE DATA (p yp			38816 18395 38816 41928 19310 41928 19642 42310 42363 19642 42310 42363 21456 45689 21456 4685 22542 46917 65395 25422 46035 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 25520 46635 2	70832 772191 773551 775271 76271 79186 80644 82186
URFACE COORDINATE YS XP	12171 12936 13684 13684 154415 15778 15778 17387 17387	20112 20112 20112 20112 21120 21120 22120 22120 23132 23132 2414	7.954 .24979 9130 .25383 9130 .25383 1444 .26485 2661 .26485 2661 .26485 2613 .27436 7363 .27723 8131 .28746 8131 .28746 8131 .28746 8131 .29531 8151 .29531 8151 .29531 8152 .30365 8153 .30365 8153 .30365 8153 .30365 8153 .30365 8153 .30365 8153 .30365 8152 .30365 8153 .30365 8153 .30365 8153 .30365	31191 31286 31387 31387 31387 31385 31333 3127
s sx	·	រប់ជំបំបំបំបំបំបំបំបំបំបំបំបំបំបំបំបំបំ	. ພິພະ ຈໍສໍສໍສໍສໍສໍສໍສໍສໍສະ ແມ່ນ ພິພະ ພິພະ ພິພິພິພິພິພິພິພິພິພິພິພິພິພິພ	
D A T A E THICKNESS	4466668640			* 6 5 5 5 6 6 5 5 5
L I N E ANGLE	***********	<b>នៃស្តស់ស្តស់ស្តស់</b> និស្	2216 18.752 22512 17.36 22565 16.755 22565 16.755 23525 15.553 23525 15.553 2445 14.55 2445 14.55 2445 14.55 25266 13.59 25525 12.51 25525	. คู่บุง จ. พ. กุง ค.
A A A A	• • • • • • • • • •	25732 150 26613 110 20085 117 31116 113 31116 113 31116 113 31110 113 3110 113 310 113 310 113 310 113 310 113 310 113 310 113 310 113 310 113 310		• • • • • • • • •
POINT NUMBER X	• • • • • • • • •	• • • • • • • • • • •	, , , , , , , , , , , , , , , , , , ,	

POINT	1. M	ANLI	O W N	ATA	SURFAC	E COORDI	SURFACE COORDINATE DATA	4
NUM BE R	×	<b>&gt;</b>	ANGLE T	X Y ANGLE THICKNESS	XX	Ř	۸ ح	<b>4</b>
2.9	. 83582		377		.83592	•31°90	. 83572	.28765
7.1	85070		-1.243		.85101	.30960	. 85643	,28153
10	86559		-2.123		.86697	.30805	.86511	.28220
, M	84948		29446 -3-309	. 02362	.68113	.33625	. 87986	.28267
7.7	89636		-3.908		60968	.33420	<b>• 89464</b>	.28292
7.2	94.125		-4.817		,91105	.30191	93945	.28295
7.2	402814		-5.736		.92597	.29935	. 92430	.28275
2.2	94337		-6.663		.94085	.29655	. 93919	.28232
. K	40450		-7.599		.95570	.29350	. 954:12	.20165
2 6	E 8 5 4 5		-8.543		.97051	.29.19	60696 •	.28073
, e	98486		6.44.6		.98527	.28652	. 98409	.27957
) <b>«</b>	25666		-10.451		1.00000	.28281	. 99914	.27815

(9LADE INLET ANGLE.)	(BLADE LEADING EDGE RADIUS AS A FRACTION OF CHORD.)	(SIADE TRAILING EDGE HALF-INICKNESS AS A FRACTION OF CHORD.)	(MERIDIONAL CHORO OF SECTION.)
# 43,286 #-13,43£	# .33228 # .35368	E . 9 228	z 2,6825
BETA1	72EP.0	YONE	Sara Cara

E 1.0399 BLADE CHORD

= 15,979 STAGGER ANGLE

CAMBER ANGLE

= 54.139

SECTION AREA = . 14368

LOCATION OF CENTROID RELATIVE TO LEADING EDGE

X3AR = .47548 Y3AR = .22988

SECOND MOMENTS OF AREA ABOUT CENTROLD

IX = .95.22 IY = .33233 IX E .33364

ANGLE OF INCLINATION OF (ONE) PRINCIPAL AXIS TO "X" AXIS = 15.756

PRINCIPAL SECOND MONENTS OF AREA ABOUT CENTROLD

(AT 15.756 WITH "X" AXIS)
(AT 15.756 WITH "Y" AXIS) = .10353 = .00249 AA

-.03173 -.06767 -.06553 -.06181 -.06181 -.06481 -.06481 -.06481 -.06481 -.06481 -.06481 -.06481 -.06481 -.06481 -.06481 -.06481 SURFACE COORDINATE DATA .02785 .03970 .05152 .66329 .07502 . 12157 . 13312 . 14465 11998 13900 .01173 .01296 .02391 .03451 .05479 .67389 .09193 .01113 .01113 .01113 .01215 .01926 .01635 .01635 .01635 .01635 .01635 EANLINE DATA Y ANGLE THICKNESS 34.245 33.487 32.767 T. POINT NUMBER

			:		ti 4 7	6	1	6
	U	. 11117	101.75	13013	010000	VICTIO	419013	71760
	COCT •	110	7	) i	10001°	01000	20107	* T C C . *
	-	00000		9 4 6 6	770010	00000	C. D.C. /T *	10001
	70704	•	200	*****	001/14	100 to 10	. 13030	27477
	2/161.			17000	*/101*	010010	17.17.	97:71
	*03F3*	1000	67:67	70T***	7476.10	212011	• 6460	4 4 4 5 5 5 4
	02577		7	10011C	410074	17007	* CC 333	16061
	245.1	20001	77 587	10 M M M M M M M M M M M M M M M M M M M	COCT 30	000	246.4	00000
	246.42	٠.	2000	34776	204079	7100	25744	4 1 1 1 0 0
	25,72	17776	1000	00000	25.546	4670	25.846	45074
	25.835	1784	76.70		25720	0,000	27012	4 554 4
	27019	1444	i k	25.00	25.55	27566	20005	1 500K
	95605	10001	901 %	20100	27001	00007*	50002	456.77
	COLUMN.	* *	24.00	. 557.70	00000	10717	44440	4 6865
	76.404		100	. 0.190	40 40 F	96266	70110	47240
	*****	٠,	20017		00000	926224	* 35503	007/10
	0.2224	202120	24,51	000000	00710	******	01000	200/10
	00778	07/. 7	21.012		426213	10000	24.	77.00
	001111	2.654	77.2	- CATOS	25.345.3	02002	16466	F + 40 + +
	4676	10010	200	A . 2044	15733	602420	20200	4 64 86
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	64 369	25457	16.819	. 05141	46.1472	25637	42248	0.000
	62522	23842	16.197	26177	4,1561	26938	15335W	20876
	. 4365	1	15.616	50250	642949	.27161	44519	.21185
	. 44545	.24491	15, 171	. 66225	44036	.27497	45655	.21486
	¥ 460 17	- 24799	14.561	• 25236	•45223	.27817	. 46791	.21781
	. 47 159	. 25395	14.768	• 06239	* 46409	.26121	* 47 928	.22070
	+ 46333	. 25392	27,651	. 06233	•47595	.28-10	• 49066	.22354
	26565	N t	13.252	• :6219	64.8779	.28686	. 53205	,22633
	30000 ·	W (	17.092	• 55196	*49963	128321	91345	63622*
	.51815	N	12.567	• 55166	.51145	*2923	. 52486	.23183
	. 52977	N I	12.282	. 36125	•52325	-29442	. 53629	.23454
	V. 1.4V.	96962 *	12.350	70000	5 35 05	27962	. 54775	52752
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	62453	N	•	. 055550	6197	.31357	<b>.</b> 52926	.25562
:	. 63335	N	•	62430	6339	.31238	. 64279	.25872
	.65253	N		. 05313	6461	.31432	. 65631	4.26153
:	* 66 6 5 1 F	. 25986	B . 1577	. 05179	622	.31556	. 56981	•26426
	76625	-29184	٠	# 051 30	764	.31680	. 66332	.26685
*	54860	~		. 04893	967	.31792	. 69682	.26940
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NUMBER	×	>	ANGLE T	Y ANGLE THICKNESS	S.	Ž.	dx Sv Sx	۸Þ
7.3	. 63693	3:240587	587		.83709	.31757	. 83678	.28723
7.1	. 85172	. 3 - 213	-1.461		•85208	.31620	. 85135	.28806
. 22	. 66651	» 3 × 163	-2.385		.86794	.31459	. 86596	.28868
73	. 86128	. 31093	-3.299		.88197	.31272	. 38060	.28908
7.	. 89637	. 29993	4.223		•8 96 85	.31.59	. 89528	.28926
75	. 91385	12862	-5.155		.91171	.33821	66606	.28922
76	. 92553	. 23726	-6. 196		492652	.30558	. 92475	,28894
77	- 94142	. 29556	-7.045		.94130	.33269	. 93954	. 28843
78	. 95521	. 29369	-8.300		*8260*	<b>.</b> 29954	. 95437	.28767
79	• 96993	. 2 3146	-8.963	. 00958	.97373	.29613	• 96954	.28667
#5 <b>©</b>	. 98477	. 29894	-9.931		• 98539	74262	. 98415	.28541
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#### SECTION NUMBER 1 '2' = 4"7500

SECTION PROPERTIES	SECTION AREA	<b>₹</b> 55	•	1.8661E-01		
	LOCATION C	OF CENTROLD TO STACK AKES	X9AR E VBAR E	-1.50 69E+00 -2.6848E-11		
	SHCOAD MOMENTS ABOUT CENTACED	MENTS OF AREA		9.4746E-13 4.6283E-12 1.9892E-12		
	PRINCIPAL GF AMER A	PRINCIPAL SECOND MONENTS OF AMER ABOUT CENTROLD	# # # # # # # # # # # # # # # # # # #	7.7865E-34 (AT 5.4979E-02 (AT	23,61 DEGREES TO "X" AXIS) 23,61 DEGREES TO "Y" AXIS)	នន
	Torsiona.	FORSIONAL CONSTANT	n	5.76692-04		
SECTION COUNDINATES						
on Trios	S # O	5.4	à	dÅ		
will d	29.437622.06	-6-79762E-91	-2.43165E+3			
Po ===	- 7. 41 F415 + 20 - 10 - 10 - 10 - 10 - 10 - 10 - 10 -	-8.263166-81	-2.37.3565+13	-8-457306-01		
•	-2.351:25.30	-7.935 365-01	-2.35338E+93			
en d	は は は は は は は は は は は は は は は は は は は	-7.7269/E-31	-2.32633E+11	-6.32538E-01		
•	-2.29518800	-7. 145 99E-01	+2.272365+0	•		
•	-2.264196.00	16-326816-9-	- 2. 24435E+49			
	000 SE 1492 120	-6,637348-01	-2.216626+33 -2.187968+03	-7.147.30E-31		
) od 1 te	-2.189376-40	-6.07865E-11	-2.157212+33			
21	-2.161%:50.90	-5-797105-35	-2.12662E+3J	ţ,		
m 4	はなるとはなるとは、なり	-5.519565-31	-2.09512E+0J	-5. 22643E-31		
* 53	004344444 004644	-5.4.50 / 55 - 5.5 -4.935 & 4.5 - 5.1	-2,329145+33	'n		
2.	-2. 336 38E - 65	-4.64872E-31	-1.994538+03			
	004 W54 4 70 W4	15-329/56-4-	*1.95663E+0.3	-5. 252 64E-31		
25	-1.95.295E-03	- 3,971316-71	-1.93906E+3 J	-		
<b>\$</b> ;	00-351 826 Te	16-30254.1-	-1.85395E+03			
22	10 10 10 10 10 10 10 10 10 10 10 10 10 1	-3.41626E-31	- 1. 87 334E+37	÷		
23	-1.651125+66	- 5. 24176E-01	-1.607188+33	*		
# S	いのもののなるのであった。	10-34-01-01-11-11-11-11-11-11-11-11-11-11-11-	-1.761356+09			
O A	304317474 -1-774515 -1-774515	16-22116-2-	**************************************			
	の日本は必要にきた。する	-2,575986-01	-1.703956+03			
42	24.724.798.00	-2.4.71215-51	· * . 67 360E+93			
194 A	40 - 12 - 12 - 12 - 12 - 12 - 12 - 12 - 1	-2.272746-01	. 4.64592E+0.			
	000325×54*X	16 - 34 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	- 1.917662+U	-3.2/154E-31		
44	000-3030-00-1-	*1.4315/c=31 *1.641215+01	1.563768+00			
	-1-568-1E-50	-1.734765-01	-1.531672+33	?		
4	-E-537722E+34	-1.571548-31	-1,53152E+03	.2		

ę,	0E+03 -2.96833E-01 9E+03 -2.158942E-01 7E+03 -1.91392E-01 7E+03 -1.91392E-01 7E+03 -1.91392E-01 7E+03 -1.91392E-01 7E+03 -1.91392E-01 7E+03 -1.91392E-01 7E+03 -1.91392E-01 7E+03 -1.91392E-01 7E+03 -1.91392E-01 7E+03 -1.91392E-02 7E+03 -1.91392E-02 7E+03 -1.91392E-02 7E+03 -1.91392E-02 7E+03 -1.91392E-02 7E+03 -1.91392E-02 7E+03 -1.91392E-02 7E+03 -1.91392E-03 7E+03	·
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٨٤	11. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4.	-8, 8326E-31 -8, 8954E-31 -8, 89448E-01 -9, 89546E-01 -8, 89548E-01 -8, 8954E-01
SX.	11. 53 59 9E 11. 57 5 5 5 5 9E 11. 58 5 5 5 9E 11. 58 5 5 9E 11. 58 5 5 9E 11. 58 5 9E 11.	-2.43195E+00 -2.43193E+00 -2.43224E+00 -2.43297E+00 -2.4339E+00 -2.4339E+00
POINT NO	2 # ###################################	ADNERIOR

	20.45 DEGREES TO 'X' AXIS) 20.45 DEGREES TO 'Y' AXIS)	
	1.7467E-31 -1.3349E+00 -2.3842E-31 6.4246E-33 4.2648E-02 5.7772E-34 (AT 4.8495E-04	YP -7.660 33E-01 -7.450 49E-01 -7.050 49E-01 -7.055 29E-01 -5.651 27E-01 -5.30 59E-01 -5.30 59E-01 -5.30 59E-01 -5.30 59E-01
	200 XX	XP 2.29 127E+0J -2.2656E+0J -2.21659E+0J -2.1659E+0J -2.13639E+0J -2.13639E+0J -2.13639E+0J -2.06309E+0J
+00 -8, 89519E-01 +00 -8, 89519E-01 +00 -8, 89508E-01 +00 -8, 89508E-01 +00 -8, 89579E-01 +00 -8, 89579E-01 +00 -8, 89519E-01 +00 -8, 89519E-01 +00 -8, 8951E-01 +00	SECTION AREA LECATION OF CENTROLO RELATIVE TO STACK AXIS SECOND MONENTS OF AREA ABOUT CENTROLO PRINCIPAL SECOND NONENTS OF AREA ABOUT CENTROLO TORSIONAL CONSTANT	7.57210E - 31 -7.57210E - 31 -7.52962E - 01 -6.69649E - 31 -6.15946E - 31 -6.15614E - 31 -6.15614E - 31 -6.15614E - 01
\$\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	SECTION AREA LOCATION OF CENTRO RELATIVE TO STACK SECOND MONENTS OF ABOUT CENTROID PRINCIPAL SECOND M OF AREA ABOUT CENT	KS -2.29737E+35 -2.27456E+30 -2.2247E+30 -2.247E+30 -2.1413E+40 -2.15594E+30 -2.15255E+00
中中公共政治政治政治政治政治政治政治政治政治政治政治政治	SECTION PROPERTIES	SECTION COORDINATES POINT NO 11 12 13 14 14 15 16 16 16 17 18 18 18 18 18 18 18 18 18 18 18 18 18

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POINT NO

d.		8E-01 -1.41858E-0 7E-01 -1.04211E-0 5E-01 -6.95051E-0
dx sa	5.6 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	13664E+02 -6.30 52614E-02 -6.05 61599E-12 -5.79
¥.S	2.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5	6. 3.848E-3 6. 88469E-0 6. 88121E-0
OINT NO	222222222222222222222222222222222222222	223

dA	1.48657E-03 3.33646E-03 4.72552E-03 6.72551E-03 8.4576E-03 8.51847E-03 7.40076E-03 7.40076E-03 7.45040E-03 1.45251E-03		
χ	-4.97528E-01 -4.69384E-01 -4.1211E-01 -3.84779E-01 -3.84779E-01 -3.86253E-01 -2.99924E-01 -2.4315E-01 -2.4315E-01 -1.86233E-01 -1.86233E-01 -1.86233E-01		
<b>A</b> S	4.64654E-12 4.55244E-12 4.41961E-12 4.33904E-12 4.21373E-12 3.97302E-12 3.97302E-12 3.07484E-12 2.78909E-12 2.37731E-12 1.46986E-12 1.46986E-13 4.2886E-13	YSEMI	-7.665 33E - 91 -7.665 30 3E - 91 -7.665 87E - 91 -7.665 87E - 91 -7.666 84E - 91 -7.666 84E - 91 -7.665 89E - 91 -7.665 89E - 91 -7.665 89E - 91 -7.659 36E - 91
XS	-4,98435E-01 -4,41220E-01 -4,12630E-01 -3,84168E-01 -3,87158E-01 -3,27158E-01 -2,9855E-01 -2,1072E-01 -2,415/7E-01 -1,86293E-01 -1,56293E-01 -1,27873E-01	XSE4I	-2.2915CE+00 -2.2915CE+00 -2.2915CE+00 -2.2935E+00 -2.29367E+00 -2.29367E+00 -2.2947E+00 -2.2947E+00 -2.2947E+00 -2.2956E+00 -2.2956E+00 -2.2977E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -2.2966E+00 -
POI'M NO	7869277777777777777777777777777777777777	POINT NO	

# SECTION NUMBER 3 'Z' = 5.5100

AXISD

			17.92 DEGREES TO "X"																														
1.6857E-31	-1.1689E+00 -1.5658E-11	4.6360E-03 4.1960E-02 1.3406E-02	4.9976E-04 (AT 17 4.6296E-02 (AT 17	4.42946-04		Q.	Ť	-6.65767E-01	•	-	-	-5. 76316E-01	•			-4. 74015E-01	-		-4.33995E-01		-3.96337E-31	-3.699.00E-J		-3. 401 80E-01		-3.12013E-01							-2.19483E-01
u	XBAR = YBAR =	XX	IPX = IPY	H.		χ	-2.18981E+8 J	-2.163486+33	-2.11.0846+03	-2,064535+03	-2.05621E+03	-2.03168E+03	-1.97 94 7E+0 0	-1.95278E+0J	-1.92637E+33	-1.67 34.25+0 3	-1.84687E+30	-1.82026E+30	-1.79357E+33 -1.76680E+03	-1.74321E+03	-1.71955E+0 3	-1.67 199E+0 J	-1.64810E+03	-1.6030kF+03	-1.57 568E+0 3	-1.55162E+00	-1,52728E+0 J	-1.47829E+01	-1.45366E+0J	-1.42892E+00	-1.40409E+00	-1.57 914E+0 E	-1.32697E+03
15.A	JF CENTROIO TO STACK AXIS	ENTS OF AREA FROID	PRINCIPAL SECOND HOMENTS OF AREA ABOUT CENTROLD	CONSTANT		YS	-6.76153E-01	-6.534866-01	-6-312C3E-01	-5.877642-01	-5.66485E-01	-5.45531E-01	-5,04654F-01	-4.84678E-31	-4.65012E-01	-4-45686E-01 -4-26666F-01	-4.079196-91	-3.834946-01	-3.71366E-01 -3.53511E-01	-3.33078E-01	-3,22868E-01	-2.93158E-31	-2.76652E-01	-Z-B4+03E-31 -2, 6362 W-41	-2.36718E-01	-2.2330E-01	-2.13180E-01	-1.84854F-01	-1.72638E-01	-1.61757E-01	-1.49228E-01	-1.0000/E-U1	-1.161148-01
SECTION AREA	LOCATION OF RELATIVE TO	SECOND MOMENTS ABOUT CENTROID	PRINCIPAL OF AREA AS	TORSIGNAL CONSTANT		SZ.	-2.1961-5-00	-2, 17 219E+0 C	**************************************	-2, 19 314E+60	-2.07593E+80	-2.05161E+00	-2.00/1385+00	-1.97794E+00	-1.95313E+00	-1.92617E+00 -1.90117F+00			-1.82582E+90 -1.831.6E+00					-1.601/6E+08				14. K1 K30F+8	-1-490905+00	-1-465705+00	-1.44 029E+00	-1.4145/E+G-0	-1.36 188E+00
SECTION PROPERTIES					SECTION COCRDINATES	POINT NO	<b>~</b>	~ '	* 4	, r.	. <b></b>	<b>.</b> 1	ú ď	<b>`</b> 3	#	27 1	3	<b>1</b>	17	<b>3</b>	Ø1 €	ដ	ន	3 1	ន	<b>18</b>	<b>1</b> 2	<b>.</b> .	S	H	N.	2 2	22

15. 1.13154E-01	POLIST NO	<del>X</del>	5.2	<b>Q</b>	Αb
15			1		
17.   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1.15   1	ኤ	. 33359E+0	1.057116-0	30 067E+3	-349 67E-
13	11	1. 335 31E+0	9.571398-3	27 422E+0	. 307 06E-0
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113 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9	1.25 1315 40	7.643595-0	22.07.3E+0	. 82695E-0
1119578E01 -5.19589E-72 -1.11653E+01 -1.65910E-75 -1.11653E+01 -1.656310E-75 -1.11653E+01 -1.666310E-75 -1.11653E+01 -1.666310E-75 -1.11653E+01 -1.666310E-75 -1.11653E+01 -1.666310E-75 -1.11653E+01 -1.6663E-75 -1.11653E+01 -1.6663E-75 -1.11653E-75 -1.11663E-75 -1.11653E-75 -1.11653E-	. 5	\$ 22747F + 5	6. 6.3876E-3	1,193665+0	. 73916E-1
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## 1.178   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1.18   775   1	17	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	A 356 20F - 2	1,113915+0	48561E-0
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49         9,80319E-01         -5,4793E-03         -9,6696E-01         -1,0973E-01         -1,0973E-03         -9,6696E-01         -1,0973E-01         -1,0973E-03         -9,6696E-01         -1,0973E-01         -1,0072E-01         -1	3	1.01875F+0	1.436785-0	9,961815-0	16498E-0
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95 -7.83519E-01 2.73547E-12 -7.69356E-11 -6.09144E- 95 -7.8259FE-01 3.47727E-02 -7.44837E-01 -6.09144E- 95 -6.97913E-01 3.47727E-02 -6.817269E-01 -6.09144E- 95 -6.97913E-01 3.47727E-02 -6.817269E-01 -7.84932E-01 -6.97913E-01 -7.84932E-02 -6.81736E-01 -7.84932E-01 -	ď	8.1234 iF-0	321665-0	7.97010E-0	.71378E-0
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57         -7.26297E-01         3.47427E-02         -7.14455E-01         -4.99952E-03           58         -6.97913E-01         3.47427E-02         -6.9776E-01         -7.9776E-01         -6.9776E-01         -7.9776E-01         -6.9776E-01         -7.9776E-01	3	7.54829E-0	12265E-0	7.41832E-9	. 48965E-3
\$\$ -6.97913E-01	15	7.26297E-0	47427E-0	7.14455E-3	. 96952E-0
59 -6.69723E-01 4.87193E-02 -6.60192E-01 -3.8220E- 61 -6.4273E-01 4.82478E-02 -6.60192E-01 -3.84777E- 62 -6.86192E-01 4.82478E-02 -6.60476E-01 -2.4909E- 63 -6.86192E-01 4.82478E-02 -6.06476E-01 -2.4909E- 64 -6.337778E-01 4.82478E-02 -6.06476E-01 -2.39247E- 65 -6.337778E-01 -2.4348E-02 -6.06476E-01 -2.39247E- 65 -6.33778E-01 6.3368E-02 -5.2636E-01 -1.37478E- 66 -6.333778E-01 5.03348E-02 -6.2636E-01 -1.37478E- 67 -6.323778E-01 5.03348E-02 -6.3649E-01 -1.37478E- 68 -6.333778E-01 5.03348E-02 -6.3649E-01 -1.37478E- 69 -6.333778E-01 5.03348E-02 -6.3649E-01 -1.37478E- 69 -7.3256E-01 5.0338E-02 -6.35366E-01 -1.453192E- 60 -7.3253138E-01 5.02548E-02 -2.35146E-01 3.76645E- 77 -2.33348E-01 5.03348E-02 -2.35146E-01 4.46418E- 78 -2.33348E-01 3.75374E-02 -2.35146E-01 4.46138E- 79 -2.533648E-01 3.753748E-02 -2.35146E-01 14.6645E- 70 -7.54418E-01 3.753748E-02 -2.35146E-01 14.65459E- 71 -1.4729E-01 2.61338E-02 -2.35146E-01 14.6645E- 72 -1.74718E-01 3.75378E-02 -2.35146E-01 14.66458E- 73 -2.533648E-01 2.61538E-02 -2.35146E-01 14.66458E- 74 -1.4729E-01 2.61338E-02 -2.35146E-01 14.66458E- 75 -2.533648E-01 6.85538E-01 -2.71408E-02 -5.03623E-  61 -7.548331E-01 3.75731E-02 -2.35146E-01 14.656458E- 73 -2.54936E-01 6.85538E-01 -2.71408E-02 -5.03623E- 74 -2.54936E-01 6.85538E-01 -2.71408E-02 -5.03623E- 75 -2.54936E-01 6.85538E-01 -2.71408E-02 -5.03623E- 75 -2.54936E-01 6.85538E-01 -2.71408E-01 -2.54768E-01 -2.71408E-01 -2.54768E-01 -2.71408E-01 -2.54768E-01 -2.54	2	6-979135-0	7-3107E-0	6.87240E-0	. 353 28E-0
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62 -5.86192E-31	61	6-138396-0	52478E-0	6.06476E-0	. 840 96E-0
63 -5.584)4E-01	29	5.86392E-3	63760E-0	5.79736E-9	. 392 67E-3
64 -5.33778E-01 4.93672E-12 -5.56296E-01 -1.56766E- 65 -5.3377E-01 5.01336E-02 -4.99567E-01 -1.23192E- 66 -5.3377E-01 5.01336E-02 -4.99567E-01 -1.23192E- 67 -5.429501E-01 5.02933E-02 -4.11666E-01 -5.73426E- 63 -5.429501E-01 4.95057E-02 -4.11666E-01 -5.73426E- 64 -5.32504E-01 4.95057E-02 -4.11666E-01 -5.73426E- 73 -5.2323640E-01 4.95057E-02 -5.9420E-01 1.35693E- 74 -5.233546E-01 5.0538E-02 -5.9420E-01 1.35693E- 75 -5.33516E-01 3.75501E-02 -5.9420E-01 1.35693E- 76 -5.33516E-01 3.75501E-02 -5.9420E-01 1.35693E- 77 -5.93546E-01 3.75301E-02 -5.9420E-01 4.40106E- 78 -5.33516E-01 3.75301E-02 -5.94201E-01 4.40106E- 79 -5.33516E-01 3.75301E-02 -5.94201E-01 4.40106E- 79 -5.33516E-01 3.75301E-02 -5.94501E-01 4.40106E- 70 -5.33516E-01 3.75301E-02 -5.94501E-01 4.40106E- 71 -5.53516E-01 3.75301E-02 -5.94501E-01 4.40109E- 72 -5.33516E-01 3.75301E-02 -5.94501E-01 4.40109E- 73 -5.33516E-01 3.75301E-02 -5.94501E-01 4.40109E- 74 -5.53516E-01 3.75301E-02 -5.94501E-01 4.40109E- 75 -5.33516E-01 3.75301E-02 -5.94501E-01 4.40109E- 75 -5.33516E-01 3.75301E-02 -5.94501E-01 4.40109E- 76 -5.33516E-01 3.75301E-02 -5.94501E-01 4.40109E- 78 -5.33516E-01 3.75301E-02 -5.95010E-01 4.40109E- 79 -6.55056E-01 3.75301E-02 -5.95010E-01 4.40109E- 79 -6.55056E-01 3.75301E-02 -5.95010E-01 4.40109E- 70 -5.53516E-01 4.9556E-01 -5.95031E-01 4.40109E-02 -5.93628E-01 -5.95031E-01 4.40109E-02 -5.93628E-01 -5	73	5-584346-0	834-88E-0	5.53015E-0	. 97475E-3
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2.18331E+00 -6.861747E-3 2.19021E+00 -6.85034E-3 2.19116E+00 -6.85276E-0 2.19116E+00 -6.85454E-3 2.19172E+00 -6.8558E-0 2.19250E+00 -6.8559E-0 2.19259E+00 -6.85631E-0	OINT H	Š	SEN		
2,183512400 -6.8504475-5 2,193275+00 -6.850346-3 2,193165+00 -6.854546-3 2,193726+00 -6.855935-3 2,192766+00 -6.855855-3 2,192795+00 -6.856545-3 2,192795+00 -6.856315-3					
2.1912/15.10 2.1911/2010 2.1911/6E-00 2.1911/6E-00 2.1911/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1921/6E-00 2.1	<del>4</del> 4 <b>1</b>	2, 18 351E+6	6.84747E-5		
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2.19152E+00 -6.8553E-0 2.1923GE+00 -6.85658E-0 2.1923GE+00 -6.85671E-0 2.19298E+00 -6.85671E-0	• 4	7-10042-7	6. 854545 6. 854545		
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2.19298E+00 -6.85633E-0		2.19249E+0	6.85671E-3		
	•	2, 1929&E+0	6-856335-9		

					16.42 DEGREES TO 'Y'				
		1.64.94.E-01	-1.1193E+30 -1.4565E-01	3.9954E-03 4.1170E-02 1.20 06E-02	4.5626E-34 (AT 4.4707E-02 (AT	4.20 06E-04		<b>d</b> ⊁	-5.33596E-01 -5.45236E-01 -5.4538E-01 -5.6236E-01 -5.45390E-01 -5.2457E-01 -4.96496E-01
		62 ° H 5.8753	XBAR = YBAR =	IXY IXY	# AdI	u		Α×	-2.13176E+03 -2.10447E+03 -2.05330E+03 -2.05330E+03 -1.9589E+03 -1.9689E+03 -1.94159E+03 -1.94159E+03
IN35A	-6.05532E-01 -6.05377E-01 -6.05377E-01 -6.05451E-01	SECTION NUMBER & 'Z' = "percettor of the control of	OF CENTROID TO STACK AXIS	ENTS OF AREA ROID	PRINCIPAL SECOND MOMENTS OF AREA ABOUT CENTROIO	CONSTANT		<b>S.A.</b>	-6.25135E-91 -5.01096E-01 -5.0126E-01 -5.0126E-01 -5.107E-01 -5.10703E-01 -4.76640E-01 -4.5913E-01
XSE4I	-2.19337E-30 -2.19336E-30 -2.19536E-30 -2.19537E-00 -2.19557E-00 -2.19557E-00 -2.19577E-00 -2.1977E-00 -2.1975E-00 -2.1973E-00 -2.1973E-00 -2.1973E-00 -2.1973E-00 -2.1973E-00 -2.1973E-00 -2.1973E-00 -2.19693E-00 -2.19693E-00 -2.19693E-00 -2.19693E-00 -2.19693E-00 -2.19693E-00 -2.19693E-00 -2.19693E-00	SECTION SECTION SEE	LOCATION C RELATIVE 1	SECOND HOMENTS ABOUT CENTROLO	PRINCIPAL OF AREA AB	TORSIONAL		S	-2.135 1E-0 6 -2.1321E-0 0 -2.0535E-0 0 -2.0535E-0 0 -2.01357E-0 0 -1.9535E-0 0 -1.9535E-0 0 -1.9535E-0 0
POINT NO	~ C I Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z	SECTION PROPERTIES					SECTION COORDINATES	POINT NO	**************************************

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11	1.637.5E+0	4.213 C4E-0	\$6367E+0	. 65453E-3
12	. 552 762 +3	4.02580E-0	1.63 390E+J	. 53415E-0
2	1.836512+0	3.844485-9	1. 85 699E+0	. 356 39E-3
*	1.811 19E+2	3.666 SEE - 3	1.78323E+0	. 21245E-0
53	755525 00	3, 492546-3	1.75 352E+3	37072E-3
3	4.759595.0	3. 32154E-0	1.726662+0	93211E-0
2	1.7542020	3.154235-1	1.70 3265+0	. 796.39E-1
91	1.71246200	3,016115-3	1.677636+0	. 683 38E-0
41	1+63357E+0	2, 850 335-0	1.655405+0	. 57 3 36E-0
R	1.665762+0	2.7-6325-1	1.632946+0	. 46393E-3
だ	1,645745+0	2,614,89年	1.61347E+0	. 35656E-0
Z	-1.62462E+00	-2.46575E-31	+1.58798E+83	-3.251.3E-01
ສ	1.672388+0	2.35910E-3	1.565462+0	. 147 53E-D
<b>3</b> 2	1.583)4E+0	2.234595-0	1.542916+0	. 045496-0
22	1.557576+9	2-213426-3	1.523345+9	. \$5.5E+0
2	1.534.34E+0	1.93462E-0	1.49773E+3	. 04.7 57E-3
r.	1.512276+0	1.875516-0	1.475.95+0	.75155E-0
ž.	1.689-3E+3	1.765225-9	1.452415+0	. 65750E-0
£	\$ * 466 * 6E * 3	1,654785-3	1. 42 959E+3	. 565 47 E-3
2	1.4. 3366.0	1-5-12-3	1. 40 692E+0	. 47550E-0
ed (	1.423125+0	1. 642 815-0	1.384135+0	. 36761E-3
다.	1. 33574E+0	1.341626-3	1. 36 124E+0	. 33183E-0
2	1. 37 322E+0	1.243195-0	1. 33 832E+3	. 21827E-3
*	1. 346 . 5€+0	1-142316-0	1-313666+0	. 13154E-0
ž	1.32279€+3	1-045216-1	1.289396+0	. 047146-3
¥	1.29762E+0	9.51687E-J	3,26484€+8	. 965 C7E-3
1	1.271365+0	8.618746-0	1.240236+0	. 88 5 22E-3
70	1-24640E+3	7.757225-3	1.21554E+3	. 8U7 46E-3
2	T-22075E+3	6.93161E-0	1.19079E+0	.73165E-0
9	1.195115+3	0-366055-9	1.165956+1	. 657 70E-0
7	1.169176+9	5.38445K-0	1.141936+0	. 585 37 E-3
?	1. 14 324E+G	4.65G26E-B	1.11603E+0	, 51441E-0
ņ	1-11721E+3	3,96556E-0	1.092936+3	. 44487E-0
4	1. 491136+0	3.330435-3	1.355742+0	. 37671E-J
Ž.	1.454306+0	2,664515-0	1.04046+0	. 30 9 85E-0
3	1.03860E+0	2.05632E-3	1.01584E+0	. 244 18E-J
7	1.01221E+0	1.474662-0	9.09525E-0	. 17962E-3
*	9.657335-0	9-18640E-0	9.63898E-0	. 115 90E-0
64	9-59166-6	3.638365-3	9.381485-0	. 352 86E-0
r,	9.293612-3	935 876-4	9. 39 31.3E-3	. 83547E-3
27	9.99567E-3	358446-3	8. 80 520E-0	. 15923E-0
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53	6.403176-9	72636E-3	8.23 346E-0	. 850 93E-0
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10	D-362509" Z	5-3758E-0	7.65701E-9	. 64516E-0
<b>2</b> €	7.50 BE 2E-0	935 31E-3	7. 37 367 6-3	. 02479E-0
15	7.21115E-0	343546-0	7.084555-3	. 454 St E-0
<b>6</b> 5	6-91++19-3	56775E-1	6.79861E-0	. 98782E-0
Ť	6.61791E-0	957 335 -0	6. 51 28 3£-0	. 363 56E-0
9	6. 32 £ 66E-0	215495-0	6.227175-0	. 880 45E-0
79	6.025682-0	641 33E-3	5.94161E-9	. 40170E-0
29	5.729396-4	6-304169	5.65611E-3	. 94997E-0
29	5.4346vE-0	745522-0	5. 37 06 35-0	. 52512E-3
ű	13953E-0	916535-0	5.08 513E-0	. 125 19E-0
Š	6.664926-0	995 05E-3	79960E-0	. 75134E-1
3	4.523-JE-0	0+358-0	4. 48 77 4E-3	. 37957E-0
*9	8-32-202	054 8 CE - B	17572E-0	. 044 37E-0
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d.	-7.39433E-03 -4.76193E-03 -2.51991E-03 -6.28352E-04 0.17736E-04 1.87644E-03 2.69654E-03 2.69654E-03 2.69654E-03 2.69654E-03 2.69654E-03 2.69654E-03 2.69654E-03 2.69654E-03 2.69654E-03 2.69654E-03	
Ж	-3.86350E-01 -3.25103E-01 -2.25031E-01 -2.561201E-01 -2.2945E-01 -1.96445E-01 -1.67046E-01 -1.67046E-01 -1.67046E-01 -1.04051E-01 -7.25110E-02 -9.31621E-03	
٨S	5.02500E-92 4.9568E-92 4.6556E-92 4.6556E-92 4.55417E-02 3.955875-92 3.955875-92 3.73671E-02 3.73671E-02 3.4621E-02 2.25170E-92 1.73196E-02 1.73196E-02	4 SE H I
ST.	-3.9616101 -3.9616101 -3.2616101 -2.923166-01 -2.65186-01 -1.966376-01 -1.661876-01 -1.661876-01 -1.661876-01 -1.661876-01 -1.966876-01 -1.9666101 -1.9666102	XSE 4I -2-13176 E+00 -2-13218 E+00 -2-13316 E+00 -2-13316 E+00 -2-13316 E+00 -2-13316 E+00 -2-13316 E+00 -2-13516
POINT NO	8974744444 8974744444 897474444 897474444 89747444 89747444 8974744 8974744 8974744 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 897474 89	0 = ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~

# SECTION MUMBER 5 '2' F 6.2573

Section properties	£115	SECTION AREA	4EA .		4	1.6887E-01			
		LOCATION RELATIVE	LOCATION OF CENTROLO RELATIVE TO STACK AXIS	KB AR	4 4 4 4 4 4	-1.0801E+30 -1.3255E-01			
		\$20040 MO ABOUT CER	SECOND MOMENTS OF AREA ABOUT CENTROID	XXX	ले जे <del>ले</del> म म म	3,6772E-13 4,2616E-02 1,1659E-02			
		PRINCIPAL OF AMER A	Principal Second Moments of area about centrolo	x to did	3 3 3 H	4.5312E-34 (AT 4.5842E-32 (AT	15.46 DEGREES TO 9	×	AXIS) AXIS)
		TOPSIONAL CONSTANT	CONSTANT	-	J.	70-36005-7			
SECTION COOPDINATES	S 71 9h	-							
1104	POINT HG	KS	43	æ		Ğ.			
-	**	75.114 :45.00	-5.957295-11	-2-107776+33		-6. 05227E-01			
	~•	-2.08852E+00	-5.74898E-31	-2.07972E+JJ		-5.87076E-01			
-	٠.	-2.63736E+30	+5.32417E-31	-2.02375E+03	•	-5.51969E-01			
	•	-2-011726-00	-5.117 31E-31	-1.99585E+30		-5. \$4994E-01			
-	۰ و	30+35' 986' 1-	-4.913925-81	-1.96 131E+0 J		-5. 15314E-01			
	. •	41.934576+64	-4.5172W-31	-1.912496403		-5. 45961E-01			
	o die	-1.938585+00	-4, 324,375-31	-1.88481E+10	•	-4. 70366E-01			
	<b>S</b>	-1-85250E+00	-4-135246-01	-1.65720E+03		-4. 54959E-01			
	1 6	-1-89097E+00	-3.44940E-01	-1.62'305E+0.4	•	4. 24. 22.			
- **	: 3	-1.434466+00	-3,56827E-31	-1.77 4735+33	•	-4-10768E-31			
•	*	-1.77 \$77E+0C	-3-413235-01	-1.74737E+3		-3.95668E-01			
	<u>s</u> :	-1.75264E+50	- 3, 24, 88E - 34	-1.72307E+D >		-3, 826 33E-01			
		-1.73723E+30	-2,93941E-31	-1.66567E+13		-3.56070E-31			
	2	-1.679 Y7E+36	-2.77975E-31	-1.64 382E+0 3		-3. 45611E-31			
	<b>5</b> £	-1.65784E+9E	-2.65230E-31 -2.637476-34	-1.62290E+99		-3. 25.339E-31			
	3 25	-1.61521E+30	-2.4 14 325-01	-1.57843E+03		-3, 153 17E-01			
	2	-1.59381E+00	-2.28392E-31	-1.55669E+03		-3.05591E-31			
	<u>ت</u>	-1.972146+30	-2,16600E-31	-1.534976+03	•	-2.96056E-01			
	2 2	0004330004444 000434004444	-2.050626-31	-1.51327E+0J		-2.00/14E-01			
- ••	្រង	-1.5u755E+60	-1.42766E-31	-1.46994E+03		-2,66622E-01			
	S	-1.465925+00	-1-32322-01	-1.44831E+30		-2.59678E-01			
	SZ:	-1.46+322+50	-1.61551E-31	-1.42669E+0J		-2. 51338E-01			
	£ :	-£.44.215E+00		-1.40509E+0.3		-2.43004E-01			
	4	-1.42322E+90	-1.4%62E-34	-1.X8350E+0.3		-2. 348 79E-01			
	12	-1-17-17-17-00 -1-17-17-17-00 -1-17-17-17-17-17-17-17-17-17-17-17-17-1	144 440 VCC 144	-1.340376+03		-2, 19258E-01			
	12	-1-15 3955-00	-1,13530E-01	-1.31862E+0 )		-2.11769E-01			
	41	-1.129566.00	-1-039925-01	09+32562*T-	•	-2, 937 395-61			
	À	-1.3512E+0		* 1. 2/ 191e*	•	-1. 950 79E-01			

<u>e</u>	-1.68594E-3	-1.61318E-0	-1.74241E-0	-1.67361E-0	-1.63668E-3	-1 - 541 435-0	-1.47791E-0	-1.415825-0	-1. 35511E-J	-1.29568E-1	-1. 237 43E-J	4. 180 25E-3	-1.12397E-0	-1.058455-0	-1.00073E-0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0-200707-0-	-7 - 461 94 F=0	-6 - 864-93E-1	-6. 20797E-J	-5.73076E-3	-5. 19121E-3	-4.67256E-0	-4. 175 52E-0	-3 - 69 8 94E-0	-3. 74473E-3	-2. 61339E-1	-2. 32563E-0	-1. 64323E-0	-1.28567E-3	-9. 69445E-0	-0 - 61 + 54 E - d	-4 - 324 57 E=0	-5.52225E-04	7 . 588 39E-0	1.622736-0	2. 468436-0	2. 369.26E-0	2110000001	0-020 TTE-0 0-020 TTE-0 0-020 TTE-0	-2.67003E-3	-5. 15277E-0									
2	784E+0	416E+0	1,239465+0	1.17575E+0	1-15 3015+0	1-129245+0	1-13 56450	1-081615+3	1.057752+0	1.03 384E+0	1-03 9906+0	9. 65 938 6-0	6-369019-6	9. 37 781E-0	9.07 816E-D		0-3066 /4 •0	7. AA 1055-0	7.584996-0	-26715E-D	6.989526-0	6.69236E-0	6.39476E-0	6.097572-0	0-384509	7.50 34 / F-D	7. 20 5455 0	4.61.249E-0	4.28918E-0	3.965802-3	3.64232E-0	3. 31. 854E-0	C-3/440/0-0	-2.34650E-01	2.02168E-0	1.696925-0	. 37 158E-3	. 04 582E-0	0-325061	540X2F-0	618915-0	931376-0									
4.5	5.616165-1	7.754515-1	6.957415-0	6.153116-0	5.4.1.945-0	4.733C3E-7	4.05566E-0	5.4.1875E-J	2.731286-3	23204E-9	1.639705-3	1-112896-0	5.910495-0	917116-3	83325E-3	アール ひとでんしつ		100 100 100 100 100 100 100 100 100 100	0-370499	2664JE-0	613%4E-0	928 SCE - 5	211665-0	-23865-0	676 98E - 3	20 - 10 to 1	1 17 1 1 1 C - C	232362-3	244176-1	253476-9	21311E-0	1 50 CBC - 1		4. 62249E-32	362356-3	1524251	69752E-3	E-312462		100000	132695-3	2549XE-3		INSSA	6.05227E-0	6.055265-0	6-05776E-0	.03973E-3	6-291165-5	C-120704-0	-6, 66202E -61
52	23364E+0	1.25512E+3	1,231566+0	1.236955+0	1.152338+0	1-157065-0	1.132966+0	1-136235+0	1.053476+3	1-05468E+0	1. 03.357E+B	1. 93 9 3 XE+D	9.641746-0	9.592596-3	9. 28 31 46-0	2		8-04-04-04-04 8-04-04-04-04-04	7-736538-6	7-427766-0	7.119225-0	6- 62 39 36-6	6.502596-0	6. 1951 35-0	5-037665-0	0 - 12 - 12 - 12 - 12 - 12 - 12 - 12 - 1	6. 95.71.65-0	0-317.199	6. 32817E-3	3. 9957 JE-0	7.66355E-8	6 - 44 C. 155 - 4	2-67334F-0	-2.3%322E-03	2.01.1572-0	1.68168E-3	1.15324E-0	0-30-626-1 0-30-626-0	0 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	- 560 196-0	795105-0	J-627E-0		ISE4I	- 13 7 7 7E+G	2.154222.0	2.10359E+0	• 10 91 9€ • B	Z-13971E+B	#4 W#4 0 0 0 0 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	2. 121.3E
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### CTION NUMBER 7 "Z" = 7.00

CONTINUE	SECTION PROPERTIES	SECTION AREA	REA	¥I	1.3536E-01	
## ADUIT CENTROLD  PRINCIPAL SECOND HONENTS  ## ADUIT CENTROLD  TITY = 1.33618 - 0.2  FREA ABOUT CENTROLD  TITY = 1.33618 - 0.2  FREA ABOUT CENTROLD  TORSIONAL CONSTANT  ## ABOUT CENTROLD  TORSIONAL CONSTANT  ## ABOUT CENTROLD  ***CONSTANT  ***CONSTANT		LOCATION	OF CENTROID TO STACK AXIS		-1.1527E+00 -1.2660E+01	
PRINCIPAL SECOND HOMENTS  TORSIONAL CONSTANT  **S***		SECOND MO ABOUT CEN	9 O F	>	4,2113E-03 5,3819E-02 1,3985E-02	•
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NO XS YEARS	CTION COCRDINATES					
-2.14.25E+0 -5.752.06=01 -2.1372E+01 -2.10.572E+01 -2.10.552E+01 -2.10.572E+01 -2.10.572E+01 -2.06.42E+01 -2.			48	ď	<del>k</del>	
-2.037676.00 -5.51276-01 -2.04978-01 -2.064286.00 -5.314886-01 -2.064286.00 -5.314886-01 -2.0649786.00 -5.314886-01 -2.0649786.00 -5.314886-01 -2.0649786.00 -5.314886-01 -2.069786.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.991496.00 -1.9	<b>.</b>	-2.14425E+30	-5.97 CO1E-01	-2.13772E+0	φ.	
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-1.98398640 -4.69117E-01 -1.56240E+01 -1.99571EE-01 -1.99751EE-01 -1.997	<b>~</b> •	-2-0113795+36	-4.895(56-31	-1.99149E+0		
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	POTest 40	26 339C+3 26 339C+3 25 394E+3	#S 8-5+266E-0 7-19628E-1	XP • 24 794 E+0 • 22 389 E+0	YP -1.93082E-0 -1.86029E-1
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## SECTION WUNDER 9 '2' E 7.7509

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* 2 %	LOCATION OF CENTROIO RELATIVE TO STACK AXIS	MENTS OF AREA TROTO	PRINCIPAL SECOND NOMEHIS OF AREA ABOUT CENTROLD	TO'STONAL CONSTANT		SA	-6.504#9E-04	*5.25868E-31	-5.629362-01	-5.55517t-01	-5.1.0965-01	-4.92547E-01	-4,714656-01	-4.318:7E-01	-4-11175E-01	- 3,73233E-01	-3.548725-01	-3.358795-01	-3.040405-02	-2.891105-91	-2.61883E-01	-2.4600JE-01	-2,157475-01	-2.05587E-01	-1.92749E-11	-1,63072E-01	-1.562496-01	-1.447 825-31	-1.33678E-01	-1, 229,465-11	-1.01752E-01	-9-138385-72
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2	1.263466+0	6.236446-0	1.22476E+0	. 967 48E-0
£	E-236 34E+0	5,432555-0	1-197346+0	. 894 22E-0
ş	1,234236+0	4.6377115-7	17 365E+0	. \$2356E-0
4	1.18 J46E+0	3.61929E-3	1.14 3975+3	. 753 85E-0
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·				15.27 DEGREES TO 'Y' AXIS)			
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OINT MG	#5 	45 436,95 6,00,63	XP 2.031255540	YP 19917F=3
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! <u>**</u>	1.952566+3	4,211266-3	+94.269€+9	67663E-3
	1.95 1972.03	4.512:95-3	1.91227E+0	72465E-3
5	1.92525201	3.61755E-3	1.061935+3	4 45E-0
بې	1.696502.0	3.62736E-1	1.85164E+0	42753E-1
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ħ.	1-652425+0	2.17728E-2	1.59982E+0	. 33501E-3
و م	1.62527E+0	2. 03527E-3	1.57255€+0	. 19495E-1
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,e	1.354.198.0	6.17665E-3	1.29844E+0	. 23777C-0
<u>.</u>	2 - 31 = 64E + 1	7.155 385-3	1.269915+0	15395E-0
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ŀ,	6.651325-3	35265E-1	6.45252E-0	. 656 59E-J
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## ECTION NUMBER 11 "Z" c 6.508

	CEGREES TO *X*	CEGREES TO "Y" AXIS!																												
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<b>33</b>				ĝ.	-2.39729E+0 /	-2,332176+9	-2.29936E+33	-2,23570E+	-2.20 384E+0 3	-2,14,9535+03	-2.10905E+0J	-2.07769E+üJ	-2.015276+91	-1.984198+03	-1.42 1162+13	-1.89136E+37	-1.86114E+3	C+366038*5*	-1.77 167E+0 J	-1.741245433 -1.741245433	-1.68188E+93	-1.652356+0)	-1.62291E+UJ	C D411 4 C C 6 C 5 C 1	-1.53518E+0 )	-1.50 612E+30	-1.477156+0	-1.44 827E+0 3	Control of the Contro	-1.35639E+0
ECTION AREA OCATION OF CENTROID ELATIVE TO STACK AXIS	SECOND NUMENTS OF AREA ABOUT CENTROLS PRINCIPAL SECOND NOMENTS	OF ARER ABOUT CENTROID Torsignal Constant		SA	+7.72349E-01	-7.196335-91	-5.61649E-31 -6.53346E-31	-6.263176-01	-5.996476-51	10-3698449-5-	-5.2+6+96-91	10-35-510-5-	-4.55980E-11	-4-343 34E -01	-4-1 32 000 -01 -4-475 057 - 34	-3.724916-31	- 3. 53223E-31	-3,159176-71	-2.978958-31	-2.672365-41	-2-46352E+04	-2.31253E-01	-2,142380-31	-4.956755-52	-1.634725-31		-1.420546-01	-1.293906-01	-1-166 JOE -01	-1,439185-01 -9,177475-02
SECTION AREA LOCATION OF RELATIVE TO	Negoco nomento Asout CENTROLO PRINCIPAL SECON	OF ARER A TOASIONAL		Z.	-2-4:59:E+3(	-2.3-894E+GC	-2.22.241E+0.0	2.263 38+00	3.4555985.5- 3.4555985.5-	-2.176-405-40	-2.14/185+63	10. 4. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6.	-2,059365-50	-2.030725+00	はなる。はないのとは、これ	95+3792 %5 · T+	・10・10×10・1×10・10・10・10・10・10・10・10・10・10・10・10・10・1	-1.456222.000	-1. 8272 E+5 6	204171887.1-	1. 73 BRSS +08	-1.71357E+00	-1-66 1 23E+0 6	50451515514 50451545514	394342651-	-1.563:9E+GB	-1.53 3 36E+0C	-1.52 356E + CC	-1-47 364E+00	-1.6>938E+30
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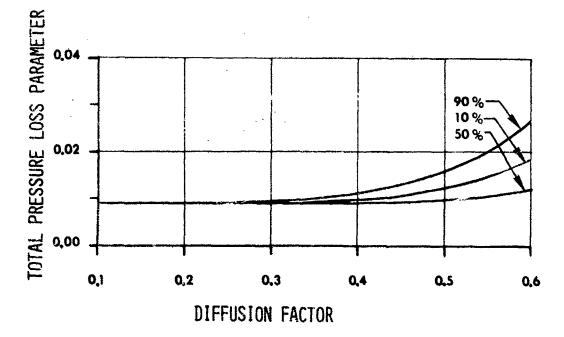


FIGURE 1A. ROTOR LOSS PARAMETER VS DIFFUSION FACTOR

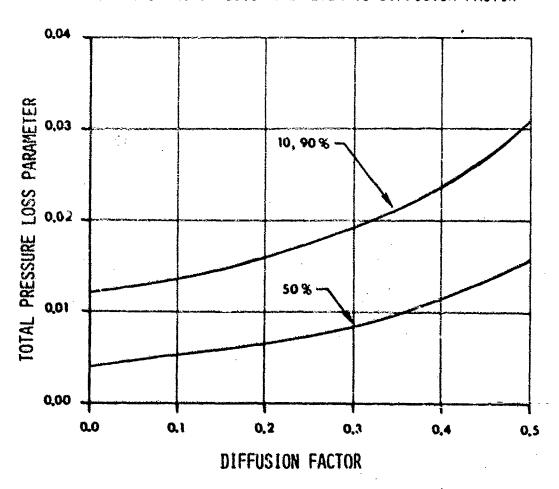


FIGURE 18. STATOR LOSS PARAMETER VS DIFFUSION FACTOR

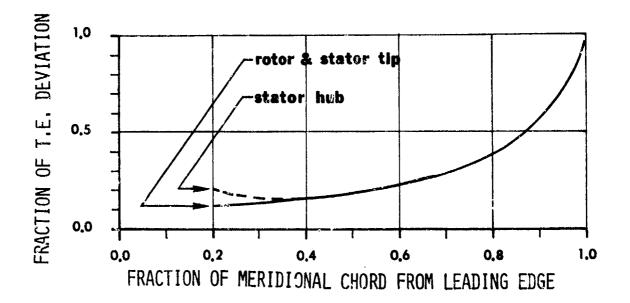


FIGURE 2. DESIGN DISTRIBUTIONS FOR INTRA-BLADE DEVIATION ANGLE

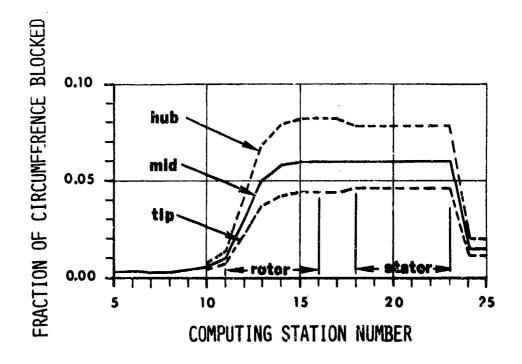


FIGURE 3. MERIDIONAL DISTRIBUTION OF BOUNDARY-LAYER AND WAKE BLOCKAGE

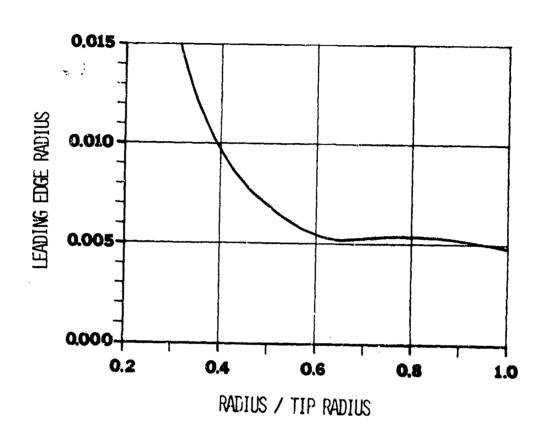


FIGURE 4. ROTOR LEADING EDGE THICKNESS DISTRIBUTION

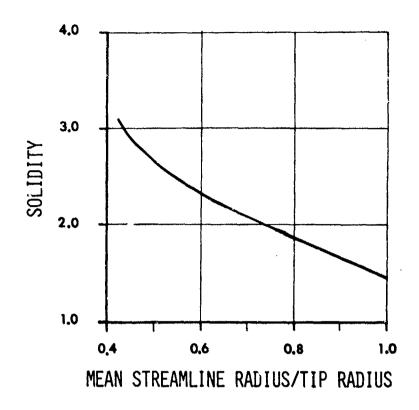


FIGURE 5. ROTOR SOLIDITY DISTRIBUTION

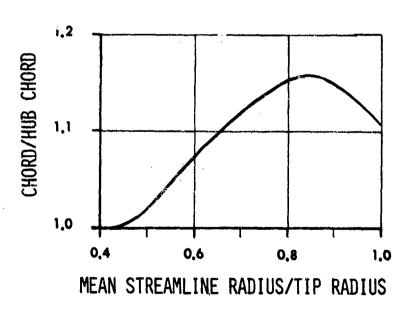


FIGURE 6. ROTOR CHORD LENGTH DISTRIBUTION

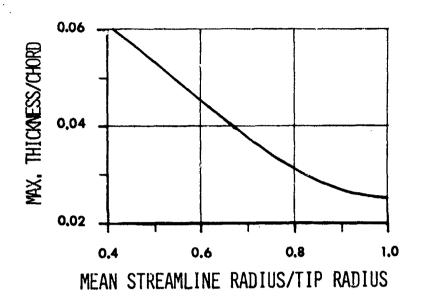


FIGURE 7. ROTOR THICKNESS-TO-CHORD RATIO

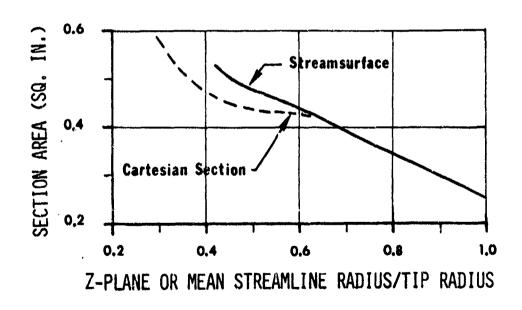


FIGURE 8. ROTOR STREAM SURFACE AND CARTESIAN SECTION AREA DISTRIBUTIONS

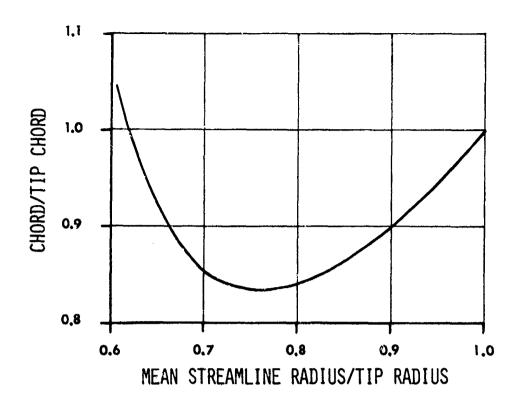


FIGURE 9. STATOR CHORD LENGTH DISTRIBUTION

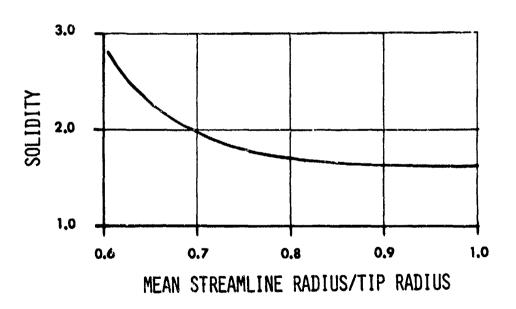


FIGURE 10. STATOR SOLIDITY DISTRIBUTION

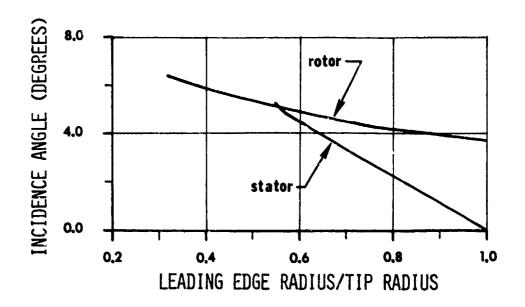


FIGURE 11. ROTOR AND STATOR INCIDENCE DISTRIBUTIONS

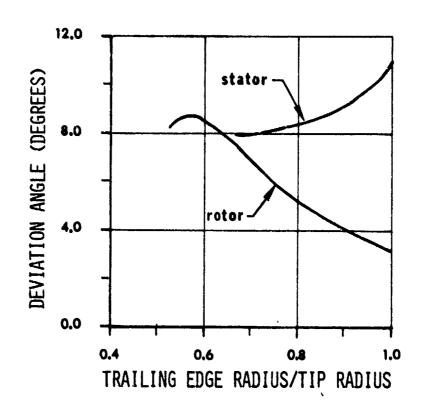


FIGURE 12. ROTOR AND STATOR DEVIATION DISTRIBUTIONS

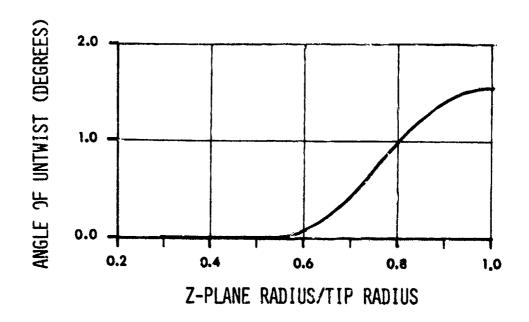
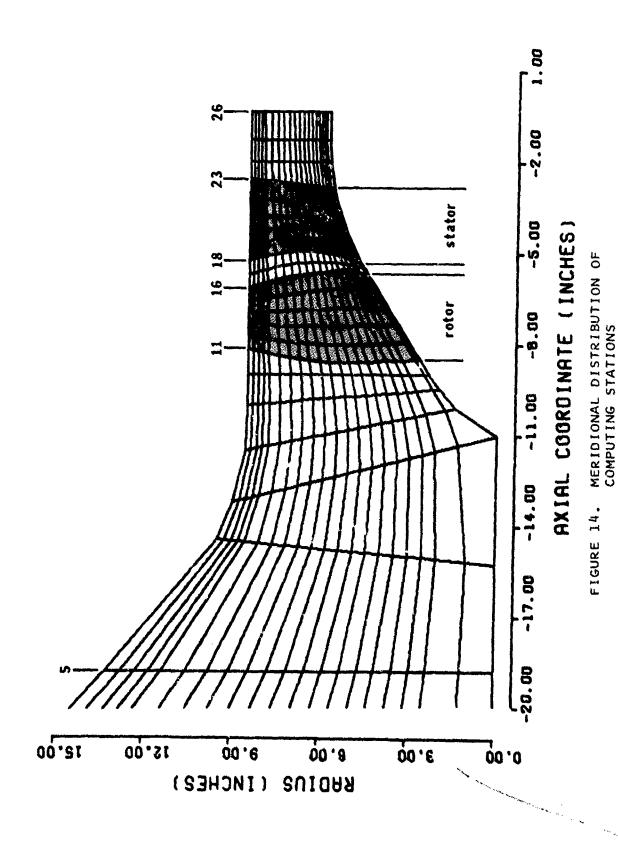


FIGURE 13. ROTOR UNTWIST DISTRIBUTION



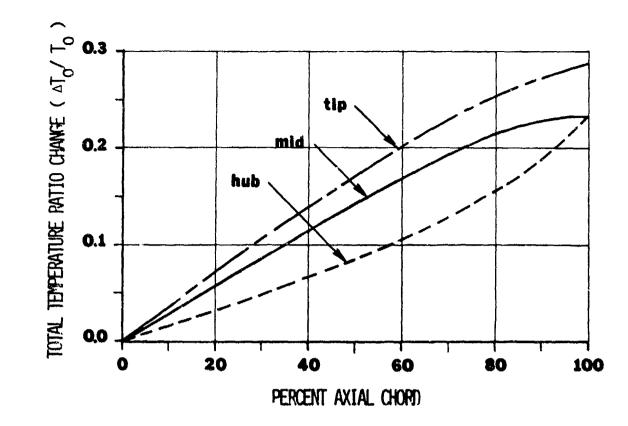


FIGURE 15A. AXIAL DISTRIBUTION OF TOTAL TEMPERATURE THROUGH ROTOR

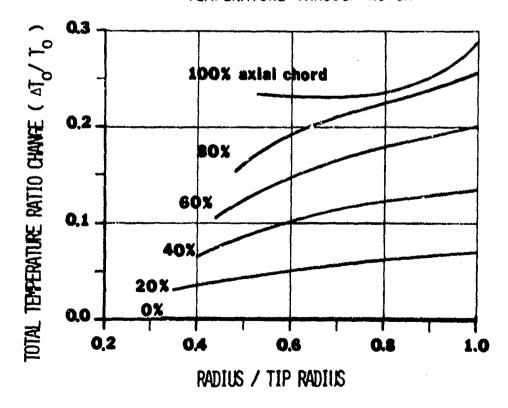


FIGURE 15B. SPANWISE DISTRIBUTION OF TOTAL TEMPERATURE THROUGH ROTOR

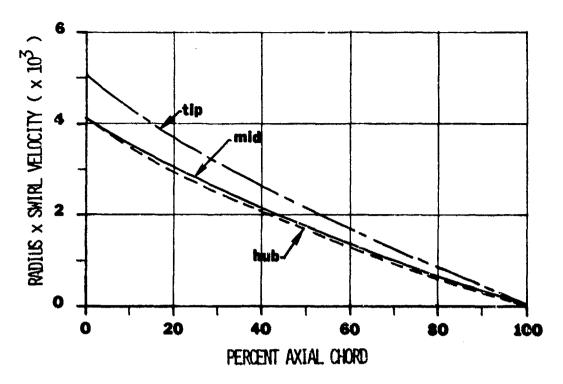


FIGURE 16A. AXIAL DISTRIBUTION OF RADIUS X SWIRL VELOCITY THROUGH STATOR

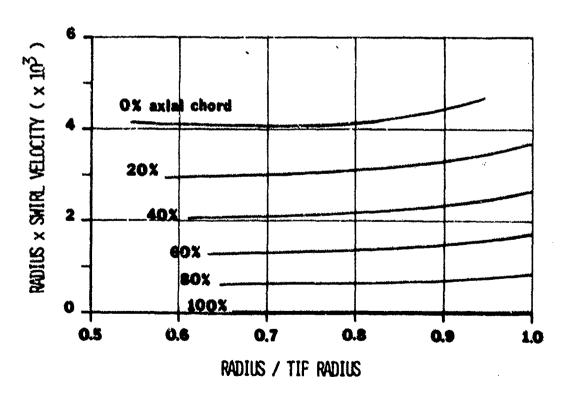


FIGURE 16B. SPANWISE DISTRIBUTION OF RADIUS X SWIRL VELOCITY THROUGH STATOR

FIGURE 17. MERIDIONAL STATIC PRESSURE DISTRIBUTIONS THROUGH STAGE

AXIAL COORDINATE (INCPES)

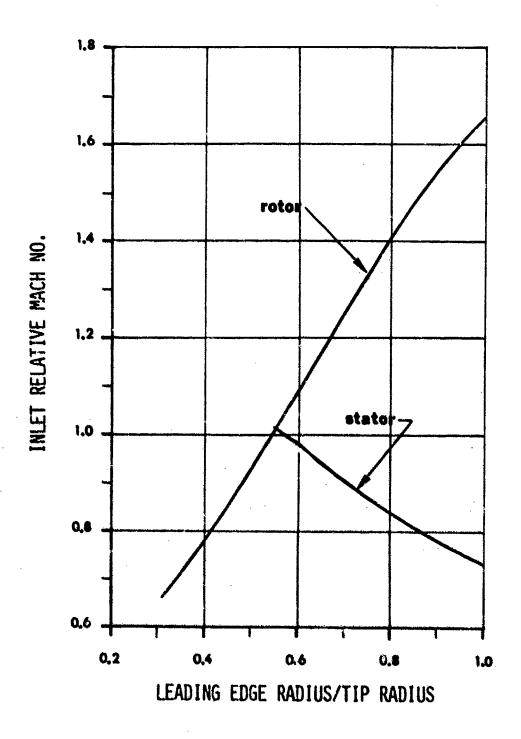


FIGURE 18. ROTOR AND STATOR RELATIVE INLET MACH NUMBER DISTRIBUTIONS

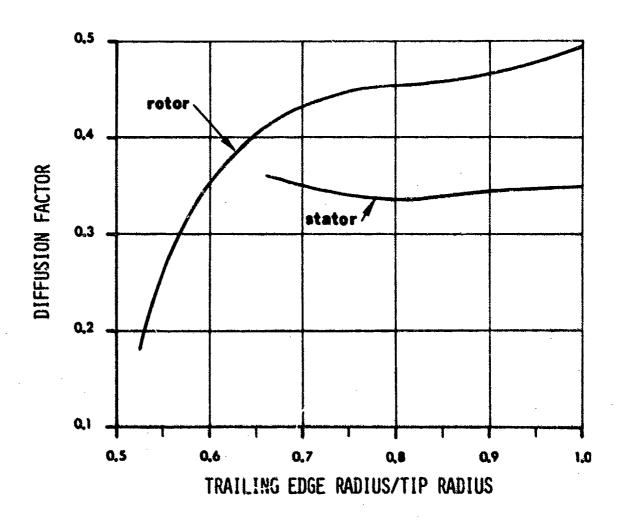


FIGURE 19. ROTOR AND STATOR DIFFUSION FACTOR DISTRIBUTIONS

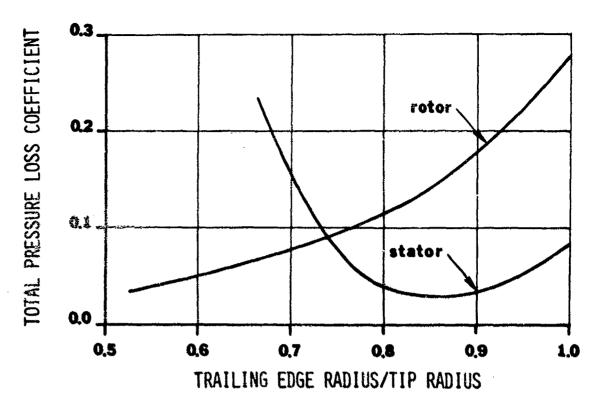


FIGURE 20. ROTOR AND STATOR TOTAL PRESSURE LOSS COEFFICIENT DISTRIBUTIONS

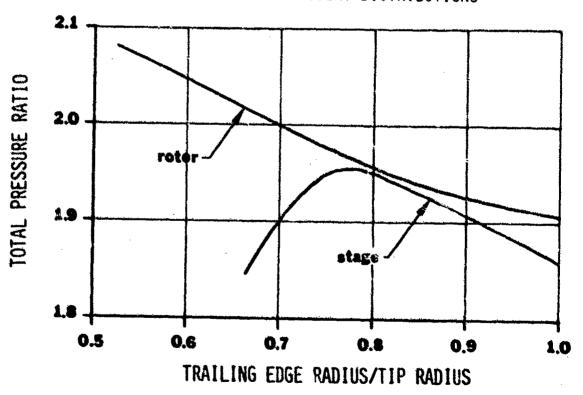


FIGURE 21. ROTOR AND STAGE EXIT TOTAL PRESSURE RATIO DISTRIBUTIONS

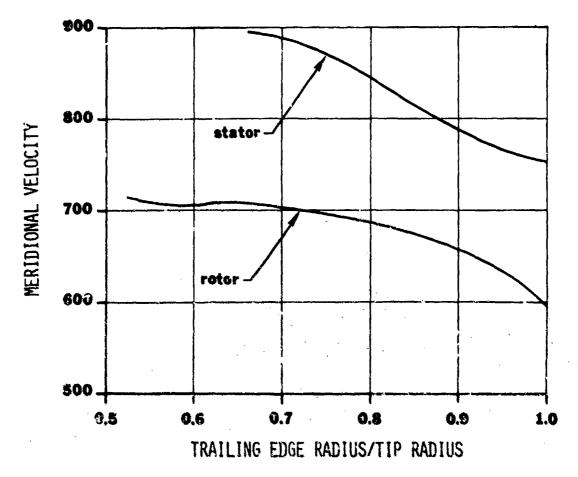


FIGURE 22. ROTGR AND STAGE EXIT MERIDIONAL VELOCITY DISTRIBUTIONS

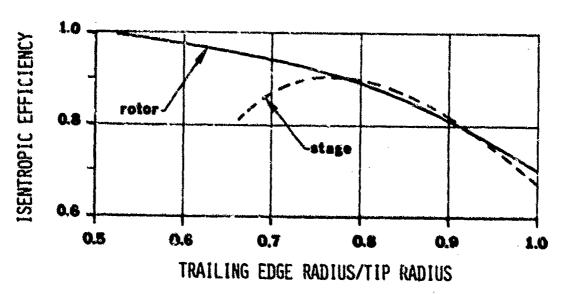


FIGURE 23. ROTOR AND STAGE EXIT ISENTROPIC EFFICIENCY DISTRIBUTIONS

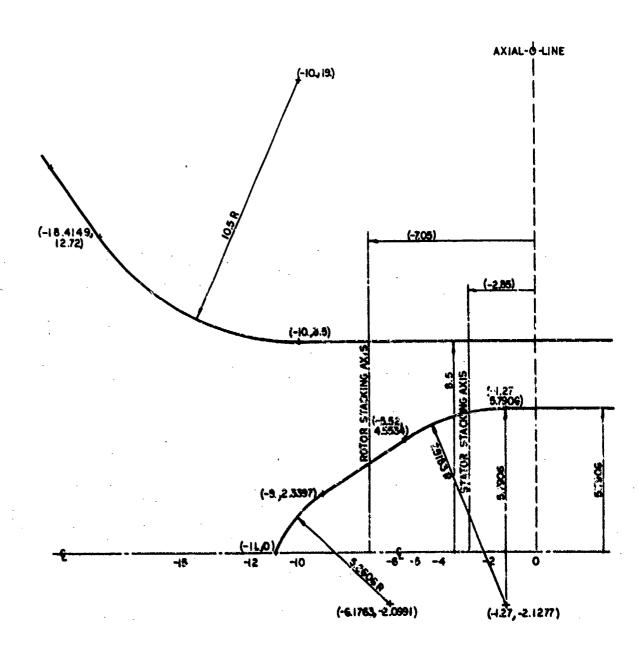


FIGURE 24. STAGE ANNULUS GEOMETRY

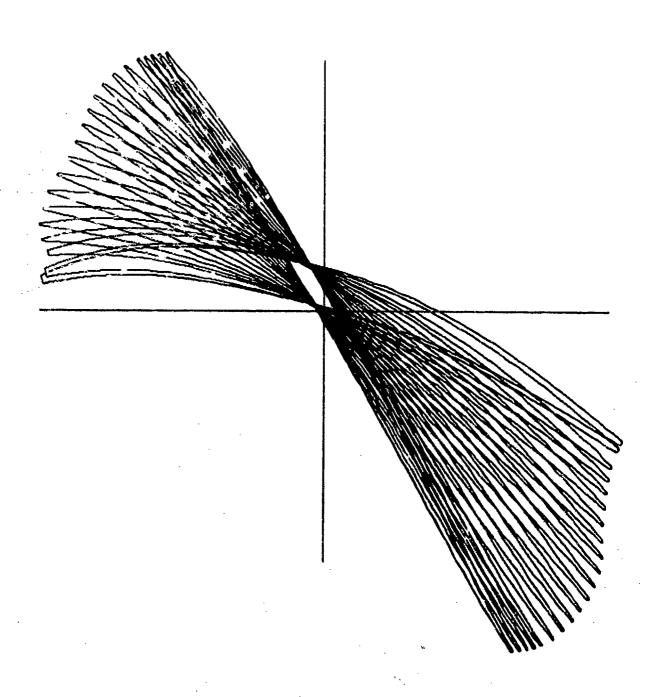


FIGURE 25. STACKED ROTOR STREAMSURFACE SECTIONS

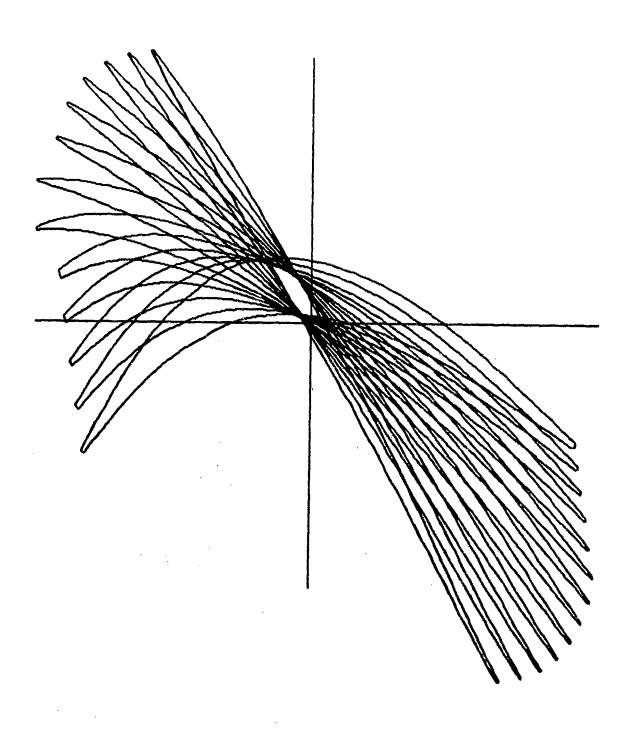


FIGURE 26. STACKED ROTOR CARTESIAN SECTIONS



FIGURE 27. STACKED STATOR STREAMSURFACE SECTIONS



FIGURE 28. STACKED STATOR CARTESIAN SECTIONS

### REFERENCES

- 1. Creveling, H.F. and Carmody, R.H., "Axial Flow Compressor Design Computer Programs Incorporating Full Radial Equilibrium, Part II-Radial Distribution of Total Pressure and Flow Path or Axial Velocity Ratio Specified (Program III)," NASA CR-54531, Department of Commerce Clearinghouse N68-38057, National Aeronautics and Space Administration, Lewis Research Center, June 1968.
- Miller, G.R., Lewis, G.W., and Hartmann, M.J., "Shock Losses in Transonic Compressor Blade Rows," Transactions of the American Society of Mechanical Engineers, Vol. 83, Series A, No. 3, pp. 235-242, July 1961.
- 3. Monsarrat, N.T., Keenan, M.J., and Tramm, P.C. "Design Report, Single-Stage Evaluation of Highly-Loaded, High-Mach-Number Compressor Stages," NASA CR-72562, National Aeronautics and Space Administration, Lewis Research Center, July 1969.
- 4. Hearsey, Richard M., "A Revised Computer Program for Axial Compressor Design," ARL TR 75-0001, Vols. I & II, A009273 and A009157, Aerospace Research Laboratories, Wright-Patterson AFB, Ohio, January 1975.
- 5. Wennerstrom, A.J., "On the Treatment of Body Forces in the Radial Equilibrium Equation of Turbomachinery," <u>Traupel-Festschrift</u>, Juris-Verlag, Zurich, 1974, pp. 351-367.
- 6. Jansen, W., "The Application of End-Wall Boundary Layer Effects in the Performance Analyses of Axial Compressors," ASME 67-WA/GT-11, The American Society of Mechanical Engineers, 1967.
- 7. Frost, George R. and Wennerstrom, Arthur J., "The Design of Axial Compressor Airfoils using Arbitrary Camber Lines," Aerospace Research Laboratories, Wright-Patterson Air Force Base, Ohio, ARL TR 73-0107, AD756165, July 1973.
- 8. Johnson, I.A., Bullock, R.O. et al., "Aerodynamic Design of Axial Flow Compressors," NASA Lewis Research Center, Cleveland, Ohio, NASA SP-36, 1965.
- 9. Frost, George R., Hearsey, Richard M. and Wennerstrom, Arthur J., "A Computer Program for the Specification of Axial Compressor Airfoils," Aerospace Research Laboratories, Wright-Patterson Air Force Base, Ohio, ARL TR 72-0171, AD756879, December 1972.

### APPENDIX A

### COMPUTER PROGRAM MODIFICATION FOR SUPERSONIC EXPANSION ANGLE

One modification was incorporated into the computer program described in Reference 1. This modification allowed the user to specify the supersonic expansion angle directly, in lieu of specifying the relative flow angle at the shock. This option proved much easier to employ than the original options when neither the relative flow angles nor the cambers were known to within three or four degrees.

The following card replacements are required:

Change 1: Subprogram LOSS, Card LOSE 2223
Replacement:
25 FRDEL(L,J) = AA/RADIAN

Change 2: Subprogram LOSS, Card LOSE 2224
Replacement:
FRDEL(L+1,J) = BB/RADIAN

Change 3: Subprogram OUTPUT, Three continuation cards in format statement 51 (after LJT. 2987)

Roplacement:

X 8HPRESSURE 3X 16H DELTA B, IN - 3X 8H SOLIDITY 23X 5H WHIRL 5X

X16H DELTA B, IN - 3X 8HSOLIDITY/11X 7PROFILE 4X X16H LET TO SHOCK 33X 8HVELOCITY 3X 16H LET TO SHOCK//)

This option is triggered by the integer 4 in columns 21-25 of Data Card number 5. Suitable descriptive corrections concerning this option should be entered on pages D-3 (under heading "Col. 21-23") and D-10 (under "Card Type 20").